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U. S. COAST AND GEODETIC SURVEY

E. LESTER JONES, SUPERINTENDENT

GEODESY

INVESTIGATIONS OF GRAVITY AND ISOSTASY

BY

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U. S. Coast and Geodetic Survey

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INVESTIGATIONS OF GRAVITY AND ISOSTASY.

By WILLIAM BOWIE, *Chief of the Division of Geodesy.*

INTRODUCTION.

For a number of years the United States Coast and Geodetic Survey has been carrying on geodetic investigations of isostasy, with special reference to the effect of the isostatic compensation upon the deflection of the vertical and the intensity of gravity.

Four reports on these investigations have appeared, the first one in 1909 and the last in 1912.*

The first two dealt with the determination of the figure of the earth from deflections of the vertical in the United States, corrected for topography and isostatic compensation. In the last two there were given the results of the investigation of the effect of topography and isostatic compensation upon the intensity of gravity at stations mostly in the United States.

The present volume gives the results of further study of the relation between gravity and isostasy. In it are embodied the gravity data resulting from the previous work. In the second gravity report 124 stations in the United States were considered, while in the investigation of which this volume is a report there are listed 219 gravity stations in the United States, 42 stations in Canada, 73 stations in India, and 40 others, principally in Europe. The Canadian stations were established by F. A. McDiarmid, of the Geodetic Survey of Canada. He reduced those stations for topography and isostatic compensation after the method described in Special Publication No. 10. The late director of the Geodetic Survey of Canada, Dr. W. F. King, generously furnished to the United States Coast and Geodetic Survey the results of their work for incorporation with the United States stations in some phases of this investigation, previous to their publication in Canada.

This report has as its main features:

1. The observed value of the intensity of gravity at stations in the United States, Canada, India, and Europe and at a few scattering stations.
2. Discussions of the relations between the gravity anomalies and the topography, the large areas of erosion and deposition, the geological formation as indicated by the surface rock at the stations, and the elevation of the station.
3. The regional versus the local distribution of isostatic compensation.
4. The determination of a gravity equation, the earth's flattening, and the depth of compensation upon each of several assumptions.
5. Summaries of the results of the field observations with the pendulums. These furnish a basis upon which to judge the accuracy of the determination of the intensity of gravity at the various stations.
6. The illustrations in the pocket at the back of the volume, which give graphically much data resulting from this investigation.

There are other lines along which investigations might have been made. Some of these may be undertaken at a later date as more data become available. One of these is the detailed study of certain regions where there are gravity and deflection stations and where the evidence

* Figure of the Earth and Isostasy from Measurements in the United States, by J. F. Hayford, 1909; Supplementary Investigation in 1909 of the Figure of the Earth and Isostasy, by J. F. Hayford, 1910; Effect of Topography and Isostatic Compensation upon the Intensity of Gravity, by J. F. Hayford and William Bowie (Special Publication No. 10), 1912; same title, second paper, by William Bowie (Special Publication No. 12), 1912.

points to strong local disturbances or causes which change the size and sign of the gravity anomalies at stations grouped comparatively close together. This phase of the subject is an important one and has been urged upon the Survey by several scientists of note.

It is hoped that many of those who are interested in the subject of isostasy will use the data contained in this and similar publications of the Survey for detailed study and investigation. It is only in this way that the data collected and published can be fully utilized. The time which can be placed on this work by members of the Survey is necessarily limited, because of many other lines of duty calling for prompt attention.

It is believed that it is desirable to publish promptly the observed values of the intensity of gravity and the reductions for topography and isostatic compensation rather than to delay for exhaustive detailed studies.

The author desires to express his appreciation of the important part taken by a number of the members of the Survey in the investigations covered by this report and in the preparation of the report itself. Especial credit is due Computers W. D. Lambert, Sarah Beall, H. G. Avers, C. H. Swick, E. F. Church, and G. E. Selby.

Assistants C. L. Garner and J. D. Powell deserve much credit for the efficient way in which they carried on the field work while establishing the 94 new stations. They did this work with great accuracy and economy. They also assisted in the office reductions.

As far as possible this report follows the general plan of the two previous gravity reports of the Survey. As the writer is the author of the second of those reports and a joint author of the first, some of the statements and definitions contained in the text of this volume may be similar to those in the former reports. Under the circumstances it is not necessary to set them off from the other text.

In Part I of this volume are given the results of the investigations, and in Part II the abstracts or summaries of observations in the field and the descriptions of the stations.

Anyone wishing to make a detailed study of the subject covered by this report should consult the four reports whose titles are given in the footnote on page 5. They may be obtained through the Division of Publications of the Department of Commerce, Washington, D. C.

Part I.—INVESTIGATION OF GRAVITY AND ISOSTASY.



Chapter I.—DEFINITION OF TERMS AND EXPLANATION OF METHODS OF COMPUTATION

ISOSTASY DEFINED.

If the earth were composed of homogeneous material, its figure of equilibrium, under the influence of gravitation^a and its own rotation, would be an ellipsoid of revolution.

The earth is composed of heterogeneous material which varies considerably in density. If this heterogeneous material were so arranged that its density at any point depended simply upon the depth of that point below the surface, or, more accurately, if all the material lying at each equipotential surface (rotation considered) were of one density, a state of equilibrium would exist, and there would be no tendency toward a rearrangement of masses. The figure of the earth in this case would be a very close approximation to an ellipsoid of revolution.

If the heterogeneous material composing the earth were not arranged in this manner at the outset, the stresses produced by gravity would tend to bring about such an arrangement; but as the material is not a perfect fluid, since it possesses considerable viscosity, at least near the surface, the rearrangement will be imperfect. In the partial rearrangement some stresses will still remain, different portions of the same horizontal stratum may have somewhat different densities, and the actual surface of the earth will be a slight departure from the ellipsoid of revolution in the sense that above each region of deficient density there will be a bulge or bump on the ellipsoid, and above each region of excessive density there will be a hollow, relatively speaking. The bumps on this supposed earth will be the mountains, the plateaus, the continents, and the hollows will be the oceans. The excess of material represented by that portion of the continent which is above sea level will be compensated for by a deficiency of density in the underlying material. The continents will be floated, so to speak, because they are composed of relatively light material; and, similarly, the floor of the ocean will, on this supposed earth, be depressed because it is composed of unusually dense material. This particular condition of approximate equilibrium has been given the name "isostasy."

The adjustment of the material toward this condition, which is produced in nature by the stresses due to gravity, may be called the "isostatic adjustment."

The compensation of the excess of matter at the surface (continents) by the deficiency of density below, and of surface deficiency of matter (oceans) by excess of density below, may be called the "isostatic compensation."

Let the depth below sea level within which the isostatic compensation is complete be called the "depth of compensation." At and below this depth the condition as to stress of any element of mass is isostatic; that is, any element of mass is subject to equal pressures from all directions as if it were a portion of a perfect fluid. Above this depth, on the other hand, each element of mass is subject in general to different pressures in different directions—to stresses which tend to distort it and to move it.

Consider the relations of the masses, densities, and volumes, above the depth of compensation, fixed by the preceding definition. The mass in any prismatic column which has for its base a unit area of the horizontal surface which lies at the depth of compensation, for

^a In this publication "gravity" is the term used for the phenomenon of weight or of the acceleration of a body falling to the earth, and, at any place, it is the resultant of the earth's attractive force, "gravitation," and the centrifugal force due to the earth's rotation. This distinction between the terms "gravity" and "gravitation" is not always clearly drawn.

In general it will be found that throughout this publication the attraction (expressed in dynes) is dealt with directly by preference rather than its numerical equivalent, the acceleration (expressed in centimeters and seconds).

its edges vertical lines (lines of gravity) and for its upper limit the actual irregular surface of the earth (or the sea surface, if the area in question is beneath the ocean), is the same as the mass in any other similar prismatic column having any other unit area of the same surface for its base.

ASSUMPTIONS MADE IN REGARD TO THE TOPOGRAPHY AND ISOSTATIC COMPENSATION.

For the purpose of making the computations by the Hayford method the earth's crust is assumed to be in a state of perfect isostasy, with each topographic feature compensated for by a deficiency (or excess) of mass directly under it, and it is assumed that this compensating deficiency (or excess) of mass is uniformly distributed to a depth of 113.7 km. This depth is that resulting from the first investigation by Hayford given in the Figure of the Earth and Isostasy from Measurements in the United States.

The mean density of the solid portion of the earth's surface is assumed to be 2.67 and the density of the ocean water 1.027. There is no assumption regarding the normal densities in the earth's crust below sea level. This fact should be clearly borne in mind, for a failure to realize this has been confusing to some who have considered the question of isostasy. It is simply assumed that the arrangement of the densities in the crust under a coastal plane at zero elevation is normal and that the densities under the continents, islands, and the oceans depart from the normal condition by the amount necessary to distribute the isostatic compensation uniformly with respect to depth of compensation. For our purpose a knowledge of the actual density at any given depth is unnecessary.

The writer does not believe any one of the assumptions stated above is exactly true. The average density (from Harkness's *The Solar Parallax and Its Related Constants*, p. 92) is certainly in error for the surface materials at many stations. The depth of compensation has a large probable error and may be largely in error for any given place. As it is the average or mean depth it may be subject to an actual error of considerable size. It is probable that the compensation for a topographic feature is not always distributed with exact uniformity with respect to depth. And it is also probable that the compensation is not located directly under a topographic feature. It may have a greater horizontal extent than the feature. The anomalies or differences between the observed gravity and the computed gravity give an idea of the extent to which the assumptions are not true. These differences are due partly to errors in the observations and computations, but mostly to departures from the conditions postulated. But it may be stated that the results show that the continents as a whole are almost perfectly compensated and that this is the condition with respect to large portions of a continent. One of the important problems of the geodesist is to determine the limits of the areas which may not be at least partly compensated.

CHANGE OF SIGN DUE TO DISTANCE.

The reader should consult pages 65 to 70 of Special Publication No. 10, which deals with the change of sign of the effect of topography and compensation due to distance.

In nearly all cases the combined effect of the topography and compensation changes sign from plus to minus before zone L is reached. This zone has an inner limit which is only 19 km. from the station. This is an important matter which should be considered by anyone studying the question of isostasy and its effect upon the intensity of gravity. One might assume without due consideration that in a mountainous region a station should have large positive corrections for each of the near zones, say within zone N, outer limit 99 km., while they may have large negative values. Pikes Peak, for example, has corrections of -0.0290 and -0.0334 dynes, respectively, for zones M and N.

The explanation of the change in sign is given in detail in Special Publication No. 10. Briefly, it is that near the station the topography has the predominating effect, as it is much closer than the center of mass of the compensation. As the distance from the station increases the ratio between the sine of the depression angle to the center of the compensation and the sine of the angle of elevation or depression to the center of the topography becomes greater.

At the same time the ratio of the distances to the compensation and to the topography becomes less. Therefore at a certain distance the vertical component of the effect of the compensation becomes greater than that of the topography.

It is evident that at great distances from the station the effect of the compensation will be greater than the topography. It should be noted that the effect of topography in the oceans is negative and its compensation positive. This fact causes the combined effect for the more distant zones, which cover water areas mostly, to be positive. These facts may be observed by referring to the table given on pages 20-48.

REDUCTION TABLES FOR EFFECT OF TOPOGRAPHY AND ISOSTATIC COMPENSATION.

The tables for making the reduction for topography and compensation were computed upon the theory that the earth's crust is in a state of perfect isostasy with a surface density of 2.67 and a density of water in the oceans of 1.027, that the compensation is complete directly under the topography, and that the depth of compensation is 113.7 km. These tables with detailed statements as to the methods employed in computing them, and directions for using them are printed in Special Publication No. 10, entitled, "The effect of topography and isostatic compensation upon the intensity of gravity," United States Coast and Geodetic Survey, 1912. It is not desirable to repeat the tables with descriptions showing how to use them. The tables are made for 33 zones, which cover the entire surface of the earth, it having been found that the resultant attraction of the topography and compensation even at the antipodes must be taken into account.

It has been found possible to save much effort in making the computations by interpolating the values for the effect of the topography and compensation for the outer zones for a station from the values for those zones computed for surrounding stations. The saving will be greater when the new station is very close to the stations used for the interpolation. The subject of interpolation is discussed fully on pages 58 to 65 of Special Publication No. 10.

CORRECTIONS AND ADDITIONS TO TABLES.

Since its publication some errors were discovered in the reduction table for zone C. This table is repeated below with the corrected numbers in boldface type. These errors had no appreciable effect on the results of the investigations reported in Special Publications Nos. 10 and 12.

On pages 11 to 18 there are given additional tables which should be used when computing the effect of topography and compensation for the close topography at mountain stations. (See p. 94.)

For computing the effect of using the tables for a subdivided zone instead of the table for the entire zone, the elevation of the entire zone must be made consistent with the elevation of its parts. If h_1 and h_2 are, respectively, the elevations of the inner and outer subzones and h the average elevation of the entire zone, then,

for zone C,	$h = h_2 + 0.255 (h_1 - h_2),$
for zone D,	$h = h_2 + 0.310 (h_1 - h_2),$
for zone E,	$h = h_2 + 0.317 (h_1 - h_2),$
for zone F,	$h = h_2 + 0.328 (h_1 - h_2).$

In conformity with the reduction tables in Special Publication No. 10 all tabular values in the following tables are expressed in units of the fourth decimal place in dynes.

[Inner radius, 68 meters; outer radius, 230 meters. Four compartments.]

^a This table should be used instead of the table for zone C as given on p. 31 of Special Publication No. 10.

REDUCTION TABLES FOR DIVIDED ZONES.

Zone C_1 .

[Inner radius, 68 meters; outer radius, 130 meters. Four compartments.]

Mean elevation of compartment, in feet	Correction for—		Correction for elevation of station—											
	Topography.	Compensation.	Above compartment						Below compartment					
			50 feet	100 feet	150 feet	200 feet	250 feet	300 feet	350 feet	400 feet	450 feet	500 feet	550 feet	600 feet
25	+0.1	0	0	0	0	0	+1	0	0	0	0	0	0	0
50	+0.2	0	0	+1	+1	+1	+1	+1	0	0	0	0	0	0
75	+0.3	0	0	+1	+1	+1	+1	+1	0	0	0	0	0	0
100	+0.4	0	+1	+1	+1	+1	+1	+1	0	0	0	0	0	0
150	+1.7	0	+1	+1	+1	+1	+1	+1	0	0	0	0	0	0
200	+2.7	0	+1	+1	+1	+1	+1	0	0	0	0	0	0	0
300	+4.8	0	+1	+1	+1	+1	0	0	0	0	0	0	0	0
400	+6.5	0	+1	+1	+1	0	0	0	0	0	0	0	0	0
500	+8.0	0	+1	+1	0	0	0	0	0	0	0	0	0	0
600	+9.2	0	0	0	0	0	0	0	0	0	0	0	0	0
800	+10.9	0	0	0	0	0	0	0	0	0	0	0	0	0
1 000	+12.0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 200	+12.8	0	0	0	0	0	0	0	0	0	0	0	0	0
1 400	+13.4	0	0	0	0	0	0	0	0	0	0	0	0	0
1 600	+13.9	0	0	0	0	0	0	0	0	0	0	0	0	0
1 800	+14.3	0	0	0	0	0	0	0	0	0	0	0	0	0
2 000	+14.6	0	0	0	0	0	0	0	0	0	0	0	0	0
2 500	+15.1	0	0	0	0	0	0	0	0	0	0	0	0	0
3 000	+15.5	0	0	0	0	0	0	0	0	0	0	0	0	0
3 500	+15.8	0	0	0	0	0	0	0	0	0	0	0	0	0
4 000	+16.0	0	0	0	0	0	0	0	0	0	0	0	0	0
5 000	+16.2	0	0	0	0	0	0	0	0	0	0	0	0	0
6 000	+16.4	0	0	0	0	0	0	0	0	0	0	0	0	0
8 000	+16.6	0	0	0	0	0	0	0	0	0	0	0	0	0
10 000	+16.8	0	0	0	0	0	0	0	0	0	0	0	0	0
12 000	+16.9	0	0	0	0	0	0	0	0	0	0	0	0	0
14 000	+17.0	0	0	0	0	0	0	0	0	0	0	0	0	0
16 000	+17.0	0	0	0	0	0	0	0	0	0	0	0	0	0
18 000	+17.0	0	0	0	0	0	0	0	0	0	0	0	0	0

Corrected reduction table for Zone C.^a

[Inner radius, 68 meters; outer radius, 230 meters. Four compartments.]

Mean elevation of compartment	Correction for—		Correction for elevation of station—											
	Topography	Topography and compensation	Above compartment						Below compartment					
			50 feet	100 feet	150 feet	200 feet	250 feet	300 feet	350 feet	400 feet	450 feet	500 feet	600 feet	
Fathoms	-9	-4	0	0	0	0	0	0	0	0	0	0	0	
80	-9	-4	0	0	0	0	0	0	0	0	0	0	0	
40	-9	-4	0	0	0	0	0	0	0	0	0	0	0	
Fetd	0	0	0	0	0	0	0	0	0	0	0	0	0	
25	0	0	0	0	0	0	0	0	0	0	0	0	0	
50	0	0	0	0	0	0	0	0	0	0	0	0	0	
75	0	0	0	0	0	0	0	0	0	0	0	0	0	
100	0	0	0	0	0	0	0	0	0	0	0	0	0	
150	0	0	0	0	0	0	0	0	0	0	0	0	0	
200	0	0	0	0	0	0	0	0	0	0	0	0	0	
300	0	0	0	0	0	0	0	0	0	0	0	0	0	
400	0	0	0	0	0	0	0	0	0	0	0	0	0	
500	0	0	0	0	0	0	0	0	0	0	0	0	0	
600	0	0	0	0	0	0	0	0	0	0	0	0	0	
800	0	0	0	0	0	0	0	0	0	0	0	0	0	
1 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
1 200	0	0	0	0	0	0	0	0	0	0	0	0	0	
1 400	0	0	0	0	0	0	0	0	0	0	0	0	0	
1 600	0	0	0	0	0	0	0	0	0	0	0	0	0	
1 800	0	0	0	0	0	0	0	0	0	0	0	0	0	
2 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
2 500	0	0	0	0	0	0	0	0	0	0	0	0	0	
3 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
3 500	0	0	0	0	0	0	0	0	0	0	0	0	0	
4 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
5 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
6 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
8 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
10 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
12 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
14 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
16 000	0	0	0	0	0	0	0	0	0	0	0	0	0	
18 000	0	0	0	0	0	0	0	0	0	0	0	0	0	

^a This table should be used instead of the table for zone C as given on p. 31 of Special Publication No. 10.

REDUCTION TABLES FOR DIVIDED ZONES.

Zone C₁.

[Inner radius, 68 meters; outer radius, 130 meters. Four compartments.]

Mean elevation of compartment, in feet	Correction for—		Correction for elevation of station—											
	Topography.	Compensation.	Above compartment						Below compartment					
			50 feet	100 feet	150 feet	200 feet	250 feet	300 feet	350 feet	400 feet	450 feet	500 feet	550 feet	600 feet
25	+0.1	0	0	0	0	0	0	0	0	0	0	0	0	0
50	+0.2	0	+1	+1	+1	+1	+1	+1	0	0	0	0	0	0
75	+0.3	0	+1	+1	+1	+1	+1	+1	0	0	0	0	0	0
100	+0.8	0	+1	+1	+1	+1	+1	+1	0	0	0	0	0	0
150	+1.7	0	+1	+1	+1	+1	+1	+1	0	0	0	0	0	0
200	+2.7	0	+1	+1	+1	+1	+1	0	0	0	0	0	0	0
300	+4.8	0	+1	+1	+1	0	0	0	0	0	0	0	0	0
400	+6.5	0	+1	+1	0	0	0	0	0	0	0	0	0	0
500	+8.0	0	+1	+1	0	0	0	0	0	0	0	0	0	0
600	+9.2	0	0	0	0	0	0	0	0	0	0	0	0	0
800	+10.9	0	0	0	0	0	0	0	0	0	0	0	0	0
1 000	+12.0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 200	+12.8	0	0	0	0	0	0	0	0	0	0	0	0	0
1 400	+13.4	0	0	0	0	0	0	0	0	0	0	0	0	0
1 600	+13.9	0	0	0	0	0	0	0	0	0	0	0	0	0
1 800	+14.3	0	0	0	0	0	0	0	0	0	0	0	0	0
2 000	+14.6	0	0	0	0	0	0	0	0	0	0	0	0	0
2 500	+15.1	0	0	0	0	0	0	0	0	0	0	0	0	0
3 000	+15.5	0	0	0	0	0	0	0	0	0	0	0	0	0
3 500	+15.8	0	0	0	0	0	0	0	0	0	0	0	0	0
4 000	+16.0	0	0	0	0	0	0	0	0	0	0	0	0	0
5 000	+16.2	0	0	0	0	0	0	0	0	0	0	0	0	0
6 000	+16.4	0	0	0	0	0	0	0	0	0	0	0	0	0
8 000	+16.6	0	0	0	0	0	0	0	0	0	0	0	0	0
10 000	+16.8	0	0	0	0	0	0	0	0	0	0	0	0	0
12 000	+16.9	0	0	0	0	0	0	0	0	0	0	0	0	0
14 000	+17.0	0	0	0	0	0	0	0	0	0	0	0	0	0
16 000	+17.0	0	0	0	0	0	0	0	0	0	0	0	0	0
18 000	+17.0	0	0	0	0	0	0	0	0	0	0	0	0	0

Zone C₂.

[Inner radius, 130 meters; outer radius, 230 meters. Four compartments.]

Mean elevation of compartment, in feet	Correction for—			Correction for elevation of station—																					
	Topography	Compensation	Topography and compensation	Above compartment										Below compartment											
				50 feet	100 feet	150 feet	200 feet	250 feet	300 feet	350 feet	400 feet	450 feet	500 feet	600 feet	50 feet	100 feet	150 feet	200 feet	250 feet	300 feet	350 feet	400 feet	450 feet	500 feet	600 feet
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
50	+0.1	0	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
75	+0.2	0	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
100	+0.4	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
150	+0.9	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
200	+1.6	0	+2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
300	+3.2	0	+3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
400	+5.0	0	+5	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
500	+6.8	0	+7	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
600	+8.5	0	+8	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
800	+11.5	0	+12	0	+1	+1	+1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 000	+13.8	0	+14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 200	+15.7	0	+16	0	0	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
1 400	+17.2	0	+17	0	0	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
1 600	+18.3	0	+18	0	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
1 800	+19.3	0	+19	0	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
2 000	+20.1	0	+20	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
2 500	+21.6	0	+22	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
3 000	+22.6	0	+23	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
3 500	+23.3	0	+23	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4 000	+23.9	0	+24	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
5 000	+24.7	0	+25	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
6 000	+25.2	0	+25	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
8 000	+25.9	0	+26	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
10 000	+26.3	0	+26	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
12 000	+26.6	-1	+26	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
14 000	+26.8	-1	+26	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
16 000	+27.0	-1	+26	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
18 000	+27.1	-1	+26	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1

Zone D₁.

[Inner radius, 230 meters; outer radius, 380 meters. Six compartments.]

Mean elevation of compartment, in feet	Correction for—		Correction for elevation of station—																																									
	Topography	Compensation	Above compartment										Below compartment																															
			100 feet	200 feet	300 feet	400 feet	500 feet	600 feet	700 feet	800 feet	900 feet	1000 feet	1100 feet	100 feet	200 feet	300 feet	400 feet	500 feet	600 feet	700 feet	800 feet	900 feet	1000 feet	1100 feet																				
100	0.1	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
200	+0.6	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
300	+1.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
400	+2.1	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
500	+3.1	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
600	+4.1	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
700	+5.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
800	+6.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
900	+7.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 000	+8.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 100	+9.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 200	+10.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 300	+11.0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 400	+11.8	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 500	+12.5	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 600	+13.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 700	+13.9	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 800	+14.5	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
1 900	+15.0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
2 000	+15.5	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
2 200	+16.4	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
2 400	+17.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
2 600	+18.0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
2 800	+18.6	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
3 000	+19.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
3 200	+19.7	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
3 400	+20.1	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
3 600	+20.5	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
3 800	+20.9	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
4 000	+21.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
4 500	+21.9	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
5 000	+22.5	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
5 500	+23.0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
6 000	+23.4	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
6 500	+23.7	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
7 000	+24.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
7 500	+24.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
8 000	+24.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
8 500	+24.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
9 000	+24.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	0	-1	-2	-3	-4	-6	-7	-8	-9	-10	-11	-12	-13	-14	-15	-16	-17	-18	-19	-20	-21	-22	-23	-24	-25	-26	-27	-28	-29	-30
9 500	+25.1	-1	+1	+																																								

Zone E₃.

[Inner radius, 870 meters; outer radius, 1280 meters. Eight compartments.]

Mean elevation of compartment, in feet	Correction for—		Correction for elevation of station—															
	Topog-raphy	Com-pensa-tion	Above compartment								Below compartment							
			200 feet	400 feet	600 feet	800 feet	1000 feet	1200 feet	1400 feet	1600 feet	1800 feet	2000 feet	2200 feet	2400 feet	2600 feet	2800 feet	3000 feet	3200 feet
200	+0.1	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
400	+0.6	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
600	+0.8	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
800	+1.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 000	+2.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 200	+3.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 400	+5.2	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 600	+6.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 800	+7.6	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 000	+8.9	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 200	+10.1	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 400	+11.4	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 600	+12.6	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 800	+13.9	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 000	+15.1	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 200	+16.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 400	+17.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 600	+18.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 800	+19.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 000	+20.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 200	+21.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 400	+22.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 600	+23.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 800	+24.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 000	+25.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 200	+26.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 400	+26.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 600	+27.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 800	+28.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 000	+29.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 200	+30.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 400	+31.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 600	+31.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 800	+32.8	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 000	+33.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 200	+34.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 400	+35.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 600	+36.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 800	+37.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 000	+38.2	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 200	+39.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 400	+40.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 600	+40.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 800	+41.8	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 000	+42.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 200	+43.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 400	+44.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 600	+45.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 800	+46.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 000	+47.2	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 200	+48.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 400	+49.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 600	+49.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 800	+50.8	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 000	+51.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 200	+52.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 400	+53.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 600	+54.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 800	+55.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 000	+56.2	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 200	+57.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 400	+58.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 600	+58.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 800	+59.8	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 000	+60.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 200	+61.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 400	+62.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 600	+63.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 800	+64.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 000	+65.2	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 200	+66.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 400	+67.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 600	+67.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 800	+68.8	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
15 000	+69.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1

Zone F_1 .

[Inner radius, 1280 meters; outer radius, 1680 meters. Ten compartments.]

Mean elevation of compartment, in feet	Correction for —		Correction for elevation of station —															
	Topography	Compensation	Above compartment								Below compartment							
			200 feet	400 feet	600 feet	800 feet	1000 feet	1200 feet	1400 feet	1600 feet	1800 feet	2000 feet	2200 feet	2400 feet	2600 feet	2800 feet	3000 feet	3200 feet
200	0.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
400	0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
600	0.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
800	0.6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 000	0.9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 200	1.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 400	1.8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 600	2.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 800	2.8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2 000	3.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2 200	4.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2 400	4.7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2 600	5.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2 800	6.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3 000	6.8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3 200	7.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3 400	8.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3 600	8.9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3 800	9.6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4 000	10.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4 200	11.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4 400	11.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4 600	12.4	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4 800	13.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5 000	13.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5 200	14.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5 400	14.9	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5 600	15.5	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5 800	16.1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6 000	16.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6 200	17.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6 400	17.8	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6 600	18.4	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6 800	18.8	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7 000	19.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7 200	19.8	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7 400	20.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7 600	20.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7 800	21.1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8 000	21.6	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8 200	22.1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8 400	22.4	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8 600	22.8	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8 800	23.2	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9 000	23.6	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9 200	23.9	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9 400	24.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9 600	24.6	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9 800	25.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10 000	25.2	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10 200	25.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10 400	26.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10 600	26.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10 800	26.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11 000	27.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11 200	27.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11 400	27.6	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11 600	28.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11 800	28.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12 000	28.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12 200	29.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12 400	29.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12 600	29.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12 800	30.1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13 000	30.4	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13 200	30.7	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13 400	31.0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13 600	31.3	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13 800	31.6	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14 000	31.9	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14 200	32.2	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14 400	32.5	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14 600	32.8	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14 800	33.1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15 000	33.4	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Zone F_2 .

[Inner radius, 1680 meters; outer radius, 2280 meters. Ten compartments.]

Mean elevation of compartment, in feet	Correction for—		Correction for elevation of station—															
	Topography	Compensation	Above compartment								Below compartment							
			200 feet	400 feet	600 feet	800 feet	1000 feet	1200 feet	1400 feet	1600 feet	1800 feet	2000 feet	2200 feet	2400 feet	2600 feet	2800 feet	3000 feet	3200 feet
200	0.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
400	+0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
600	+0.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
800	+0.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 000	+0.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 200	+1.2	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 400	+1.6	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 600	+2.0	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
1 800	+2.5	0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 000	+3.1	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 200	+3.7	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 400	+4.3	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 600	+5.0	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
2 800	+5.6	0	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 000	+6.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 200	+7.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 400	+7.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 600	+8.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
3 800	+9.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 000	+10.2	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 200	+11.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 400	+11.8	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 600	+12.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
4 800	+13.5	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 000	+14.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 200	+15.1	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 400	+15.9	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 600	+16.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
5 800	+17.4	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 000	+18.2	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 200	+19.7	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 400	+21.2	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 600	+22.6	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
6 800	+24.0	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 000	+25.3	-1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 200	+26.6	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 400	+27.8	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 600	+29.0	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
7 800	+30.0	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 000	+31.1	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 200	+32.6	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 400	+33.6	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 600	+34.4	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
8 800	+35.8	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 000	+37.8	-2	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 200	+39.5	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 400	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 600	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
9 800	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 000	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 200	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 400	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 600	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
10 800	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 000	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 200	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 400	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 600	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
11 800	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 000	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 200	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 400	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 600	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
12 800	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 000	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 200	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 400	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 600	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
13 800	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 000	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 200	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 400	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 600	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
14 800	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1
15 000	+41.1	-3	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1	+1

**Chapter II.—CORRECTIONS FOR TOPOGRAPHY AND ISOSTATIC COMPENSATION AND
PRINCIPAL FACTS FOR GRAVITY STATIONS.**

**MEAN ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND ISOSTATIC COMPENSATION FOR
SEPARATE ZONES AT STATIONS IN THE UNITED STATES.**

There are given in the following tables (pp. 20 to 45) the combined effect of the topography and compensation for all zones and the separate effects of the topography and the compensation for each of the lettered zones for the 219 stations in the United States. In addition, there is given the mean elevation of the topography for each of the lettered zones for all of the stations from No. 57 to No. 219. No record of the elevation of the topography for the separate zones was made for the first 56 stations, when the topography and compensation effects were computed, and it was not deemed expedient to read the maps again to obtain that information for publication here. With the combined effect of topography and compensation given for separate zones at the first 56 stations one may get from the tables an approximate value of the elevation of the topography for the zones. The values of the effects of topography and compensation, separately and combined, are expressed in the fourth decimal place in dynes. Values resulting from interpolation from surrounding stations are indicated by italic type. (For explanation of process of interpolation, see pp. 58-65 of Special Publication No. 10.) The following table gives the radii of the zones and the number of compartments in each of them:

Designation of zone	Inner radius of zone	Outer radius of zone	Compartments
	<i>Meters</i>	<i>Meters</i>	
A	0	2	1
B	2	68	4
C	68	230	4
D	230	590	6
E	590	1 280	8
F	1 280	2 290	10
G	2 290	3 520	12
H	3 520	5 240	16
I	5 240	8 440	20
J	8 440	12 400	16
K	12 400	18 800	20
L	18 800	28 800	24
M	28 800	58 800	14
N	58 800	99 000	16
O	99 000	166 700	28
	° / "	° / "	
18	1 29 58	1 41 13	1
17	1 41 13	1 54 52	1
16	1 54 52	2 11 53	1
15	2 11 53	2 33 46	1
14	2 33 46	3 03 05	1
13	3 03 05	4 19 13	16
12	4 19 13	5 46 34	10
11	5 46 34	7 51 30	8
10	7 51 30	10 44	6
9	10 44	14 09	4
8	14 09	20 41	4
7	20 41	28 41	2
6	26 41	35 58	18
5	35 58	51 04	16
4	51 04	72 13	12
3	72 13	105 48	10
2	105 48	150 56	6
1	150 56	180	1

Corrections for topography and isostatic compensation, separate zones, for United States stations.

Zone	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion
	Key West, Fla., No. 1			West Palm Beach, Fla., No. 2			Punta Gorda, Fla., No. 3			Apalachicola, Fla., No. 4			New Orleans, La., No. 5			Rayville, La., No. 6		
A	+1	0	+1	+2	0	+2	+1	0	+1	+2	0	+2	+1	0	+1	+2	0	+2
B	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	+20	0	+20
C	-1	0	-1	0	0	0	0	0	0	0	0	0	0	0	0	+4	0	+4
D	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	+6	0	+6
E	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
F	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
K	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
L	0	0	0	0	+5	+5	0	0	0	0	0	0	0	0	0	0	0	0
M	0	+14	+14	0	+20	+20	0	0	0	0	0	0	0	0	0	0	0	0
N	0	+42	+42	0	+24	+24	0	0	0	0	0	0	0	0	0	0	0	0
O	0	+55	+55	0	+16	+16	0	0	0	0	+6	+6	0	0	0	0	0	0
18			+8			+4			0			+2			+2			-1
17			+4			+5			+1			+3			+2			-1
16			+3			+5			+2			+4			+5			-1
15			+5			+5			+6			+9			+7			-2
14			+8			+9			+10			+11			+11			-3
13			+38			+33			+30			+17			+24			+5
12			+38			+39			+31			+11			+22			+5
11			+42			+45			+33			+9			+7			0
10			+25			+27			+22			+14			+3			-1
9			+15			+16			+14			+12			-2			-3
8			+15			+15			+13			+10			+5			+3
7			+5			+5			+5			+6			+7			+8
6			+6			+6			+6			+8			+10			+9
5			+10			+10			+10			+10			+10			+11
4			+8			+8			+8			+7			+8			+7
3			+6			+6			+6			+6			+6			+5
2			+2			+2			+2			+3			+3			+3
1			+1			+1			+1			+1			+1			+1
Total			+350			+306			+201			+151			+132			+77

	Galveston, Tex., No. 7			Point Isabel, Tex., No. 8			Laredo, Tex., No. 9			Austin, Tex. (Capitol), No. 10			Austin, Tex. (Uni- versity), No. 11			McAlester, Okla., No. 12		
A	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2
B	0	0	0	+4	0	+4	+56	0	+56	+56	0	+56	+56	0	+56	+60	0	+60
C	0	0	0	0	0	0	+50	0	+50	+64	0	+64	+72	0	+72	+87	0	+87
D	0	0	0	0	0	0	+21	0	+21	+31	0	+31	+40	0	+40	+52	0	+52
E	0	0	0	0	0	0	+8	0	+8	+15	0	+15	+16	0	+16	+21	0	+21
F	0	0	0	0	0	0	0	0	0	+2	0	+2	+6	0	+6	+10	0	+10
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	0	0	0	0	0	0	-14	-14	0	-14	-14	0	-13	-13
K	0	0	0	0	0	0	0	-4	-4	0	-18	-18	0	-18	-18	0	-16	-16
L	0	0	0	0	0	0	0	-10	-10	0	-22	-22	0	-22	-22	0	-22	-22
M	0	0	0	0	0	0	0	-24	-24	0	-41	-41	0	-41	-41	0	-46	-46
N	0	0	0	0	-1	-1	0	-25	-25	0	-43	-43	0	-43	-43	0	-35	-35
O	0	0	0	0	+27	+27	0	-21	-21	0	-44	-44	0	-44	-44	0	-40	-40
18			0			+10			-5			-8			-8			-8
17			+2			+12			-6			-8			-8			-8
16			+3			+13			-7			-7			-7			-9
15			+4			+15			-10			-7			-7			-9
14			+6			+14			-8			-7			-7			-9
13			+6			+12			-21			-12			-12			-15
12			+4			-1			-10			-9			-9			-13
11			-2			-9			-12			-7			-7			-12
10			-5			-5			-4			-11			-11			-12
9			+1			+5			+4			+1			+1			-4
8			+7			+9			+10			+7			+7			+2
7			+8			+9			+9			+9			+9			+8
6			+10			+10			+10			+10			+10			+9
5			+10			+10			+10			+10			+10			+11
4			+9			+9			+9			+9			+9			+8
3			+6			+6			+6			+6			+6			+5
2			+2			+2			+2			+2			+2			+3
1			+1			+1			+1			+1			+1			+1
Total			+74			+154			+30			-30			-11			+8

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topography	Compensation	Topography and compensation	Topography	Compensation	Topography and compensation	Topography	Compensation	Topography and compensation	Topography	Compensation	Topography and compensation	Topography	Compensation	Topography and compensation	Topography	Compensation	Topography and compensation
	Little Rock, No. 13	Ark., No. 14	Columbia, Tenn., No. 15	Atlanta, Ga., No. 16	McCormick, S. C., No. 17	Charleston, S. C., No. 18	Beaufort, N. C., No. 19											
A	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+1	0	+1			
B	+48	0	+48	+60	0	+60	+64	0	+64	+56	0	+56	0	0	0			
C	+31	0	+31	+78	0	+78	+104	0	+104	+64	0	+64	0	0	0			
D	+12	0	+12	+48	0	+48	+90	0	+90	+30	0	+30	0	0	0			
E	+5	0	+5	+19	0	+19	+40	0	+40	+13	0	+13	0	0	0			
F	0	0	0	+7	0	+7	+19	0	+19	0	0	0	0	0	0			
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
J	0	0	0	0	-12	-12	0	-16	-16	0	-2	-2	0	0	0			
K	0	-1	-1	0	-16	-16	0	-20	-20	0	-5	-5	0	0	0			
L	0	0	0	0	-17	-17	0	-24	-24	0	-7	-7	0	0	0			
M	0	-20	-20	0	-34	-34	0	-50	-50	0	-28	-28	0	0	0			
N	0	-30	-30	0	-39	-39	0	-44	-44	0	-31	-31	0	0	0			
O	0	-29	-29	0	-42	-42	0	-49	-49	0	-37	-37	0	+2	+2			
18			-5		-7	-7			-9		-7	-7		+2	+2			+14
17			-5		-7	-7			-10		-8	-8		+2	+2			+16
16			-5		-7	-7			-9		-8	-8		+2	+2			+20
15			-5		-7	-7			-7		-3	-3		+3	+3			+27
14			-5		-7	-7			-6		-3	-3		+4	+4			+34
13			-8		-10	-10			-7		-1	-1		+12	+12			+52
12			-7		-5	-5			-1		+7	+7		+21	+21			+36
11			-5		0	0			+6		+13	+13		+24	+24			+29
10			-2		+6	+6			+14		+17	+17		+21	+21			+19
9			-5		+3	+3			+9		+10	+10		+19	+19			+14
8			+2		+4	+4			+6		+8	+8		+12	+12			+14
7			+6		+6	+6			+6		+6	+6		+5	+5			+5
6			+9		+7	+7			+7		+7	+7		+6	+6			+6
5			+11		+10	+10			+10		+10	+10		+9	+9			+8
4			+7		+7	+7			+7		+7	+7		+7	+7			+7
3			+5		+6	+6			+6		+6	+6		+6	+6			+6
2			+3		+3	+3			+3		+3	+3		+3	+3			+3
1			+1		+1	+1			+1		+1	+1		+1	+1			+1
Total			+12		+59	+59			+142		+120	+120		+159	+159			+361
	Charlottesville, Va., No. 19			Deer Park, Md., No. 20			Washington, D. C., C. and G. S. Office, No. 21			Washington, D. C., Smithsonian Institution, No. 22			Baltimore, Md., No. 23			Philadelphia, Pa., No. 24		
A	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2
B	+56	0	+56	+68	0	+68	+12	0	+12	+8	0	+8	+24	0	+24	+12	0	+12
C	+62	0	+62	+144	0	+144	+2	0	+2	0	0	0	+4	0	+4	0	0	0
D	+33	0	+33	+209	0	+209	0	0	0	0	0	0	+6	0	+6	0	0	0
E	+11	0	+11	+186	-8	+178	0	0	0	0	0	0	0	0	0	0	0	0
F	+3	0	+3	+101	-10	+91	0	0	0	0	0	0	0	0	0	0	0	0
G	0	0	0	+52	-12	+40	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	+36	-16	+20	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	+20	-20	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	-7	-7	+16	-32	-16	0	0	0	0	0	0	0	-1	-1	0	0	0
K	0	-11	-11	0	-36	-36	0	0	0	0	0	0	0	-2	-2	0	0	0
L	0	-21	-21	0	-59	-59	0	0	0	0	0	0	0	-3	-3	0	0	0
M	0	-52	-52	0	-97	-97	0	-12	-12	0	-12	-12	0	-20	-20	0	-6	-6
N	0	-46	-46	0	-79	-79	0	-17	-17	0	-17	-17	0	-16	-16	0	-10	-10
O	0	-52	-52	0	-72	-72	0	-23	-23	0	-23	-23	0	-20	-20	0	-19	-19
18			-10			-11			-5		-5	-5		-6	-6			-3
17			-9			-10			-8		-8	-8		-7	-7			-6
16			-8			-10			-9		-9	-9		-8	-8			-5
15			-7			-8			-8		-8	-8		-8	-8			-3
14			-7			-8			-4		-4	-4		-3	-3			0
13			-10			-11			+3		+3	+3		+7	+7			+12
12			+8			+2			+13		+13	+13		+14	+14			+19
11			+13			+7			+18		+18	+18		+19	+19			+21
10			+18			+13			+17		+17	+17		+17	+17			+16
9			+12			+10			+11		+11	+11		+10	+10			+11
8			+11			+10			+12		+12	+12		+13	+13			+14
7			+6			+5			+6		+6	+6		+6	+6			+6
6			+6			+6			+6		+6	+6		+6	+6			+6
5			+8			+7			+7		+7	+7		+7	+7			+6
4			+7			+7			+6		+6	+6		+6	+6			+6
3			+6			+6			+6		+6	+6		+6	+6			+6
2			+4			+3			+4		+4	+4		+4	+4			+4
1			+1			+1			+1		+1	+1		+1	+1			+1
Total			+25			+413			+40		+34	+34		+57	+57			+93

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion
	Princeton, N. J., No. 25			Hoboken, N. J., No. 26			New York, N. Y., No. 27			Worcester, Mass., No. 28			Boston, Mass., No. 29			Cambridge, Mass., No. 30		
A	+ 2	0	+ 2	+2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+40	0	+40	+8	0	+ 8	+27	0	+27	+56	0	+56	+16	0	+16	+12	0	+12
C	+16	0	+16	0	0	0	+7	0	+7	+64	0	+64	+4	0	+4	0	0	0
D	+ 6	0	+ 6	0	0	0	+ 2	0	+ 2	+31	0	+31	+ 1	0	+ 1	0	0	0
E	0	0	0	0	0	0	0	0	0	+11	0	+11	0	0	0	0	0	0
F	0	0	0	0	0	0	0	0	0	+ 7	0	+ 7	0	0	0	0	0	0
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	0	0	0	0	0	0	-10	-10	0	0	0	0	- 2	- 2
K	0	0	0	0	0	0	0	0	0	0	-13	-13	0	0	0	0	- 3	- 3
L	0	0	0	0	0	0	0	0	0	0	-14	-14	0	0	0	0	- 3	- 3
M	0	-11	-11	0	-12	-12	0	-12	-12	0	-27	-27	0	- 4	- 4	0	- 9	- 9
N	0	-16	-16	0	-18	-18	0	-18	-18	0	-25	-25	0	-12	-12	0	-15	-15
O	0	-22	-22	0	-25	-25	0	-26	-26	0	-28	-28	0	-10	-10	0	-14	-14
18			- 4			- 6			- 6			- 2			- 2			- 2
17			- 5			- 5			- 5			- 3			- 3			- 3
16			- 5			- 3			- 3			- 4			- 1			- 2
15			- 1			- 1			- 1			- 2			- 2			- 2
14			+ 1			+ 3			+ 3			- 2			- 2			- 2
13			+13			+14			+14			+ 9			+11			+10
12			+20			+22			+22			+24			+26			+25
11			+21			+21			+21			+23			+25			+25
10			+16			+16			+16			+17			+18			+18
9			+11			+11			+11			+12			+12			+12
8			+14			+15			+15			+17			+17			+17
7			+ 6			+ 6			+ 6			+ 6			+ 6			+ 6
6			+ 6			+ 6			+ 6			+ 6			+ 6			+ 6
5			+ 6			+ 6			+ 6			+ 6			+ 6			+ 6
4			+ 6			+ 6			+ 6			+ 6			+ 6			+ 6
3			+ 6			+ 6			+ 6			+ 6			+ 6			+ 6
2			+ 4			+ 4			+ 4			+ 4			+ 4			+ 4
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total			+130			+79			+106			+178			+133			+101
Calais, Me., No. 31			Ithaca, N. Y., No. 32			Cleveland, Ohio, No. 33			Cincinnati, Ohio, No. 34			Terre Haute, Ind., No. 35			Chicago, Ill., No. 36			
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+25	0	+25	+60	0	+60	+58	0	+58	+60	0	+60	+56	0	+56	+56	0	+56
C	+4	0	+4	+88	0	+88	+78	0	+78	+84	0	+84	+60	0	+60	+72	0	+72
D	+4	0	+4	+59	0	+59	+48	0	+48	+57	0	+57	+28	0	+28	+42	0	+42
E	0	0	0	+27	0	+27	+20	0	+20	+22	0	+22	+12	0	+12	+16	0	+16
F	0	0	0	+ 6	0	+ 6	+10	0	+10	0	0	0	+ 2	0	+ 2	+ 4	0	+ 4
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	-16	-16	0	-16	-16	0	-11	-11	0	- 8	- 8	0	- 7	- 7
K	0	0	0	0	-20	-20	0	-20	-20	0	-17	-17	0	-10	-10	0	- 9	- 9
L	0	0	0	0	-32	-32	0	-24	-24	0	-20	-20	0	-12	-12	0	-11	-11
M	0	- 5	- 5	0	-50	-50	0	-42	-42	0	-42	-42	0	-30	-30	0	-22	-22
N	0	- 4	- 4	0	-56	-56	0	-41	-41	0	-50	-50	0	-37	-37	0	-26	-26
O	0	-15	-15	0	-58	-58	0	-45	-45	0	-48	-48	0	-35	-35	0	-23	-23
18			- 3			- 8			- 9			- 8			- 6			- 6
17			- 3			- 8			-10			- 8			- 6			- 6
16			- 3			- 7			-10			- 8			- 6			- 7
15			- 4			- 7			-11			- 8			- 6			- 8
14			- 3			- 7			-11			- 8			- 7			- 9
13			- 3			- 6			-18			-15			-16			-16
12			+ 9			+ 7			-10			- 8			- 9			-10
11			+18			+ 8			- 5			- 3			- 7			- 4
10			+18			+11			+ 4			+ 4			- 2			- 1
9			+13			+ 8			+ 5			+ 4			+ 1			+ 1
8			+16			+12			+ 8			+ 6			+ 4			+ 6
7			+ 6			+ 6			+ 6			+ 6			+ 7			+ 7
6			+ 6			+ 6			+ 7			+ 7			+ 8			+ 8
5			+ 5			+ 7			+ 8			+ 9			+ 9			+ 9
4			+ 6			+ 6			+ 7			+ 7			+ 7			+ 7
3			+ 6			+ 6			+ 5			+ 5			+ 5			+ 5
2			+ 5			+ 4			+ 3			+ 3			+ 3			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total			+101			+49			- 2			+23			+ 8			+74

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation
	Madison, Wis., No. 37			St. Louis, Mo., No. 38			Kansas City, Mo., No. 39			Ellsworth, Kans., No. 40			Wallace, Kans., No. 41			Colorado Springs, Colo., No. 42		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+62	0	+62	+56	0	+56	+64	0	+64	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68
C	+95	0	+95	+60	0	+60	+97	0	+97	+124	0	+124	+152	0	+152	+164	0	+160
D	+70	0	+70	+30	0	+30	+72	0	+72	+140	0	+140	+252	0	+252	+312	0	+306
E	+30	0	+30	+13	0	+13	+30	0	+30	+ 82	0	+ 82	+256	0	+256	+424	0	+408
F	+10	0	+10	0	0	0	+16	0	+16	+ 40	0	+ 40	+150	0	+150	+351	0	+331
G	0	0	0	0	0	0	0	0	0	+ 12	0	+ 12	+ 84	0	+ 84	+216	0	+192
H	0	0	0	0	0	0	0	0	0	+ 16	0	+ 16	+ 48	0	+ 48	+312	0	+272
I	0	0	0	0	0	0	0	0	0	+ 20	0	+ 20	+ 60	0	+ 60	+336	0	+296
J	0	-16	-16	0	-3	-3	0	-16	-16	0	-16	-16	+ 24	-40	-16	+ 63	-74	-11
K	0	-20	-20	0	-12	-12	0	-20	-20	0	-20	-20	+ 10	-50	-40	+ 52	-123	-71
L	0	-24	-24	0	-13	-13	0	-24	-24	0	-24	-24	+ 12	-84	-72	+ 31	-178	-147
M	0	-57	-57	0	-28	-28	0	-53	-53	+ 2	-89	-87	+ 6	-217	-211	+ 30	-399	-369
N	0	-48	-48	0	-32	-32	0	-47	-47	0	-85	-85	0	-192	-192	+ 17	-359	-342
O	0	-49	-49	0	-33	-33	0	-55	-55	0	-95	-95	0	-169	-169	+ 13	-352	-339
18			- 7			- 5			-10			-19			- 36			- 68
17			- 7			- 5			-10			-19			- 36			- 69
16			- 8			- 5			-10			-19			- 36			- 69
15			- 8			- 5			-11			-19			- 37			- 68
14			- 9			- 9			-11			-20			- 39			- 62
13			-16			-16			-20			-44			- 69			- 81
12			-10			-10			-13			-26			- 38			- 48
11			- 3			- 9			-14			-19			-25			- 30
10			- 2			- 5			-14			-15			-16			- 17
9			0			- 2			- 8			- 4			- 2			0
8			+ 6			+ 2			- 1			+ 3			+ 6			+ 9
7			+ 7			+ 7			+ 8			+ 7			+ 7			+ 7
6			+ 8			+ 8			+ 9			+ 9			+ 9			+ 9
5			+ 9			+ 10			+11			+10			+10			+ 9
4			+ 7			+ 7			+ 7			+ 8			+ 8			+ 8
3			+ 5			+ 5			+ 5			+ 5			+ 5			+ 5
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total			+31			+10			-12			-40			- 5			- 68
	Pikes Peak, Colo., No. 43			Denver, Colo., No. 44			Gunnison, Colo., No. 45			Grand Junction, Colo., No. 46			Green River, Utah, No. 47			Pleasant Valley Junc- tion, Utah, No. 48		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+80	- 8	+72	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68
C	+165	- 8	+157	+164	- 4	+160	+164	- 4	+164	+164	- 4	+160	+156	0	+156	+164	- 4	+160
D	+325	-15	+310	+306	- 6	+300	+320	- 6	+321	+288	- 6	+282	+276	- 6	+270	+324	- 6	+318
E	+545	-25	+520	+392	- 8	+384	+488	-16	+472	+344	- 8	+336	+310	- 8	+302	+467	-16	+451
F	+639	-37	+602	+310	-20	+290	+450	-20	+430	+249	-10	+239	+209	-10	+199	+419	-20	+399
G	+552	-40	+512	+192	-24	+168	+309	-24	+285	+136	-16	+120	+109	-12	+ 97	+278	-24	+254
H	+498	-55	+443	+130	-32	+ 98	+240	-38	+202	+ 89	-23	+ 66	+ 72	-16	+ 56	+208	-34	+174
I	+503	-91	+412	+100	-40	+ 60	+210	-80	+130	+ 75	-42	+ 33	+ 67	-40	+ 27	+175	-74	+101
J	+298	-97	+201	+48	-48	0	+103	-81	+ 22	+ 44	-51	- 7	+ 32	-48	-16	+ 84	-80	+ 4
K	+221	-142	+ 79	+ 40	-80	-40	+ 87	-143	- 56	+ 33	-98	-65	+ 22	-73	-51	+ 91	-140	-49
L	+152	-184	-32	+ 22	-120	-98	+ 53	-221	-168	+ 24	-156	-132	+ 14	-115	-101	+ 61	-203	-142
M	+142	-432	-290	+ 21	-383	-362	+ 42	-568	-526	+ 10	-401	-391	+ 12	-341	-329	+ 49	-427	-378
N	+ 50	-384	-334	+ 13	-380	-376	+ 31	-493	-462	+ 8	-382	-374	+ 16	-311	-295	+ 17	-360	-343
O	+ 42	-371	-329	+ 18	-364	-346	+ 17	-426	-409	+ 14	-363	-349	0	-324	-324	+ 4	-319	-315
18			- 68			- 68			- 76			- 74			- 65			- 59
17			- 68			- 67			- 74			- 73			- 70			- 61
16			- 68			- 67			- 68			- 67			- 67			- 63
15			- 64			- 64			- 64			- 66			- 68			- 64
14			- 59			- 63			- 62			- 66			- 69			- 65
13			- 83			- 84			- 97			-101			-108			-104
12			- 48			- 48			-52			-55			-59			-58
11			- 30			- 30			-33			-34			-35			-35
10			- 17			- 17			-18			-15			-12			-14
9			0			0			+ 2			+ 3			+ 4			+ 4
8			+ 9			+ 9			+11			+11			+11			+11
7			+ 7			+ 7			+ 7			+ 7			+ 8			+ 7
6			+ 9			+ 9			+ 9			+ 9			+ 9			+ 9
5			+ 9			+10			+ 9			+ 9			+ 9			+ 9
4			+ 8			+ 8			+ 8			+ 8			+ 8			+ 8
3			+ 5			+ 5			+ 5			+ 5			+ 5			+ 5
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total			+1871			-148			-11			-511			-434			+238

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation
	Salt Lake City, Utah, No. 49			Grand Canyon, Wyo., No. 50			Norris Geyser Basin, Wyo., No. 51			Lower Geyser Basin, Wyo., No. 52			Seattle, Wash. (Uni- versity), No. 53			San Francisco, Cal., No. 54		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68	+ 33	0	+ 33	+ 48	0	+ 48
C	+ 160	- 4	+ 156	+ 168	- 4	+ 164	+ 168	- 4	+ 164	+ 164	- 4	+ 160	+ 12	0	+ 12	+ 35	0	+ 35
D	+ 282	- 6	+ 276	+ 333	- 6	+ 327	+ 330	- 6	+ 324	+ 324	- 6	+ 318	+ 6	0	+ 6	+ 15	0	+ 15
E	+ 333	- 8	+ 325	+ 489	- 16	+ 473	+ 480	- 16	+ 464	+ 475	- 16	+ 459	+ 1	0	+ 1	+ 1	0	+ 1
F	+ 226	- 10	+ 216	+ 449	- 20	+ 429	+ 431	- 20	+ 411	+ 423	- 20	+ 403	0	0	0	0	0	0
G	+ 125	- 16	+ 109	+ 312	- 24	+ 288	+ 288	- 24	+ 264	+ 278	- 24	+ 254	0	0	0	0	0	0
H	+ 81	- 22	+ 59	+ 242	- 43	+ 199	+ 218	- 34	+ 184	+ 208	- 32	+ 176	0	0	0	0	0	0
I	+ 62	- 43	+ 19	+ 212	- 80	+ 132	+ 190	- 75	+ 115	+ 174	- 67	+ 107	0	0	0	0	0	0
J	+ 39	- 57	- 18	+ 105	- 80	+ 25	+ 97	- 80	+ 17	+ 92	- 80	+ 12	0	0	0	0	- 2	- 2
K	+ 20	- 93	- 73	+ 101	- 140	- 39	+ 94	- 140	- 46	+ 99	- 140	- 41	0	0	0	0	- 1	- 1
L	+ 16	- 137	- 121	+ 73	- 198	- 125	+ 69	- 193	- 124	+ 62	- 188	- 126	0	- 1	- 1	0	- 7	- 7
M	+ 15	- 351	- 336	+ 53	- 473	- 420	+ 43	- 452	- 409	+ 44	- 450	- 406	0	- 19	- 19	0	- 14	- 14
N	+ 6	- 322	- 316	+ 16	- 405	- 389	+ 22	- 403	- 381	+ 36	- 415	- 379	0	- 95	- 95	0	+ 15	+ 15
O	+ 2	- 301	- 299	0	- 308	- 308	+ 13	- 316	- 303	+ 31	- 330	- 299	0	- 90	- 90	0	+ 99	+ 99
18			- 65			- 57			- 55			- 55			- 14			+ 24
17			- 64			- 60			- 59			- 58			- 11			+ 21
16			- 63			- 61			- 60			- 59			- 10			+ 20
15			- 65			- 60			- 59			- 58			- 10			+ 19
14			- 65			- 54			- 53			- 52			- 11			+ 17
13			- 107			- 86			- 84			- 83			- 21			+ 25
12			- 62			- 51			- 51			- 49			- 18			+ 23
11			- 36			- 38			- 38			- 37			- 8			+ 21
10			- 12			- 22			- 22			- 21			0			+ 14
9			+ 5			- 1			- 1			- 1			+ 4			+ 10
8			+ 11			+ 9			+ 9			+ 9			+ 10			+ 15
7			+ 7			+ 6			+ 6			+ 6			+ 6			+ 10
6			+ 9			+ 8			+ 8			+ 8			+ 7			+ 9
5			+ 9			+ 8			+ 8			+ 8			+ 8			+ 9
4			+ 8			+ 7			+ 7			+ 7			+ 7			+ 8
3			+ 6			+ 4			+ 4			+ 4			+ 3			+ 5
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 4
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			- 414			+ 382			+ 313			+ 281			- 205			+ 446

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Mount Hamilton, Cal., No. 55				Seattle, Wash. (high school), No. 56				Iron River, Mich., No. 57				Ely, Minn., No. 58			
A		+ 2	0	+ 2		+ 2	0	+ 2	1500	+ 2	0	+ 2	1470	+ 2	0	+ 2
B		+ 68	0	+ 68		+44	0	+ 44	1500	+ 64	0	+ 64	1470	+ 64	0	+ 64
C		+156	0	+156		+18	0	+ 18	1500	+124	0	+124	1470	+124	0	+124
D		+246	- 6	+240		+10	0	+ 10	1500	+138	0	+138	1470	+138	0	+138
E		+282	- 8	+274		+ 3	0	+ 3	1560	+ 80	0	+ 80	1470	+ 80	0	+ 80
F		+194	-10	+184		0	0	0	1580	+ 40	0	+ 40	1470	+ 30	0	+ 30
G		+104	-12	+ 92		0	0	0	1580	+ 12	0	+ 12	1470	+ 12	0	+ 12
H		+ 69	-16	+ 53		0	0	0	1580	+ 16	-16	0	1470	+ 16	-16	0
I		+ 53	-20	+ 33		0	0	0	1590	+ 20	-20	0	1480	+ 20	-20	0
J		+ 32	-25	+ 7		0	0	0	1580	0	-16	-16	1560	0	-16	-16
K		+ 20	-28	- 8		0	0	0	1530	0	-20	-20	1600	0	-20	-20
L		0	-18	-18		0	-1	-1	1580	0	-42	-42	1580	0	-33	-33
M		0	-24	-24		0	-19	-19	1470	0	-84	-84	1550	0	-85	-85
N		0	-16	-16		0	-95	-95	1200	0	-63	-63	1240	0	-69	-69
O		0	0	0		0	-89	-89	890	0	-50	-50	1180	0	-67	-67
18				+ 2				-14				- 6				-12
17				- 2				-11				- 6				-12
16				0				-10				- 6				-12
15				+ 2				-10				- 7				-12
14				+ 8				-11				- 7				-11
13				+22				-21				-18				-16
12				+19				-18				-12				-13
11				+20				- 8				- 9				-11
10				+15				0				- 7				-10
9				+10				+ 4				- 8				- 5
8				+15				+10				+ 8				- 1
7				+10				+ 6				+ 5				+ 5
6				+ 9				+ 7				+ 8				+ 9
5				+ 9				+ 8				+ 8				+ 9
4				+ 8				+ 7				+ 6				+ 6
3				+ 5				+ 3				+ 4				+ 4
2				+ 4				+ 3				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total				+1200				-181				+143				+ 83
	Pembina, N. Dak., No. 59				Mitchell, S. Dak., No. 60				Sweetwater, Tex., No. 61				Kerrville, Tex., No. 62			
A	796	+ 2	0	+ 2	1340	+ 2	0	+ 2	2149	+ 2	0	+ 2	1633	+ 2	0	+ 2
B	796	+60	0	+60	1340	+ 64	0	+ 64	2150	+ 68	0	+ 68	1650	+ 68	0	+ 68
C	796	+88	0	+88	1340	+116	0	+116	2150	+136	0	+136	1650	+128	0	+128
D	796	+60	0	+60	1330	+123	0	+123	2160	+191	0	+191	1667	+151	0	+151
E	796	+24	0	+24	1320	+ 65	0	+ 65	2160	+156	- 8	+148	1700	+ 92	0	+ 92
F	796	+10	0	+10	1320	+ 30	0	+ 30	2156	+ 79	-10	+ 69	1740	+ 49	- 4	+ 45
G	796	0	0	0	1330	+12	0	+ 12	2130	+ 37	-12	+ 25	1750	+ 32	-12	+ 20
H	796	0	0	0	1320	+16	-16	0	2140	+ 32	-16	+ 16	1830	+ 32	-16	+ 16
I	796	0	0	0	1320	+20	-20	0	2200	+ 20	-20	0	1835	+ 20	-20	0
J	800	0	-16	-16	1330	0	-16	-16	2260	0	-16	-16	1930	0	-16	-16
K	800	0	-20	-20	1330	0	-20	-20	2280	0	-24	-24	1912	0	-20	-20
L	800	0	-24	-24	1360	0	-28	-28	2290	0	-54	-54	1900	0	-48	-48
M	960	0	-52	-52	1410	0	-78	-78	2150	0	-123	-123	1870	0	-107	-107
N	990	0	-52	-52	1540	0	-80	-80	2000	0	-100	-100	1460	0	-76	-76
O	1100	0	-62	-62	1620	0	-89	-89	2100	0	-107	-107	1210	0	-64	-64
18				-13				-18				-24				-12
17				-13				-18				-22				-12
16				-13				-18				-21				-11
15				-13				-19				-22				-13
14				-14				-19				-22				-13
13				-25				-31				-38				-23
12				-14				-21				-21				-13
11				-13				-24				-14				-11
10				-15				-16				-11				- 8
9				- 8				-10				+ 2				+ 8
8				- 5				- 5				+ 8				+ 8
7				+ 4				+ 6				+ 9				+ 9
6				+10				+ 9				+10				+10
5				+10				+11				+10				+10
4				+ 7				+ 7				+ 9				+ 9
3				+ 3				+ 4				+ 6				+ 6
2				+ 4				+ 3				+ 8				+ 8
1				+ 1				+ 1				+ 1				+ 1
Total				-89				-57				+ 93				+133

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	El Paso, Tex., No. 63				Nogales, Ariz., No. 64				Yuma, Ariz., No. 65				Compton, Cal., No. 66			
A	3760	+ 2	0	+ 2	3874	+ 2	0	+ 2	176	+ 2	0	+ 2	69	+ 2	0	+ 2
B	3760	+ 68	0	+ 68	3874	+ 68	0	+ 68	176	+ 36	0	+ 36	70	+ 16	0	+ 16
C	3770	+ 156	0	+ 156	3874	+ 156	0	+ 156	176	+ 12	0	+ 12	70	+ 4	0	+ 4
D	3770	+ 268	- 6	+ 262	3874	+ 270	- 6	+ 264	168	+ 6	0	+ 6	69	0	0	0
E	3800	+ 292	- 8	+ 284	3900	+ 296	- 8	+ 288	162	0	0	0	69	0	0	0
F	3885	+ 187	- 10	+ 177	3930	+ 193	- 10	+ 183	155	0	0	0	74	0	0	0
G	3880	+ 98	- 12	+ 86	3910	+ 105	- 12	+ 93	140	0	0	0	86	0	0	0
H	3910	+ 61	- 16	+ 45	3960	+ 61	- 16	+ 48	151	0	0	0	91	0	0	0
I	3960	+ 60	- 40	+ 20	3980	+ 60	- 40	+ 20	159	0	0	0	81	0	0	0
J	4070	+ 32	- 48	- 16	3820	+ 32	- 48	- 16	207	0	0	0	90	0	0	0
K	4030	+ 20	- 60	- 40	3900	+ 20	- 60	- 40	298	0	- 6	- 6	134	0	0	0
L	3910	+ 24	- 96	- 72	3600	+ 14	- 86	- 72	415	0	- 12	- 12	200	0	- 5	- 5
M	4200	+ 16	- 212	- 226	2890	+ 9	- 171	- 162	430	0	- 28	- 28	390	0	- 25	- 25
N	4200	+ 6	- 216	- 210	2875	0	- 150	- 150	470	0	- 25	- 25	1010	0	- 50	- 50
O	4570	0	- 221	- 221	2920	0	- 148	- 148	932	0	- 48	- 48	1130	0	- 60	- 60
18				- 46				- 30				- 17				- 10
17				- 45				- 24				- 17				- 8
16				- 44				- 24				- 18				0
15				- 48				- 28				- 18				+ 6
14				- 49				- 28				- 20				+ 7
13				- 75				- 49				- 15				+ 18
12				- 32				- 27				- 9				+ 14
11				- 23				- 12				+ 3				+ 9
10				- 7				0				+ 3				+ 13
9				+ 3				+ 6				+ 10				+ 11
8				+ 14				+ 15				+ 16				+ 16
7				+ 5				+ 8				+ 10				+ 11
6				+ 10				+ 9				+ 9				+ 9
5				+ 10				+ 9				+ 9				+ 9
4				+ 9				+ 8				+ 8				+ 8
3				+ 6				+ 5				+ 5				+ 5
2				+ 5				+ 4				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total...				+ 7				+ 377				- 99				+ 5
	Goldfield, Nev., No. 67				Yavapai, Ariz., No. 68				Grand Canyon, Ariz., No. 69				Gallup, N. Mex., No. 70			
A	5629	+ 2	0	+ 2	7150	+ 2	0	+ 2	2784	+ 2	0	+ 2	6196	+ 2	0	+ 2
B	5700	+ 68	0	+ 68	7150	+ 68	0	+ 68	2784	+ 68	0	+ 68	6196	+ 68	0	+ 68
C	5690	+ 164	- 4	+ 160	6800	+ 126	- 4	+ 122	2875	+ 148	0	+ 148	6196	+ 164	- 4	+ 160
D	5688	+ 301	- 6	+ 295	6410	+ 267	- 6	+ 261	3100	+ 190	- 5	+ 185	6196	+ 318	- 6	+ 312
E	5700	+ 406	- 12	+ 394	5850	+ 391	- 12	+ 379	3510	+ 182	- 8	+ 174	6600	+ 440	- 16	+ 424
F	5810	+ 328	- 20	+ 308	5210	+ 339	- 15	+ 324	3800	+ 92	- 10	+ 82	6690	+ 390	- 20	+ 370
G	5970	+ 195	- 24	+ 171	5590	+ 247	- 20	+ 227	4410	+ 37	- 16	+ 21	6720	+ 242	- 24	+ 218
H	5970	+ 147	- 32	+ 115	5320	+ 177	- 25	+ 152	4820	+ 11	- 23	- 12	6720	+ 175	- 32	+ 143
I	5975	+ 113	- 52	+ 61	5110	+ 158	- 49	+ 109	5170	+ 7	- 48	- 41	6760	+ 148	- 60	+ 88
J	5990	+ 51	- 62	- 11	5510	+ 85	- 60	+ 25	5500	+ 15	- 61	- 46	6850	+ 83	- 79	+ 4
K	5610	+ 51	- 91	- 40	6210	+ 79	- 105	- 26	6390	- 6	- 106	- 112	6960	+ 75	- 120	- 45
L	5400	+ 29	- 125	- 96	6160	+ 49	- 156	- 107	6280	- 5	- 149	- 154	7050	+ 48	- 169	- 121
M	5900	0	- 313	- 313	5930	+ 51	- 345	- 294	6150	+ 2	- 359	- 357	7190	+ 34	- 417	- 383
N	5480	+ 16	- 293	- 277	5970	+ 17	- 306	- 289	5950	+ 7	- 306	- 299	6820	+ 16	- 359	- 343
O	6210	+ 1	- 302	- 301	5200	+ 9	- 265	- 256	5200	+ 9	- 265	- 256	6410	+ 9	- 321	- 312
18				- 61				- 56				- 56				- 63
17				- 56				- 53				- 53				- 63
16				- 51				- 48				- 48				- 65
15				- 41				- 48				- 48				- 69
14				- 40				- 50				- 50				- 63
13				- 61				- 81				- 81				- 91
12				- 20				- 56				- 56				- 47
11				- 4				- 25				- 25				- 32
10				+ 5				- 4				- 4				- 9
9				+ 8				+ 6				+ 0				+ 4
8				+ 12				+ 12				+ 12				+ 12
7				+ 9				+ 8				+ 8				+ 7
6				+ 9				+ 9				+ 9				+ 9
5				+ 9				+ 9				+ 9				+ 9
4				+ 8				+ 8				+ 8				+ 8
3				+ 5				+ 5				+ 5				+ 5
2				+ 4				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total...				+ 272				+ 337				- 957				+ 141

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Las Vegas, N. Mex., No. 71				Shamrock, Tex., No. 72				Denison, Tex., No. 73				Minneapolis, Minn., No. 74			
A	6429	+ 2	0	+ 2	2300	+ 2	0	+ 2	754	+ 2	0	+ 2	840	+ 2	0	+ 2
B	6429	+ 68	0	+ 68	2300	+ 68	0	+ 68	754	+ 60	0	+ 60	840	+ 60	0	+ 60
C	6429	+ 114	- 4	+ 110	2300	+ 140	0	+ 140	740	+ 84	0	+ 84	840	+ 92	0	+ 92
D	6429	+ 318	- 6	+ 312	2300	+ 198	0	+ 198	740	+ 54	0	+ 54	830	+ 64	0	+ 64
E	6400	+ 440	- 16	+ 424	2300	+ 168	- 8	+ 160	730	+ 24	0	+ 24	820	+ 24	0	+ 24
F	6460	+ 381	- 20	+ 361	2300	+ 90	- 10	+ 80	690	+ 10	0	+ 10	840	+ 10	0	+ 10
G	6530	+ 241	- 24	+ 217	2300	+ 48	- 12	+ 36	690	0	0	0	830	0	0	0
H	6560	+ 109	- 32	+ 137	2300	+ 32	- 16	+ 16	690	0	0	0	830	0	0	0
I	6680	+ 148	- 60	+ 88	2350	+ 20	- 20	0	650	0	0	0	880	0	0	0
J	6800	+ 85	- 79	+ 6	2390	+ 4	- 20	- 16	690	0	- 16	- 16	880	0	- 16	- 16
K	6850	+ 78	- 120	- 42	2425	+ 13	- 40	- 27	670	0	- 20	- 20	900	0	- 20	- 20
L	7100	+ 43	- 171	- 128	2420	+ 4	- 56	- 52	700	0	- 24	- 24	920	0	- 24	- 24
M	7100	+ 35	- 412	- 377	2300	0	- 128	- 128	680	0	- 37	- 37	990	0	- 56	- 56
N	6650	+ 21	- 350	- 329	2260	0	- 115	- 115	710	0	- 42	- 42	1000	0	- 48	- 48
O	6140	+ 12	- 309	- 297	2410	0	- 122	- 122	760	0	- 45	- 45	1040	0	- 56	- 56
18				- 62				- 24				- 9				- 12
17				- 62				- 24				- 9				- 12
16				- 62				- 24				- 9				- 12
15				- 59				- 24				- 9				- 13
14				- 61				- 25				- 9				- 13
13				- 80				- 44				- 20				- 21
12				- 43				- 25				- 13				- 16
11				- 26				- 17				- 11				- 12
10				- 18				- 14				- 12				- 9
9				- 1				- 1				- 3				- 5
8				+ 9				+ 6				+ 3				0
7				+ 7				+ 8				+ 8				+ 6
6				+ 9				+ 10				+ 10				+ 9
5				+ 10				+ 10				+ 11				+ 10
4				+ 8				+ 9				+ 8				+ 6
3				+ 5				+ 6				+ 5				+ 4
2				+ 3				+ 2				+ 3				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total				+ 171				+ 70				- 6				- 52
	Lead, S. Dak., No. 75				Bismarck, N. Dak., No. 76				Hinsdale, Mont., No. 77				Sand Point, Idaho, No. 78			
A	5216	+ 2	0	+ 2	1690	+ 2	0	+ 2	2170	+ 2	0	+ 2	2090	+ 2	0	+ 2
B	5200	+ 64	0	+ 64	1690	+ 68	0	+ 68	2170	+ 68	0	+ 68	2090	+ 68	0	+ 68
C	5200	+ 164	- 4	+ 160	1690	+ 128	0	+ 128	2160	+ 140	0	+ 140	2100	+ 136	0	+ 136
D	5200	+ 300	- 6	+ 294	1700	+ 156	0	+ 156	2160	+ 190	0	+ 190	2100	+ 186	0	+ 186
E	5290	+ 386	- 8	+ 378	1700	+ 98	0	+ 98	2170	+ 155	- 8	+ 147	2080	+ 148	- 8	+ 140
F	5300	+ 296	- 20	+ 276	1720	+ 49	- 5	+ 44	2210	+ 80	- 10	+ 70	2050	+ 73	- 10	+ 63
G	5420	+ 182	- 24	+ 158	1730	+ 24	- 6	+ 18	2270	+ 38	- 12	+ 26	2080	+ 36	- 12	+ 24
H	5550	+ 131	- 32	+ 99	1710	+ 22	- 16	+ 6	2230	+ 17	- 16	+ 1	2230	+ 26	- 16	+ 10
I	5600	+ 83	- 40	+ 43	1730	+ 20	- 20	0	2350	+ 20	- 20	0	2510	+ 15	- 20	- 5
J	5260	+ 45	- 48	- 3	1780	0	- 16	- 16	2360	0	- 16	- 16	2720	+ 16	- 32	- 16
K	5040	+ 45	- 80	- 35	1820	0	- 20	- 20	2320	0	- 25	- 25	2900	0	- 43	- 43
L	4840	+ 32	- 120	- 88	1880	0	- 48	- 48	2390	0	- 54	- 54	3100	+ 1	- 72	- 71
M	4400	+ 27	- 260	- 233	2000	0	- 112	- 112	2650	0	- 149	- 149	3890	+ 11	- 238	- 227
N	3890	0	- 199	- 199	2010	0	- 96	- 96	2790	0	- 145	- 145	3970	0	- 204	- 204
O	3610	0	- 174	- 174	2020	0	- 105	- 105	2890	0	- 135	- 135	4110	0	- 205	- 205
18				- 36				- 20				- 31				- 42
17				- 37				- 20				- 31				- 42
16				- 37				- 19				- 31				- 40
15				- 39				- 20				- 32				- 40
14				- 40				- 20				- 33				- 40
13				- 61				- 38				- 66				- 70
12				- 35				- 26				- 40				- 39
11				- 30				- 23				- 30				- 21
10				- 19				- 17				- 21				- 11
9				- 6				- 10				- 13				0
8				+ 1				- 3				+ 2				+ 7
7				+ 6				+ 5				+ 5				+ 6
6				+ 9				+ 10				+ 10				+ 8
5				+ 10				+ 10				+ 9				+ 8
4				+ 7				+ 7				+ 7				+ 7
3				+ 4				+ 4				+ 3				+ 3
2				+ 3				+ 3				+ 4				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total				+ 443				- 54				- 167				- 444

Inner radius, 1280 meters; outer radius, 1680 meters. Ten compartments.)

[illegible]

Inner radius, 1680 meters; outer radius, 2280 meters. Ten compartments.)

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**Chapter II.—CORRECTIONS FOR TOPOGRAPHY AND ISOSTATIC COMPENSATION AND
PRINCIPAL FACTS FOR GRAVITY STATIONS.**

**MEAN ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND ISOSTATIC COMPENSATION FOR
SEPARATE ZONES AT STATIONS IN THE UNITED STATES.**

There are given in the following tables (pp. 20 to 45) the combined effect of the topography and compensation for all zones and the separate effects of the topography and the compensation for each of the lettered zones for the 219 stations in the United States. In addition, there is given the mean elevation of the topography for each of the lettered zones for all of the stations from No. 57 to No. 219. No record of the elevation of the topography for the separate zones was made for the first 56 stations, when the topography and compensation effects were computed, and it was not deemed expedient to read the maps again to obtain that information for publication here. With the combined effect of topography and compensation given for separate zones at the first 56 stations one may get from the tables an approximate value of the elevation of the topography for the zones. The values of the effects of topography and compensation, separately and combined, are expressed in the fourth decimal place in dynes. Values resulting from interpolation from surrounding stations are indicated by italic type. (For explanation of process of interpolation, see pp. 58–65 of Special Publication No. 10.) The following table gives the radii of the zones and the number of compartments in each of them:

Designation of zone	Inner radius of zone	Outer radius of zone	Compartments
	<i>Meters</i>	<i>Meters</i>	
A	0	2	1
B	2	68	4
C	68	230	4
D	230	590	6
E	590	1 280	8
F	1 280	2 290	10
G	2 290	3 520	12
H	3 520	5 240	16
I	5 240	8 440	20
J	8 440	12 400	16
K	12 400	18 800	20
L	18 800	28 800	24
M	28 800	58 800	14
N	58 800	99 000	16
O	99 000	166 700	28
	° / "	° / "	
18	1 29 58	1 41 13	1
17	1 41 13	1 54 52	1
16	1 54 52	2 11 53	1
15	2 11 53	2 33 46	1
14	2 33 46	3 03 05	1
13	3 03 05	4 19 13	16
12	4 19 13	5 46 34	10
11	5 46 34	7 51 30	8
10	7 51 30	10 44	6
9	10 44	14 09	4
8	14 09	20 41	4
7	20 41	26 41	2
6	26 41	35 58	18
5	35 58	51 04	16
4	51 04	72 13	12
3	72 13	105 48	10
2	105 48	150 56	6
1	150 56	180	1

Corrections for topography and isostatic compensation, separate zones, for United States stations.

Zone	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion
	Key West, Fla., No. 1			West Palm Beach, Fla., No. 2			Punta Gorda, Fla., No. 3			Apalachicola, Fla., No. 4			New Orleans, La., No. 5			Rayville, La., No. 6		
A	+1	0	+ 1	+2	0	+ 2	+1	0	+ 1	+2	0	+ 2	+1	0	+ 1	+ 2	0	+ 2
B	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	+20	0	+20
C	-1	0	- 1	0	0	0	0	0	0	0	0	0	0	0	0	+ 4	0	+ 4
D	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	+ 6	0	+ 6
E	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
F	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
K	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
L	0	0	0	0	+ 5	+ 5	0	0	0	0	0	0	0	0	0	0	0	0
M	0	+14	+14	0	+20	+20	0	0	0	0	0	0	0	0	0	0	0	0
N	0	+42	+42	0	+24	+24	0	0	0	0	0	0	0	0	0	0	0	0
O	0	+55	+55	0	+16	+16	0	0	0	0	+6	+ 6	0	0	0	0	0	0
18			+ 8			+ 4			0			+ 2			+ 2			- 1
17			+ 4			+ 5			+ 1			+ 3			+ 2			- 1
16			+ 3			+ 5			+ 2			+ 4			+ 5			- 1
15			+ 5			+ 5			+ 6			+ 9			+ 7			- 2
14			+ 8			+ 9			+10			+11			+11			- 3
13			+38			+33			+30			+17			+24			+ 5
12			+38			+39			+31			+11			+22			+ 5
11			+42			+45			+33			+ 9			+ 7			0
10			+25			+27			+22			+14			+ 3			- 1
9			+15			+16			+14			+12			- 2			- 3
8			+15			+15			+13			+10			+ 5			+ 3
7			+ 5			+ 5			+ 6			+ 6			+ 7			+ 8
6			+ 6			+ 6			+ 6			+ 8			+10			+ 9
5			+10			+10			+10			+10			+10			+11
4			+ 8			+ 8			+ 8			+ 7			+ 8			+ 7
3			+ 6			+ 6			+ 6			+ 6			+ 6			+ 5
2			+ 2			+ 2			+ 3			+ 3			+ 3			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			+350			+306			+201			+151			+132			+77

	Galveston, Tex., No. 7			Point Isabel, Tex., No. 8			Laredo, Tex., No. 9			Austin, Tex. (Capitol), No. 10			Austin, Tex. (Uni- versity), No. 11			McAlester, Okla., No. 12		
A	+2	0	+ 2	+2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	0	0	0	+4	0	+ 4	+56	0	+56	+56	0	+56	+56	0	+56	+60	0	+60
C	0	0	0	0	0	0	+50	0	+50	+64	0	+64	+72	0	+72	+87	0	+87
D	0	0	0	0	0	0	+21	0	+21	+34	0	+34	+40	0	+40	+52	0	+52
E	0	0	0	0	0	0	+ 8	0	+ 8	+15	0	+15	+16	0	+16	+21	0	+21
F	0	0	0	0	0	0	0	0	0	+ 2	0	+ 2	+ 6	0	+ 6	+10	0	+10
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	0	0	0	0	0	-14	-14	0	-14	-14	0	-13	-13	-13
K	0	0	0	0	0	0	0	- 4	- 4	0	-18	-18	0	-18	-18	0	-16	-16
L	0	0	0	0	0	0	0	-10	-10	0	-22	-22	0	-22	-22	0	-22	-22
M	0	0	0	0	0	0	0	-24	-24	0	-41	-41	0	-41	-41	0	-46	-46
N	0	0	0	0	- 1	- 1	0	-26	-26	0	-43	-43	0	-43	-43	0	-35	-35
O	0	0	0	0	+27	+27	0	-21	-21	0	-44	-44	0	-44	-44	0	-40	-40
18			0			+10			- 5			- 8			- 8			- 8
17			+ 2			+12			- 6			- 8			- 8			- 8
16			+ 3			+13			- 7			- 7			- 7			- 9
15			+ 4			+15			-10			- 7			- 7			- 9
14			+ 6			+14			- 8			- 7			- 7			- 9
13			+ 6			+12			-21			-12			-12			-15
12			+ 4			- 1			-10			- 9			- 9			-13
11			- 2			- 9			-12			- 7			- 7			-12
10			- 5			- 5			- 4			-11			-11			-12
9			+ 1			+ 5			+ 4			+ 1			+ 1			- 4
8			+ 7			+ 9			+10			+ 7			+ 7			+ 8
7			+ 8			+ 9			+ 9			+ 9			+ 9			+ 8
6			+10			+10			+10			+10			+10			+ 9
5			+10			+10			+10			+10			+10			+11
4			+ 9			+ 9			+ 9			+ 9			+ 9			+ 8
3			+ 6			+ 6			+ 6			+ 6			+ 6			+ 5
2			+ 2			+ 2			+ 2			+ 2			+ 2			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			+74			+154			+30			-30			-11			+ 8

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation
	Little Rock, Ark., No. 13			Columbia, Tenn., No. 14			Atlanta, Ga., No. 15			McCormick, S. C., No. 16			Charleston, S. C., No. 17			Beaufort, N. C., No. 18		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 1	0	+ 1
B	+48	0	+48	+60	0	+60	+64	0	+64	+56	0	+56	+4	0	+4	0	0	0
C	+31	0	+31	+78	0	+78	+104	0	+104	+64	0	+64	0	0	0	0	0	0
D	+12	0	+12	+48	0	+48	+90	0	+90	+30	0	+30	0	0	0	0	0	0
E	+ 5	0	+ 5	+19	0	+19	+40	0	+40	+13	0	+13	0	0	0	0	0	0
F	0	0	0	+ 7	0	+ 7	+19	0	+19	0	0	0	0	0	0	0	0	0
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	-12	-12	0	-16	-16	0	-2	-2	0	0	0	0	0	0
K	0	-1	-1	0	-16	-16	0	-20	-20	0	-5	-5	0	0	0	0	0	0
L	0	0	0	0	-17	-17	0	-24	-24	0	-7	-7	0	0	0	0	0	0
M	0	-20	-20	0	-34	-34	0	-50	-50	0	-28	-28	0	0	0	0	0	0
N	0	-30	-30	0	-39	-39	0	-44	-44	0	-31	-31	0	-1	-1	0	+4	+4
O	0	-29	-29	0	-42	-42	0	-49	-49	0	-37	-37	0	+2	+2	0	+45	+45
18			- 5			- 7			- 9			- 7			+ 2			+14
17			- 5			- 7			- 9			- 8			+ 2			+16
16			- 5			- 6			- 9			- 8			+ 2			+20
15			- 5			- 6			- 7			- 3			+ 3			+27
14			- 5			- 7			- 6			- 3			+ 4			+34
13			- 8			-10			- 7			- 1			+12			+52
12			- 7			- 7			- 1			+ 7			+21			+36
11			- 5			0			+ 6			+13			+24			+29
10			- 2			+ 6			+14			+17			+21			+19
9			- 5			+ 3			+ 9			+10			+12			+14
8			+ 8			+ 4			+ 6			+ 8			+12			+14
7			+ 8			+ 6			+ 6			+ 6			+ 5			+ 5
6			+ 9			+ 7			+ 7			+ 7			+ 6			+ 6
5			+11			+10			+10			+10			+ 9			+ 8
4			+ 7			+ 7			+ 7			+ 7			+ 7			+ 7
3			+ 5			+ 6			+ 6			+ 6			+ 6			+ 6
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			+12			+59			+142			+120			+159			+361
	Charlottesville, Va., No. 19			Deer Park, Md., No. 20			Washington, D. C., C. and G. S. Office, No. 21			Washington, D. C., Smithsonian Insti- tution, No. 22			Baltimore, Md., No. 23			Philadelphia, Pa., No. 24		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+56	0	+56	+68	0	+68	+12	0	+12	+8	0	+8	+24	0	+24	+12	0	+12
C	+62	0	+62	+144	0	+144	+2	0	+2	0	0	0	+4	0	+4	+4	0	+4
D	+33	0	+33	+209	0	+209	0	0	0	0	0	0	+6	0	+6	0	0	0
E	+11	0	+11	+186	- 8	+178	0	0	0	0	0	0	0	0	0	0	0	0
F	+ 3	0	+ 3	+101	-10	+ 91	0	0	0	0	0	0	0	0	0	0	0	0
G	0	0	0	+52	-12	+40	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	+38	-16	+20	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	+20	-20	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	-7	-7	+16	-32	-16	0	0	0	0	0	0	0	-1	-1	0	0	0
K	0	-11	-11	0	-36	-36	0	0	0	0	0	0	0	-2	-2	0	0	0
L	0	-21	-21	0	-59	-59	0	0	0	0	0	0	0	-3	-3	0	0	0
M	0	-52	-52	0	-97	-97	0	-12	-12	0	-12	-12	0	-20	-20	0	-6	-6
N	0	-46	-46	0	-79	-79	0	-17	-17	0	-17	-17	0	-16	-16	0	-10	-10
O	0	-52	-52	0	-72	-72	0	-23	-23	0	-23	-23	0	-20	-20	0	-19	-19
18			-10			-11			- 5			- 5			- 6			- 3
17			- 9			-10			- 8			- 8			- 7			- 6
16			- 8			-10			- 9			- 9			- 9			- 8
15			- 7			- 8			- 8			- 8			- 8			- 3
14			- 7			- 8			- 4			- 4			- 3			0
13			-10			-11			+ 3			+ 3			+ 7			+12
12			+ 8			+13			+13			+13			+14			+19
11			+13			+17			+18			+18			+19			+21
10			+18			+13			+17			+17			+17			+16
9			+12			+10			+11			+11			+10			+11
8			+11			+10			+12			+12			+13			+14
7			+ 5			+ 6			+ 6			+ 6			+ 6			+ 6
6			+ 6			+ 6			+ 6			+ 6			+ 6			+ 6
5			+ 8			+ 7			+ 7			+ 7			+ 7			+ 6
4			+ 7			+ 7			+ 6			+ 6			+ 6			+ 6
3			+ 6			+ 6			+ 6			+ 6			+ 6			+ 6
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 4
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			+25			+413			+40			+34			+57			+93

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion
	Princeton, N. J., No. 25			Hoboken, N. J., No. 26			New York, N. Y., No. 27			Worcester, Mass., No. 28			Boston, Mass., No. 29			Cambridge, Mass., No. 30		
A	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2
B	+40	0	+40	+8	0	+8	+27	0	+27	+56	0	+56	+16	0	+16	+12	0	+12
C	+16	0	+16	0	0	0	+7	0	+7	+64	0	+64	+4	0	+4	0	0	0
D	+6	0	+6	0	0	0	+2	0	+2	+31	0	+31	+1	0	+1	0	0	0
E	0	0	0	0	0	0	0	0	0	+11	0	+11	0	0	0	0	0	0
F	0	0	0	0	0	0	0	0	0	+7	0	+7	0	0	0	0	0	0
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	0	0	0	0	0	-10	-10	0	0	0	0	-2	-2	0
K	0	0	0	0	0	0	0	0	0	-13	-13	0	0	0	0	-3	-3	0
L	0	0	0	0	0	0	0	0	0	-14	-14	0	0	0	0	-3	-3	0
M	-11	-11	-11	-12	-12	-12	-12	-12	-12	-27	-27	0	-4	-4	-4	-9	-9	-9
N	0	-16	-16	0	-18	-18	0	-18	-18	0	-25	-25	0	-12	-12	0	-15	-15
O	0	-22	-22	0	-25	-25	0	-26	-26	0	-28	-28	0	-10	-10	0	-14	-14
18			-4			-6			-6			-2			-2			-2
17			-6			-5			-5			-3			-1			-1
16			-5			-3			-3			-4			1			2
15			-1			+1			+1			-2			-2			-2
14			+1			+3			+3			-2			-2			-2
13			+15			+14			+14			+9			+11			+10
12			+20			+22			+22			+24			+26			+25
11			+21			+21			+21			+23			+25			+25
10			+16			+16			+16			+17			+18			+18
9			+11			+11			+11			+12			+12			+12
8			+14			+15			+15			+17			+17			+17
7			+6			+6			+6			+6			+6			+6
6			+6			+6			+6			+6			+6			+6
5			+6			+6			+6			+6			+6			+6
4			+6			+6			+6			+6			+6			+6
3			+6			+6			+6			+6			+6			+6
2			+4			+4			+4			+4			+4			+4
1			+1			+1			+1			+1			+1			+1
Total			+130			+79			+106			+178			+133			+101
	Calais, Me., No. 31			Ithaca, N. Y., No. 32			Cleveland, Ohio, No. 33			Cincinnati, Ohio, No. 34			Terre Haute, Ind., No. 35			Chicago, Ill., No. 36		
	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion	Topog- raphy	Com- pen- sa- tion	Topog- raphy and com- pen- sa- tion
A	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2	+2	0	+2
B	+25	0	+25	+60	0	+60	+58	0	+58	+60	0	+60	+56	0	+56	+56	0	+56
C	+4	0	+4	+88	0	+88	+78	0	+78	+84	0	+84	+60	0	+60	+72	0	+72
D	+4	0	+4	+59	0	+59	+48	0	+48	+57	0	+57	+28	0	+28	+42	0	+42
E	0	0	0	+27	0	+27	+20	0	+20	+22	0	+22	+12	0	+12	+16	0	+16
F	0	0	0	+6	0	+6	+10	0	+10	0	0	0	+2	0	+2	+4	0	+4
G	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
H	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
I	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
J	0	0	0	0	-16	-16	0	-16	-16	0	-11	-11	0	-8	-8	0	-7	-7
K	0	0	0	0	-20	-20	0	-20	-20	0	-17	-17	0	-10	-10	0	-9	-9
L	0	0	0	0	-32	-32	0	-24	-24	0	-20	-20	0	-12	-12	0	-11	-11
M	0	-5	-5	0	-50	-50	0	-42	-42	0	-42	-42	0	-30	-30	0	-22	-22
N	0	-4	-4	0	-56	-56	0	-41	-41	0	-50	-50	0	-37	-37	0	-26	-26
O	0	-15	-15	0	-58	-58	0	-45	-45	0	-48	-48	0	-35	-35	0	-23	-23
18			-3			-8			-9			-8			-6			-6
17			-3			-8			-10			-8			-6			-6
16			-3			-7			-10			-8			-6			-7
15			-4			-7			-11			-8			-6			-8
14			-3			-7			-11			-8			-7			-9
13			-3			-6			-18			-15			-16			-16
12			+9			+7			-10			-8			-9			-10
11			+18			+8			-5			-3			-7			-4
10			+18			+11			+4			+4			-2			-1
9			+13			+8			+5			+4			+1			+1
8			+16			+12			+8			+6			+4			+6
7			+6			+6			+6			+6			+7			+7
6			+6			+6			+7			+7			+8			+8
5			+5			+7			+8			+9			+9			+9
4			+6			+6			+7			+7			+7			+7
3			+6			+6			+5			+5			+5			+5
2			+5			+4			+3			+3			+3			+3
1			+1			+1			+1			+1			+1			+1
Total			+101			+49			-2			+23			+8			+74

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation
	Madison, Wis., No. 37			St. Louis, Mo., No. 38			Kansas City, Mo., No. 39			Ellsworth, Kans., No. 40			Wallace, Kans., No. 41			Colorado Springs, Colo., No. 42		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+62	0	+62	+62	0	+62	+64	0	+64	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68
C	+95	0	+95	+60	0	+60	+97	0	+97	+124	0	+124	+152	0	+152	+164	0	+160
D	+70	0	+70	+30	0	+30	+72	0	+72	+140	0	+140	+252	0	+252	+312	0	+306
E	+30	0	+30	+13	0	+13	+30	0	+30	+ 82	0	+ 82	+250	0	+250	+424	0	+408
F	+10	0	+10	0	0	0	+16	0	+16	+ 40	0	+ 40	+150	0	+150	+351	0	+331
G	0	0	0	0	0	0	0	0	0	+ 12	0	+ 12	+ 84	0	+ 84	+216	0	+192
H	0	0	0	0	0	0	0	0	0	+ 16	0	+ 16	+ 48	0	+ 48	+150	0	+127
I	0	0	0	0	0	0	0	0	0	+ 20	0	+ 20	+ 60	0	+ 60	+138	0	+ 78
J	0	-16	-16	0	-3	-3	0	-16	-16	0	-16	-16	+ 24	-40	-16	+ 63	-74	-11
K	0	-20	-20	0	-12	-12	0	-20	-20	0	-20	-20	+ 10	-50	-40	+ 52	-123	-71
L	0	-24	-24	0	-13	-13	0	-24	-24	0	-47	-47	+ 12	-84	-72	+ 31	-178	-147
M	0	-57	-57	0	-28	-28	0	-53	-53	+ 2	-89	-87	+ 6	-217	-211	+ 30	-399	-369
N	0	-48	-48	0	-32	-32	0	-47	-47	0	-85	-85	0	-192	-192	+ 17	-359	-342
O	0	-49	-49	0	-33	-33	0	-55	-55	0	-95	-95	0	-169	-169	+ 13	-352	-339
18			- 7			- 5			-10			-19			-36			- 68
17			- 7			- 5			-10			-19			-36			- 69
16			- 8			- 5			-10			-19			-36			- 69
15			- 8			- 7			-11			-19			-37			- 68
14			- 9			- 9			-11			-20			-39			- 62
13			-16			-16			-20			-44			-69			- 81
12			-10			-10			-13			-26			-38			- 48
11			- 5			- 9			-14			-19			-25			- 30
10			- 2			- 5			-14			-15			-16			- 17
9			0			- 2			- 8			- 4			- 2			0
8			+ 6			+ 2			- 1			+ 3			+ 6			+ 9
7			+ 7			+ 7			+ 8			+ 7			+ 7			+ 7
6			+ 8			+ 8			+ 9			+ 9			+ 9			+ 9
5			+ 9			+10			+11			+10			+11			+ 9
4			+ 7			+ 7			+ 7			+ 8			+ 8			+ 8
3			+ 5			+ 5			+ 5			+ 5			+ 5			+ 5
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			+31			+10			-12			-40			- 5			- 68
	Pikes Peak, Colo., No. 43			Denver, Colo., No. 44			Gunnison, Colo., No. 45			Grand Junction, Colo., No. 46			Green River, Utah, No. 47			Pleasant Valley Junction, Utah, No. 48		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+80	0	+80	+68	0	+68	+68	0	+68	+68	0	+68	+68	0	+68	+68	0	+68
C	+165	0	+165	+164	0	+164	+168	0	+168	+164	0	+164	+156	0	+156	+164	0	+160
D	+325	0	+325	+306	0	+306	+330	0	+330	+288	0	+288	+276	0	+276	+324	0	+318
E	+545	0	+545	+392	0	+392	+488	0	+488	+344	0	+344	+310	0	+310	+467	0	+451
F	+639	0	+639	+310	0	+310	+450	0	+450	+249	0	+249	+209	0	+209	+419	0	+399
G	+552	0	+552	+192	0	+192	+309	0	+309	+136	0	+136	+109	0	+109	+278	0	+254
H	+498	0	+498	+130	0	+130	+240	0	+240	+ 89	0	+ 89	+ 66	0	+ 66	+208	0	+174
I	+503	0	+503	+100	0	+100	+210	0	+210	+ 75	0	+ 75	+ 42	0	+ 42	+175	0	+141
J	+298	0	+298	+ 48	0	+ 48	+103	0	+103	+ 44	0	+ 44	+ 32	0	+ 32	+ 84	0	+ 4
K	+221	0	+221	+ 40	0	+ 40	+ 87	0	+ 87	+ 33	0	+ 33	+ 22	0	+ 22	+ 51	0	+ 29
L	+152	0	+152	+ 22	0	+ 22	+ 53	0	+ 53	+ 24	0	+ 24	+ 14	0	+ 14	+101	0	+142
M	+142	0	+142	+290	0	+290	+362	0	+362	+10	0	+10	+12	0	+12	+329	0	+378
N	+50	0	+50	+13	0	+13	+31	0	+31	+ 8	0	+ 8	+16	0	+16	+295	0	+343
O	+42	0	+42	+18	0	+18	+17	0	+17	+14	0	+14	0	0	0	+ 4	0	+315
18			- 68			- 68			- 76			- 74			- 65			- 59
17			- 68			- 67			- 74			- 73			- 70			- 61
16			- 68			- 67			- 74			- 73			- 70			- 63
15			- 64			- 64			- 64			- 66			- 68			- 64
14			- 59			- 63			- 62			- 65			- 69			- 65
13			- 83			- 84			- 97			-101			-108			-104
12			- 48			- 48			- 52			- 55			- 59			- 58
11			- 30			- 30			- 33			- 34			- 35			- 35
10			- 17			- 17			- 18			- 15			- 12			- 14
9			0			0			+ 2			+ 3			+ 4			+ 4
8			+ 9			+ 9			+11			+11			+11			+11
7			+ 7			+ 7			+ 7			+ 7			+ 8			+ 7
6			+ 9			+ 9			+ 9			+ 9			+ 9			+ 9
5			+ 8			+10			+ 9			+ 9			+ 9			+ 9
4			+ 8			+ 8			+ 8			+ 8			+ 8			+ 8
3			+ 5			+ 5			+ 5			+ 5			+ 5			+ 5
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 3
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			+1871			-148			- 11			-511			-434			+238

Corrections for topography and isostatic compensation, separate zones, for United States stations—Continued.

Zone	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation
	Salt Lake City, Utah, No. 49			Grand Canyon, Wyo., No. 50			Norris Geyser Basin, Wyo., No. 51			Lower Geyser Basin, Wyo., No. 52			Seattle, Wash. (Uni- versity), No. 53			San Francisco, Cal., No. 54		
A	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2	+ 2	0	+ 2
B	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68	+ 68	0	+ 68	+ 33	0	+ 33	+ 48	0	+ 48
C	+ 160	- 4	+ 156	+ 168	- 4	+ 164	+ 168	- 4	+ 164	+ 164	- 4	+ 160	+ 12	0	+ 12	+ 35	0	+ 35
D	+ 282	- 6	+ 276	+ 333	- 6	+ 327	+ 330	- 6	+ 324	+ 324	- 6	+ 318	+ 6	0	+ 6	+ 15	0	+ 15
E	+ 333	- 8	+ 325	+ 489	- 16	+ 473	+ 480	- 16	+ 464	+ 475	- 16	+ 459	+ 1	0	+ 1	+ 1	0	+ 1
F	+ 226	- 10	+ 216	+ 449	- 20	+ 429	+ 431	- 20	+ 411	+ 423	- 20	+ 403	0	0	0	0	0	0
G	+ 125	- 16	+ 109	+ 312	- 24	+ 288	+ 288	- 24	+ 264	+ 278	- 24	+ 254	0	0	0	0	0	0
H	+ 81	- 22	+ 59	+ 242	- 43	+ 199	+ 218	- 34	+ 184	+ 208	- 32	+ 176	0	0	0	0	0	0
I	+ 62	- 43	+ 19	+ 212	- 80	+ 132	+ 190	- 75	+ 115	+ 174	- 67	+ 107	0	0	0	0	0	0
J	+ 39	- 57	+ 18	+ 105	- 80	+ 25	+ 97	- 80	+ 17	+ 92	- 80	+ 12	0	0	0	- 2	- 2	- 2
K	+ 20	- 93	- 73	+ 101	- 140	- 39	+ 94	- 140	- 46	+ 99	- 140	- 41	0	0	0	0	- 1	- 1
L	+ 16	- 137	- 121	+ 73	- 198	- 125	+ 69	- 193	- 124	+ 62	- 188	- 126	0	- 1	- 1	0	- 7	- 7
M	+ 15	- 351	- 336	+ 53	- 473	- 420	+ 43	- 452	- 409	+ 44	- 450	- 406	0	- 19	- 19	0	- 14	- 14
N	+ 6	- 322	- 316	+ 16	- 405	- 389	+ 22	- 403	- 381	+ 36	- 415	- 379	0	- 95	- 95	0	+ 15	+ 15
O	+ 2	- 301	- 299	0	- 308	- 308	+ 13	- 316	- 303	+ 31	- 330	- 299	0	- 90	- 90	0	+ 99	+ 99
18			- 65			- 57			- 55			- 55			- 14			+ 24
17			- 64			- 60			- 59			- 58			- 11			+ 21
16			- 63			- 61			- 60			- 59			- 10			+ 20
15			- 65			- 60			- 59			- 58			- 10			+ 19
14			- 65			- 54			- 53			- 52			- 11			+ 17
13			- 107			- 86			- 84			- 83			- 21			+ 25
12			- 62			- 51			- 51			- 49			- 18			+ 23
11			- 36			- 38			- 38			- 37			- 8			+ 21
10			- 12			- 22			- 22			- 21			0			+ 14
9			+ 5			- 1			- 1			- 1			+ 4			+ 10
8			+ 11			+ 9			+ 9			+ 9			+ 10			+ 15
7			+ 7			+ 6			+ 6			+ 6			+ 6			+ 10
6			+ 9			+ 8			+ 8			+ 8			+ 7			+ 9
5			+ 9			+ 8			+ 8			+ 8			+ 8			+ 9
4			+ 8			+ 7			+ 7			+ 7			+ 7			+ 8
3			+ 5			+ 4			+ 4			+ 4			+ 3			+ 5
2			+ 3			+ 3			+ 3			+ 3			+ 3			+ 4
1			+ 1			+ 1			+ 1			+ 1			+ 1			+ 1
Total.			- 414			+ 382			+ 313			+ 281			- 205			+ 446

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Mount Hamilton, Cal., No. 55				Seattle, Wash. (high school), No. 56				Iron River, Mich., No. 57				Ely, Minn., No. 58			
A		+ 2	0	+ 2		+ 2	0	+ 2	1500	+ 2	0	+ 2	1470	+ 2	0	+ 2
B		+ 68	0	+ 68		+ 44	0	+ 44	1500	+ 64	0	+ 64	1470	+ 64	0	+ 64
C		+ 156	0	+ 156		+ 18	0	+ 18	1500	+ 124	0	+ 124	1470	+ 124	0	+ 124
D		+ 246	- 6	+ 240		+ 10	0	+ 10	1500	+ 138	0	+ 138	1470	+ 138	0	+ 138
E		+ 282	- 8	+ 274		+ 3	0	+ 3	1560	+ 80	0	+ 80	1470	+ 80	0	+ 80
F		+ 194	- 10	+ 184		0	0	0	1580	+ 40	0	+ 40	1470	+ 30	0	+ 30
G		+ 104	- 12	+ 92		0	0	0	1580	+ 12	0	+ 12	1470	+ 12	0	+ 12
H		+ 69	- 16	+ 53		0	0	0	1580	+ 16	- 16	0	1470	+ 16	- 16	0
I		+ 53	- 20	+ 33		0	0	0	1590	+ 20	- 20	0	1480	+ 20	- 20	0
J		+ 32	- 25	+ 7		0	0	0	1580	0	- 16	- 16	1560	0	- 16	- 16
K		+ 20	- 28	- 8		0	0	0	1530	0	- 20	- 20	1600	0	- 20	- 20
L		0	- 18	- 18		0	- 1	- 1	1580	0	- 42	- 42	1580	0	- 33	- 33
M		0	- 24	- 24		0	- 19	- 19	1470	0	- 84	- 84	1550	0	- 85	- 85
N		0	- 16	- 16		0	- 95	- 95	1200	0	- 63	- 63	1240	0	- 69	- 69
O		0	0	0		0	- 89	- 89	860	0	- 50	- 50	1180	0	- 67	- 67
18				+ 2				- 14				- 6				- 12
17				- 2				- 11				- 6				- 12
16				0				- 10				- 6				- 12
15				+ 2				- 10				- 7				- 12
14				+ 8				- 11				- 7				- 11
13				+ 22				- 81				- 18				- 16
12				+ 19				- 18				- 12				- 13
11				+ 20				- 8				- 9				- 11
10				+ 15				0				- 7				- 10
9				+ 10				+ 4				- 8				- 6
8				+ 15				+ 10				+ 8				- 1
7				+ 10				+ 6				+ 8				+ 5
6				+ 9				+ 7				+ 8				+ 9
5				+ 9				+ 8				+ 8				+ 9
4				+ 8				+ 7				+ 6				+ 6
3				+ 5				+ 3				+ 4				+ 4
2				+ 4				+ 3				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total...				+ 1200				- 181				+ 143				+ 83
	Pembina, N. Dak., No. 59				Mitchell, S. Dak., No. 60				Sweetwater, Tex., No. 61				Kerrville, Tex., No. 62			
A	796	+ 2	0	+ 2	1340	+ 2	0	+ 2	2149	+ 2	0	+ 2	1633	+ 2	0	+ 2
B	796	+ 60	0	+ 60	1340	+ 64	0	+ 64	2150	+ 68	0	+ 68	1650	+ 68	0	+ 68
C	796	+ 88	0	+ 88	1340	+ 116	0	+ 116	2150	+ 136	0	+ 136	1650	+ 128	0	+ 128
D	796	+ 60	0	+ 60	1330	+ 123	0	+ 123	2160	+ 191	0	+ 191	1667	+ 151	0	+ 151
E	796	+ 24	0	+ 24	1320	+ 65	0	+ 65	2160	+ 156	- 8	+ 148	1700	+ 92	0	+ 92
F	796	+ 10	0	+ 10	1320	+ 30	0	+ 30	2156	+ 79	- 10	+ 69	1740	+ 49	- 4	+ 45
G	796	0	0	0	1330	+ 12	0	+ 12	2130	+ 37	- 12	+ 25	1750	+ 32	- 12	+ 20
H	796	0	0	0	1320	+ 16	- 16	0	2140	+ 32	- 16	+ 16	1830	+ 32	- 16	+ 16
I	796	0	0	0	1320	+ 20	- 20	0	2200	+ 20	- 20	0	1835	+ 20	- 20	0
J	800	0	- 16	- 16	1330	0	- 16	- 16	2260	0	- 16	- 16	1930	0	- 16	- 16
K	800	0	- 20	- 20	1330	0	- 20	- 20	2280	0	- 24	- 24	1912	0	- 20	- 20
L	800	0	- 24	- 24	1360	0	- 28	- 28	2290	0	- 54	- 54	1900	0	- 48	- 48
M	960	0	- 52	- 52	1410	0	- 78	- 78	2150	0	- 123	- 123	1870	0	- 107	- 107
N	990	0	- 52	- 52	1540	0	- 80	- 80	2000	0	- 100	- 100	1460	0	- 76	- 76
O	1100	0	- 62	- 62	1620	0	- 89	- 89	2100	0	- 107	- 107	1210	0	- 64	- 64
18				- 13				- 18				- 24				- 12
17				- 13				- 18				- 22				- 12
16				- 13				- 18				- 21				- 11
15				- 13				- 19				- 22				- 13
14				- 14				- 19				- 22				- 18
13				- 25				- 31				- 38				- 23
12				- 14				- 21				- 31				- 13
11				- 13				- 24				- 14				- 11
10				- 15				- 16				- 11				- 8
9				- 8				- 10				+ 2				+ 9
8				- 5				- 5				+ 8				+ 8
7				+ 4				+ 6				+ 9				+ 9
6				+ 10				+ 9				+ 10				+ 10
5				+ 10				+ 11				+ 10				+ 10
4				+ 7				+ 7				+ 9				+ 9
3				+ 3				+ 4				+ 6				+ 6
2				+ 4				+ 3				+ 8				+ 8
1				+ 1				+ 1				+ 1				+ 1
Total...				- 89				- 57				+ 93				+ 133

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	El Paso, Tex., No. 63				Nogales, Ariz., No. 64				Yuma, Ariz., No. 65				Compton, Cal., No. 66			
A	3760	+ 2	0	+ 2	3874	+ 2	0	+ 2	176	+ 2	0	+ 2	69	+ 2	0	+ 2
B	3760	+ 68	0	+ 68	3874	+ 68	0	+ 68	176	+ 36	0	+ 36	70	+ 16	0	+ 16
C	3770	+ 156	0	+ 156	3874	+ 156	0	+ 156	176	+ 12	0	+ 12	70	+ 4	0	+ 4
D	3770	+ 268	- 6	+ 262	3874	+ 270	- 6	+ 264	168	+ 6	0	+ 6	69	0	0	0
E	3800	+ 292	- 8	+ 284	3900	+ 296	- 8	+ 288	162	0	0	0	69	0	0	0
F	3865	+ 187	- 10	+ 177	3930	+ 193	- 10	+ 183	155	0	0	0	74	0	0	0
G	3880	+ 98	- 12	+ 86	3910	+ 105	- 12	+ 93	140	0	0	0	86	0	0	0
H	3910	+ 61	- 16	+ 45	3960	+ 61	- 16	+ 48	151	0	0	0	91	0	0	0
I	3960	+ 60	- 40	+ 20	3980	+ 60	- 40	+ 20	159	0	0	0	81	0	0	0
J	4070	+ 32	- 48	- 16	3820	+ 32	- 48	- 16	207	0	0	0	90	0	0	0
K	4030	+ 20	- 60	- 40	3900	+ 20	- 60	- 40	298	0	- 6	- 6	134	0	0	0
L	3910	+ 24	- 96	- 72	3600	+ 11	- 86	- 72	415	0	- 12	- 12	200	0	- 5	- 5
M	4200	+ 16	- 212	- 226	2890	+ 9	- 171	- 162	430	0	- 28	- 28	390	0	- 25	- 25
N	4200	+ 6	- 216	- 210	2875	0	- 150	- 150	470	0	- 25	- 25	1010	0	- 50	- 50
O	4570	0	- 221	- 221	2920	0	- 148	- 148	932	0	- 48	- 48	1130	0	- 60	- 60
18				- 46				- 30				- 17				- 10
17				- 45				- 24				- 17				- 8
16				- 44				- 24				- 18				0
15				- 48				- 28				- 18				+ 6
14				- 49				- 28				- 20				+ 7
13				- 75				- 49				- 15				+ 18
12				- 32				- 27				- 9				+ 14
11				- 23				- 12				+ 3				+ 9
10				- 7				0				+ 3				+ 13
9				+ 3				+ 6				+ 10				+ 11
8				+ 14				+ 15				+ 16				+ 16
7				+ 5				+ 8				+ 10				+ 11
6				+ 10				+ 9				+ 9				+ 9
5				+ 10				+ 9				+ 9				+ 9
4				+ 9				+ 8				+ 8				+ 8
3				+ 6				+ 6				+ 6				+ 6
2				+ 3				+ 4				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total...				+ 7				+ 377				- 99				+ 5
	Goldfield, Nev., No. 67				Yavapai, Ariz., No. 68				Grand Canyon, Ariz., No. 69				Gallup, N. Mex., No. 70			
A	5629	+ 2	0	+ 2	7150	+ 2	0	+ 2	2784	+ 2	0	+ 2	6496	+ 2	0	+ 2
B	5700	+ 68	0	+ 68	7150	+ 68	0	+ 68	2784	+ 68	0	+ 68	6496	+ 68	0	+ 68
C	5690	+ 164	- 4	+ 160	6800	+ 126	- 4	+ 122	2875	+ 148	0	+ 148	6496	+ 164	- 4	+ 160
D	5688	+ 301	- 6	+ 295	6440	+ 267	- 6	+ 261	3100	+ 190	- 5	+ 185	6496	+ 318	- 6	+ 312
E	5700	+ 406	- 12	+ 394	5850	+ 391	- 12	+ 379	3510	+ 182	- 8	+ 174	6600	+ 440	- 16	+ 424
F	5840	+ 328	- 20	+ 308	5210	+ 339	- 15	+ 324	3800	+ 92	- 10	+ 82	6660	+ 390	- 20	+ 370
G	5970	+ 195	- 24	+ 171	5590	+ 247	- 20	+ 227	4410	+ 37	- 16	+ 21	6720	+ 242	- 24	+ 218
H	5970	+ 147	- 32	+ 115	5320	+ 177	- 25	+ 152	4820	+ 11	- 23	- 12	6720	+ 175	- 32	+ 143
I	5975	+ 113	- 52	+ 61	5110	+ 158	- 49	+ 109	5170	+ 7	- 48	- 41	6760	+ 148	- 60	+ 88
J	5990	+ 51	- 62	- 11	5510	+ 85	- 60	+ 25	5500	+ 15	- 61	- 46	6850	+ 83	- 79	+ 4
K	5610	+ 51	- 91	- 40	6240	+ 79	- 105	- 26	6390	- 6	- 106	- 112	6960	+ 75	- 120	- 45
L	5400	+ 29	- 125	- 96	6160	+ 49	- 156	- 107	6280	- 5	- 149	- 154	7050	+ 48	- 169	- 121
M	5900	0	- 313	- 313	5930	+ 51	- 345	- 294	6150	+ 2	- 359	- 357	7190	+ 34	- 417	- 383
N	5480	+ 16	- 293	- 277	5950	+ 17	- 306	- 289	5950	+ 7	- 306	- 299	6820	+ 16	- 359	- 343
O	6210	+ 1	- 302	- 301	5200	+ 9	- 265	- 256	5200	+ 9	- 265	- 266	6410	+ 9	- 321	- 312
18				- 61				- 56				- 56				- 63
17				- 56				- 53				- 53				- 63
16				- 51				- 48				- 48				- 65
15				- 41				- 48				- 48				- 69
14				- 40				- 50				- 50				- 63
13				- 61				- 81				- 81				- 91
12				- 20				- 56				- 56				- 47
11				- 4				- 25				- 25				- 32
10				+ 5				- 4				- 4				- 9
9				+ 8				+ 6				+ 6				+ 4
8				+ 12				+ 12				+ 12				+ 12
7				+ 9				+ 8				+ 8				+ 7
6				+ 9				+ 9				+ 9				+ 9
5				+ 9				+ 9				+ 9				+ 9
4				+ 8				+ 8				+ 8				+ 8
3				+ 5				+ 5				+ 5				+ 5
2				+ 4				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total...				+ 272				+ 337				- 957				+ 141

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
Las Vegas, N. Mex., No. 71					Shamrock, Tex., No. 72				Denison, Tex., No. 73				Minneapolis, Minn., No. 74			
A	6429	+ 2	0	+ 2	2300	+ 2	0	+ 2	754	+ 2	0	+ 2	840	+ 2	0	+ 2
B	6429	+ 68	0	+ 68	2300	+ 68	0	+ 68	754	+ 60	0	+ 60	840	+ 60	0	+ 60
C	6429	+ 164	- 4	+ 160	2300	+ 140	0	+ 140	740	+ 84	0	+ 84	840	+ 92	0	+ 92
D	6429	+ 318	- 6	+ 312	2300	+ 198	0	+ 198	740	+ 54	0	+ 54	830	+ 64	0	+ 64
E	6400	+ 440	- 16	+ 424	2300	+ 168	- 8	+ 160	730	+ 24	0	+ 24	820	+ 24	0	+ 24
F	6460	+ 381	- 20	+ 361	2300	+ 90	- 10	+ 80	690	+ 10	0	+ 10	840	+ 10	0	+ 10
G	6530	+ 241	- 24	+ 217	2300	+ 48	- 12	+ 36	660	0	0	0	880	0	0	0
H	6540	+ 169	- 32	+ 137	2300	+ 32	- 16	+ 16	690	0	0	0	890	0	0	0
I	6680	+ 148	- 60	+ 88	2350	+ 20	- 20	0	650	0	0	0	880	0	0	0
J	6800	+ 85	- 79	+ 6	2390	+ 4	- 20	- 16	690	0	- 16	- 16	880	0	- 16	- 16
K	6850	+ 78	- 120	- 42	2425	+ 13	- 40	- 27	670	0	- 20	- 20	900	0	- 20	- 20
L	7100	+ 43	- 171	- 128	2420	+ 4	- 56	- 52	700	0	- 24	- 24	920	0	- 24	- 24
M	7100	+ 35	- 412	- 377	2300	0	- 128	- 128	680	0	- 37	- 37	990	0	- 56	- 56
N	6650	+ 21	- 350	- 329	2260	0	- 115	- 115	710	0	- 42	- 42	1000	0	- 48	- 48
O	6140	+ 12	- 309	- 297	2410	0	- 122	- 122	760	0	- 45	- 45	1040	0	- 56	- 56
18				- 62				- 24				- 9				- 12
17				- 62				- 24				- 9				- 12
16				- 62				- 24				- 9				- 12
15				- 59				- 24				- 9				- 13
14				- 61				- 25				- 9				- 13
13				- 89				- 44				- 20				- 21
12				- 43				- 25				- 13				- 15
11				- 26				- 17				- 11				- 18
10				- 18				- 14				- 12				- 9
9				- 1				- 1				- 3				- 6
8				+ 9				+ 6				+ 3				0
7				+ 7				+ 8				+ 8				+ 6
6				+ 9				+ 10				+ 9				+ 9
5				+ 10				+ 10				+ 11				+ 10
4				+ 8				+ 9				+ 8				+ 6
3				+ 5				+ 6				+ 5				+ 4
2				+ 3				+ 3				+ 3				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total..				+ 171				+ 70				- 6				- 52
Lead, S. Dak., No. 75					Bismarck, N. Dak., No. 76				Hinsdale, Mont., No. 77				Sand Point, Idaho, No. 78			
A	5216	+ 2	0	+ 2	1690	+ 2	0	+ 2	2170	+ 2	0	+ 2	2090	+ 2	0	+ 2
B	5200	+ 64	0	+ 64	1690	+ 68	0	+ 68	2170	+ 68	0	+ 68	2090	+ 68	0	+ 68
C	5200	+ 164	- 4	+ 160	1690	+ 128	0	+ 128	2160	+ 140	0	+ 140	2100	+ 136	0	+ 136
D	5200	+ 300	- 6	+ 294	1700	+ 156	0	+ 156	2160	+ 190	0	+ 190	2100	+ 186	0	+ 186
E	5290	+ 386	- 8	+ 378	1700	+ 98	0	+ 98	2170	+ 155	- 8	+ 147	2080	+ 148	- 8	+ 140
F	5300	+ 296	- 20	+ 276	1720	+ 49	- 5	+ 44	2210	+ 80	- 10	+ 70	2050	+ 73	- 10	+ 63
G	5420	+ 182	- 24	+ 158	1730	+ 24	- 6	+ 18	2270	+ 38	- 12	+ 26	2080	+ 36	- 12	+ 24
H	5550	+ 131	- 32	+ 99	1710	+ 22	- 16	+ 6	2330	+ 17	- 16	+ 1	2230	+ 26	- 16	+ 10
I	5600	+ 83	- 40	+ 43	1730	+ 20	- 20	0	2350	+ 20	- 20	0	2510	+ 15	- 20	- 5
J	5260	+ 45	- 48	- 3	1780	0	- 16	- 16	2360	0	- 16	- 16	2720	+ 16	- 32	- 16
K	5040	+ 45	- 80	- 35	1820	0	- 20	- 20	2320	0	- 25	- 25	2900	0	- 43	- 43
L	4840	+ 32	- 120	- 88	1880	0	- 48	- 48	2390	0	- 54	- 54	3100	+ 1	- 72	- 71
M	4400	+ 27	- 260	- 233	2000	0	- 112	- 112	2650	0	- 149	- 149	3890	+ 11	- 238	- 227
N	3890	0	- 199	- 199	2010	0	- 96	- 96	2790	0	- 145	- 145	3970	0	- 204	- 204
O	3610	0	- 174	- 174	2020	0	- 105	- 105	2890	0	- 135	- 135	4110	0	- 205	- 205
18				- 36				- 20				- 31				- 42
17				- 37				- 20				- 31				- 42
16				- 37				- 19				- 31				- 40
15				- 39				- 20				- 32				- 40
14				- 40				- 20				- 33				- 40
13				- 61				- 38				- 66				- 70
12				- 35				- 26				- 40				- 39
11				- 30				- 23				- 30				- 21
10				- 18				- 17				- 21				- 11
9				- 6				- 10				- 13				0
8				+ 1				- 3				+ 2				+ 7
7				+ 6				+ 5				+ 5				+ 6
6				+ 9				+ 9				+ 10				+ 8
5				+ 10				+ 10				+ 9				+ 8
4				+ 7				+ 7				+ 7				+ 7
3				+ 4				+ 4				+ 3				+ 3
2				+ 3				+ 3				+ 4				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+ 443				- 54				- 167				- 444

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Eleva- tion in feet	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Eleva- tion in feet	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Eleva- tion in feet	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation	Eleva- tion in feet	Topog- raphy	Com- pen- sation	Topog- raphy and com- pen- sation
	Boise, Idaho, No. 79				Astoria, Oreg., No. 80				Sisson, Cal., No. 81				Rock Springs, Wyo., No. 82			
A	2690	+ 2	0	+ 2	5	+1	0	+ 1	3440	+ 2	0	+ 2	6260	+ 2	0	+ 2
B	2690	+ 68	0	+ 68	5	0	0	0	3440	+ 68	0	+ 68	6260	+ 68	0	+ 68
C	2690	+148	0	+148	15	0	0	0	3420	+151	0	+151	6250	+164	- 4	+160
D	2700	+222	0	+222	50	-5	0	- 5	3400	+259	- 6	+253	6270	+315	- 6	+309
E	2720	+201	- 8	+193	120	-1	0	- 1	3390	+264	- 8	+256	6290	+433	-16	+417
F	2760	+111	-10	+101	50	0	0	0	3640	+169	-10	+159	6360	+370	-20	+350
G	2830	+ 60	-12	+ 48	20	0	0	0	3790	+ 84	-12	+ 72	6420	+234	-24	+210
H	2930	+ 41	-16	+ 25	20	0	0	0	3890	+ 48	-16	+ 32	6510	+161	-32	+129
I	3120	+18	-20	- 2	20	0	0	0	4550	+35	-40	- 5	6700	+146	-60	+ 86
J	3440	+18	-32	-14	80	0	0	0	5450	+16	-48	-32	6540	+ 89	- 80	+ 9
K	3560	+ 5	- 60	- 55	90	0	0	0	5290	+ 2	- 80	- 78	6610	+ 80	-120	- 40
L	3560	- 4	- 81	- 85	190	0	- 4	- 4	4610	+ 8	-111	-103	6880	+ 43	-163	-120
M	3880	+ 8	-231	-223	410	0	-23	-23	4250	+11	-252	-241	7020	+ 56	-406	-350
N	4410	+ 7	-234	-227	- 40	0	+ 4	+ 4	4010	0	-205	-205	7180	+15	-378	-363
O	4790	+ 8	-241	-233	-552	0	+29	+29	3510	0	-174	-174	7730	+ 6	-377	-371
18				- 53				+ 3				- 29				- 73
17				- 56				0				- 25				- 71
16				- 56				+ 3				- 21				- 71
15				- 54				+ 5				- 17				- 73
14				- 52				+ 3				- 7				- 67
13				- 80				0				- 2				- 99
12				- 57				- 1				+ 8				- 55
11				- 24				+ 3				+ 12				- 38
10				- 8				+ 6				+ 9				- 16
9				+ 2				+ 6				+ 8				+ 8
8				+ 9				+11				+13				+10
7				+ 7				+ 7				+ 9				+ 7
6				+ 8				+ 7				+ 8				+ 9
5				+ 8				+ 8				+ 9				+ 9
4				+ 7				+ 7				+ 8				+ 8
3				+ 4				+ 3				+ 4				+ 5
2				+ 3				+ 3				+ 4				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				-423				+76				+147				-13
	Paxton, Nebr., No. 83				Washington, D. C. (Bureau of Standards), No. 84				North Hero, Vt., No. 85				Lake Placid, N. Y., No. 86			
A	3060	+ 2	0	+ 2		+ 2	0	+ 2	115	+ 2	0	+ 2	1870	+ 2	0	+ 2
B	3060	+ 68	0	+ 68		+48	0	+ 48	115	+24	0	+24	1870	+ 68	0	+ 68
C	3060	+152	0	+152		+32	0	+ 32	115	+ 4	0	+ 4	1880	+136	0	+136
D	3070	+243	- 3	+240		+16	0	+ 16	120	+ 6	0	+ 6	1890	+170	0	+170
E	3080	+236	- 8	+228		+ 8	0	+ 8	110	0	0	0	1860	+119	- 3	+116
F	3110	+140	-10	+130		0	0	0	110	0	0	0	1920	+ 59	- 7	+ 52
G	3120	+ 72	-12	+ 60		0	0	0	100	0	0	0	1930	+ 37	-12	+ 25
H	3110	+ 48	-16	+ 32		0	0	0	100	0	0	0	2020	+ 23	- 7	+ 15
I	3120	+ 20	-20	0		0	0	0	110	0	0	0	2320	+11	-20	- 9
J	3170	+16	-32	-16		0	- 1	- 1	110	0	0	0	2406	+ 8	-24	-16
K	3210	0	-40	-40		0	- 1	- 1	150	0	0	0	2260	+ 6	-40	- 34
L	3270	0	-72	-72		0	- 2	- 2	260	0	- 3	- 3	2050	0	-50	- 50
M	3250	+13	-196	-183		0	-15	-15	660	0	-32	-32	1280	0	-75	- 75
N	3270	0	-170	-170		0	-19	-19	680	0	-44	-44	980	0	-52	- 52
O	3280	0	-155	-155		0	-25	-25	680	0	-48	-48	700	0	-41	- 41
18				- 33				- 5				-10				-10
17				- 34				- 8				-10				- 9
16				- 33				- 9				-11				- 9
15				- 33				- 8				- 7				- 8
14				- 33				- 4				- 7				- 7
13				- 59				+ 8				-16				-13
12				- 33				+13				- 6				- 3
11				- 28				+18				+ 3				+ 4
10				- 17				+17				+11				+11
9				- 4				+11				+10				+ 9
8				+ 3				+18				+11				+11
7				+ 7				+ 6				+ 6				+ 6
6				+ 9				+ 6				+ 6				+ 6
5				+10				+ 7				+ 7				+ 7
4				+ 8				+ 6				+ 6				+ 6
3				+ 5				+ 6				+ 6				+ 6
2				+ 1				+ 1				+ 1				+ 1
1																
Total..				+17				+118				-86				+320

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Potsdam, N. Y., No. 87				Wilson, N. Y., No. 88				Alpena, Mich., No. 89				Virginia Beach, Va., No. 90			
A	430	+ 2	0	+ 2	280	+ 2	0	+ 2	585	+ 2	0	+ 2	12	+ 2	0	+ 2
B	430	+56	0	+56	280	+48	0	+48	580	+56	0	+56	12	0	0	0
C	430	+52	0	+52	280	+28	0	+28	580	+68	0	+68	3	0	0	0
D	440	+22	0	+22	280	+12	0	+12	580	+42	0	+42	2	0	0	0
E	420	+ 8	0	+ 8	280	+ 8	0	+ 8	580	+16	0	+16	4	0	0	0
F	430	0	0	0	270	0	0	0	580	0	0	0	2	0	0	0
G	470	0	0	0	280	0	0	0	580	0	0	0	2	0	0	0
H	475	0	0	0	270	0	0	0	580	0	0	0	0	0	0	0
I	527	0	0	0	290	0	0	0	590	0	0	0	- 3	0	0	0
J	600	0	-13	-13	270	0	0	0	590	0	-16	-16	-10	0	0	0
K	577	0	-17	-17	300	0	0	0	590	0	-20	-20	-11	0	0	0
L	635	0	-18	-18	350	0	- 8	- 8	590	0	-24	-24	-20	0	0	0
M	746	0	-40	-40	350	0	-20	-20	640	0	-35	-35	-15	0	0	0
N	810	0	-47	-47	580	0	-33	-33	660	0	-36	-36	-24	0	0	0
O	680	0	-42	-42	850	0	-46	-46	660	0	-34	-34	-98	0	+5	+ 5
18				- 8				- 9				- 7				+ 7
17				- 8				-10				- 7				+11
16				- 9				- 9				- 7				+12
15				- 8				-10				- 7				+16
14				- 9				-10				- 8				+21
13				-16				-13				-15				+38
12				- 5				- 5				-10				+30
11				+ 1				- 1				- 5				+27
10				+ 8				+ 8				- 1				+18
9				+ 7				+ 5				+ 1				+13
8				+11				+10				+ 6				+14
7				+ 7				+ 7				+ 6				+ 5
6				+ 6				+ 6				+ 7				+ 6
5				+ 6				+ 6				+ 7				+ 7
4				+ 5				+ 5				+ 5				+ 7
3				+ 6				+ 6				+ 5				+ 6
2				+ 5				+ 5				+ 5				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				-37				-18				- 5				+249
	Durham, N. C., No. 91				Fernandina, Fla., No. 92				Wilmer, Ala., No. 93				Aliceville, Ala., No. 94			
A	413	+ 2	0	+ 2	10	+2	0	+ 2	226	+ 2	0	+ 2	242	+ 2	0	+ 2
B	413	+56	0	+56	10	0	0	0	226	+42	0	+42	242	+44	0	+44
C	413	+43	0	+43	10	0	0	0	226	+20	0	+20	244	+24	0	+24
D	413	+18	0	+18	7	0	0	0	226	+12	0	+12	246	+12	0	+12
E	413	+ 8	0	+ 8	2	0	0	0	226	+ 8	0	+ 8	247	+ 8	0	+ 8
F	413	0	0	0	7	0	0	0	226	0	0	0	245	0	0	0
G	416	0	0	0	4	0	0	0	213	0	0	0	245	0	0	0
H	415	0	0	0	- 3	0	0	0	213	0	0	0	248	0	0	0
I	428	0	0	0	- 2	0	0	0	217	0	0	0	248	0	0	0
J	426	0	0	0	0	0	0	0	219	0	0	0	247	0	0	0
K	439	0	- 5	- 5	- 3	0	0	0	217	0	0	0	249	0	0	0
L	437	0	- 5	- 5	-15	0	0	0	172	0	0	0	251	0	0	0
M	444	0	-26	-26	-10	0	0	0	131	0	-7	- 7	255	0	-14	-14
N	401	0	-24	-24	- 2	0	0	0	94	0	-5	- 5	269	0	-17	-17
O	447	0	-20	-20	-35	0	0	0	71	0	0	0	323	0	-18	-18
18				- 5				+ 2				0				- 4
17				- 7				+ 3				+ 1				- 4
16				- 7				+ 4				+ 2				- 4
15				- 1				+ 5				+ 5				- 4
14				- 1				+ 7				+ 7				- 4
13				+ 2				+18				+15				- 1
12				+15				+22				+14				+ 2
11				+18				+24				+ 7				+ 3
10				+19				+20				+ 6				+ 6
9				+12				+13				+ 2				+ 3
8				+11				+12				+ 6				+ 4
7				+ 5				+ 5				+ 7				+ 7
6				+ 6				+ 7				+ 9				+ 8
5				+ 8				+ 9				+10				+11
4				+ 7				+ 7				+ 8				+ 7
3				+ 6				+ 6				+ 6				+ 6
2				+ 3				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+144				+170				+181				+80

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	New Madrid, Mo., No. 95				Mena, Ark., No. 96				Nacogdoches, Tex., No. 97				Alpine, Tex., No. 98			
A	258	+ 2	0	+ 2	1209	+ 2	0	+ 2	303	+ 2	0	+ 2	4460	+ 2	0	+ 2
B	258	+44	0	+44	1209	+ 64	0	+ 64	300	+48	0	+48	4460	+ 68	0	+ 68
C	258	+24	0	+24	1209	+112	0	+112	300	+32	0	+32	4460	+164	- 4	+160
D	258	+12	0	+12	1200	+108	0	+108	300	+12	0	+12	4470	+288	- 6	+282
E	260	+ 8	0	+ 8	1119	+ 56	0	+ 56	300	+ 8	0	+ 8	4500	+344	- 8	+336
F	260	0	0	0	1120	+ 22	0	+ 22	300	0	0	0	4550	+240	-10	+230
G	260	0	0	0	1175	+ 3	0	+ 3	300	0	0	0	4520	+129	-12	+117
H	259	0	0	0	1247	+ 4	- 4	0	300	0	0	0	4540	+ 80	-16	+ 64
I	288	0	0	0	1205	+ 5	- 5	0	300	0	0	0	4730	+ 67	-40	+ 27
J	288	0	0	0	1222	0	-16	- 16	291	0	0	0	4960	+ 34	-48	- 14
K	290	0	0	0	1192	0	-20	- 20	281	0	0	0	4910	+ 37	-80	-43
L	290	0	0	0	1169	0	-27	- 27	267	0	0	0	4800	+ 23	-115	-92
M	305	0	-14	-14	902	0	-51	- 51	286	0	-14	-14	4669	+ 22	-275	-253
N	388	0	-27	-27	688	0	-37	- 37	306	0	-19	-19	4100	+ 4	-214	-210
O	506	0	-30	-30	700	0	-37	- 37	259	0	-13	-13	3200	0	-153	-153
18				- 6				- 7				- 3				- 28
17				- 6				- 7				- 3				- 30
16				- 6				- 7				- 3				- 30
15				- 6				- 7				- 2				- 32
14				- 7				- 7				- 1				- 32
13				-12				-13				- 3				- 55
12				- 8				-10				- 2				- 24
11				- 5				- 9				- 4				- 19
10				0				- 7				- 7				- 6
9				- 1				- 4				- 1				+ 3
8				+ 3				+ 2				+ 5				+13
7				+ 7				+ 8				+ 8				+ 6
6				+ 8				+ 9				+10				+10
5				+10				+11				+10				+10
4				+ 7				+ 8				+ 8				+ 9
3				+ 6				+ 5				+ 6				+ 6
2				+ 5				+ 3				+ 2				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+ 7				+148				+77				+326
	Farwell, Tex., No. 99				Guymon, Okla., No. 100				Helenwood, Tenn., No. 101				Cloudland, Tenn., No. 102			
A	4130	+ 2	0	+ 2	3000	+ 2	0	+ 2	1386	+ 2	0	+ 2	6200	+ 2	0	+ 2
B	4130	+ 68	0	+ 68	3100	+ 68	0	+ 68	1386	+ 64	0	+ 64	6200	+ 68	0	+ 68
C	4130	+158	- 2	+156	3100	+152	0	+152	1400	+120	0	+120	6100	+164	- 4	+160
D	4130	+282	- 6	+276	3100	+243	- 2	+240	1400	+132	0	+132	5800	+296	- 6	+290
E	4125	+314	- 8	+306	3050	+236	- 8	+228	1419	+ 75	0	+ 75	5450	+408	-11	+397
F	4125	+213	-10	+203	3050	+135	-10	+125	1470	+ 36	0	+ 36	5040	+336	-15	+321
G	4125	+114	-12	+102	3050	+ 72	-12	+ 60	1520	+12	0	+12	4480	+196	-15	+181
H	4125	+ 64	-16	+ 48	3050	+ 48	-16	+ 32	1440	+16	-16	0	3980	+127	-18	+109
I	4125	+ 60	-40	+ 20	3050	+ 20	-20	0	1450	+ 20	-20	0	3680	+114	-35	+ 79
J	4144	+ 32	-48	-16	3080	+16	-32	-16	1430	0	-16	-16	3470	+ 55	-41	+ 14
K	4150	+ 20	-60	-40	3180	0	-40	-40	1570	0	-20	-20	3150	+ 44	-43	+ 1
L	4150	+ 24	-96	-72	3430	0	-72	-72	1610	0	-45	-45	2830	+ 21	-65	-44
M	4170	+ 15	-249	-234	3490	+ 14	-210	-196	1430	0	-80	-80	2340	+ 18	-135	-117
N	4190	+ 3	-220	-217	3390	0	-176	-176	1170	0	-59	-59	2000	+ 7	-100	-93
O	3920	0	-194	-194	3480	0	-167	-167	1280	0	-68	-68	1680	0	-91	-91
18				-41				-34				-13				-14
17				-42				-34				-14				-12
16				-43				-34				-12				-10
15				-43				-34				- 8				-10
14				-44				-38				- 6				- 6
13				-67				-60				- 9				- 7
12				-34				-32				- 2				+ 3
11				-21				-21				+ 4				+ 9
10				-15				-15				+ 9				+14
9				0				- 1				+ 6				+ 9
8				+ 9				+ 7				+ 6				+ 8
7				+ 8				+ 8				+ 6				+ 6
6				+ 9				+10				+ 7				+ 7
5				+10				+10				+10				+10
4				+ 8				+ 9				+ 7				+ 7
3				+ 5				+ 6				+ 6				+ 6
2				+ 5				+ 2				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+111				- 8				+154				+1302

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Hughes, Tenn., No. 103				Charleston, W. Va., No. 104				State College, Pa., No. 105				Fort Kent, Me., No. 106			
A	3260	+ 2	0	+ 2	602	+ 2	0	+ 2	1174	+ 2	0	+ 2	524	+ 2	0	+ 2
B	3260	+ 68	0	+ 68	602	+ 56	0	+ 56	1174	+ 64	0	+ 64	525	+ 56	0	+ 56
C	3220	+ 152	0	+ 152	602	+ 72	0	+ 72	1180	+ 112	0	+ 112	525	+ 60	0	+ 60
D	3350	+ 235	- 6	+ 249	625	+ 39	0	+ 39	1165	+ 103	0	+ 103	525	+ 30	0	+ 30
E	3450	+ 250	- 8	+ 242	630	+ 14	0	+ 14	1160	+ 55	0	+ 55	525	+ 16	0	+ 16
F	3720	+ 154	- 10	+ 144	785	+ 8	0	+ 8	1130	+ 20	0	+ 20	525	0	0	0
G	4060	+ 73	- 12	+ 61	855	0	0	0	1135	0	0	0	525	0	0	0
H	4060	+ 42	- 21	+ 21	880	0	0	0	1165	0	0	0	525	0	0	0
I	3840	+ 31	- 33	- 2	920	0	0	0	1298	+ 10	- 10	0	525	0	0	0
J	3490	+ 24	- 40	- 16	985	0	- 16	- 16	1290	0	- 16	- 16	525	0	- 8	- 8
K	3250	+ 6	- 45	- 39	980	0	- 20	- 20	1340	0	- 20	- 20	525	0	- 10	- 10
L	3000	+ 10	- 72	- 62	980	0	- 24	- 24	1475	0	- 40	- 40	530	0	- 12	- 12
M	2340	+ 6	- 138	- 132	1140	0	- 62	- 62	1310	0	- 75	- 75	750	0	- 35	- 35
N	2000	0	- 98	- 98	1220	0	- 64	- 64	1230	0	- 64	- 64	830	0	- 47	- 47
O	1680	0	- 87	- 87	1670	0	- 86	- 86	1290	0	- 73	- 73	670	0	- 44	- 44
18				- 14				- 18				- 12				- 8
17				- 12				- 18				- 11				- 8
16				- 12				- 14				- 10				- 8
15				- 10				- 12				- 8				- 6
14				- 6				- 10				- 6				- 7
13				- 7				- 11				- 3				- 23
12				+ 3				- 1				+ 6				- 16
11				+ 9				+ 5				+ 9				+ 2
10				+ 14				+ 10				+ 12				+ 13
9				+ 9				+ 8				+ 8				+ 12
8				+ 8				+ 8				+ 11				+ 12
7				+ 6				+ 5				+ 6				+ 6
6				+ 7				+ 6				+ 6				+ 6
5				+ 10				+ 8				+ 7				+ 6
4				+ 7				+ 7				+ 6				+ 6
3				+ 6				+ 6				+ 6				+ 6
2				+ 3				+ 3				+ 4				+ 6
1				+ 1				+ 1				+ 1				+ 1
Total..				+ 526				- 98				+ 100				+ 9
	Prentice, Wis., No. 107				Fergus Falls, Minn., No. 108				Sheridan, Wyo., No. 109				Boulder, Mont., No. 110			
A	1539	+ 2	0	+ 2	1200	+ 2	0	+ 2	3773	+ 2	0	+ 2	4898	+ 2	0	+ 2
B	1539	+ 68	0	+ 68	1200	+ 64	0	+ 64	3773	+ 68	0	+ 68	4900	+ 68	0	+ 68
C	1539	+ 124	0	+ 124	1200	+ 112	0	+ 112	3790	+ 158	- 2	+ 156	4900	+ 164	- 4	+ 160
D	1500	+ 138	0	+ 138	1200	+ 108	0	+ 108	3768	+ 270	- 6	+ 264	4900	+ 300	- 6	+ 294
E	1500	+ 80	0	+ 80	1200	+ 56	0	+ 56	3812	+ 291	- 8	+ 283	4900	+ 364	- 8	+ 356
F	1500	+ 30	0	+ 30	1200	+ 20	0	+ 20	3840	+ 182	- 10	+ 172	5000	+ 268	- 18	+ 250
G	1500	+ 12	0	+ 12	1200	0	0	0	3883	+ 96	- 12	+ 84	5117	+ 166	- 23	+ 143
H	1500	+ 16	- 16	0	1200	+ 6	- 6	0	3881	+ 64	- 16	+ 48	5294	+ 115	- 32	+ 83
I	1500	+ 20	- 20	0	1200	+ 8	- 8	0	3885	+ 60	- 40	+ 20	5600	+ 78	- 40	+ 38
J	1500	0	- 16	- 16	1200	0	- 16	- 16	4025	+ 30	- 46	- 16	6281	+ 49	- 68	- 19
K	1500	0	- 20	- 20	1200	0	- 20	- 20	4150	+ 18	- 63	- 45	6415	+ 42	- 108	- 66
L	1483	0	- 44	- 44	1105	0	- 24	- 24	5215	+ 12	- 121	- 109	6346	+ 33	- 153	- 120
M	1443	0	- 82	- 82	1128	0	- 63	- 63	6093	+ 1	- 358	- 357	5314	+ 23	- 310	- 287
N	1359	0	- 71	- 71	1156	0	- 58	- 58	5375	+ 9	- 284	- 275	5950	+ 17	- 317	- 300
O	1089	0	- 61	- 61	1202	0	- 69	- 69	4736	+ 2	- 229	- 227	5965	0	- 287	- 287
18				- 9				- 12				- 46				- 54
17				- 9				- 12				- 49				- 53
16				- 9				- 12				- 51				- 50
15				- 9				- 12				- 51				- 61
14				- 9				- 16				- 46				- 48
13				- 19				- 25				- 73				- 78
12				- 13				- 16				- 43				- 46
11				- 10				- 15				- 34				- 32
10				- 8				- 7				- 20				- 18
9				- 3				- 3				- 6				- 2
8				+ 1				- 3				+ 5				+ 7
7				+ 6				+ 9				+ 6				+ 6
6				+ 8				+ 9				+ 9				+ 8
5				+ 9				+ 9				+ 9				+ 8
4				+ 6				+ 6				+ 7				+ 7
3				+ 4				+ 4				+ 4				+ 4
2				+ 4				+ 4				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+ 100				+ 9				- 306				- 73

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
Skyomish, Wash., No. 111				Olympia, Wash., No. 112				Heppner, Oreg., No. 113				Truckee, Cal., No. 114				
A	920	+ 2	0	+ 2	62	+ 2	0	+ 2	1960	+ 2	0	+ 2	5922	+ 2	0	+ 2
B	920	+ 64	0	+ 64	60	+ 16	0	+ 16	1960	+ 68	0	+ 68	5920	+ 68	0	+ 68
C	920	+ 96	0	+ 96	60	+ 4	0	+ 4	1960	+ 136	0	+ 136	5925	+ 163	- 4	+ 159
D	933	+ 72	0	+ 72	60	0	0	0	1960	+ 180	0	+ 180	5940	+ 308	- 6	+ 302
E	1144	+ 28	0	+ 28	60	0	0	0	1960	+ 134	- 6	+ 128	6019	+ 420	- 16	+ 404
F	1740	+ 3	- 5	- 2	60	0	0	0	1960	+ 69	- 9	+ 60	6070	+ 344	- 20	+ 324
G	1925	- 5	- 6	- 11	60	0	0	0	1960	+ 35	- 11	+ 24	6142	+ 211	- 24	+ 187
H	2275	- 1	- 13	- 14	60	0	0	0	1960	+ 32	- 16	+ 16	6150	+ 151	- 32	+ 119
I	2885	- 19	- 27	- 46	60	0	0	0	1960	+ 20	- 20	0	6335	+ 123	- 51	+ 72
J	3575	- 6	- 40	- 46	60	0	0	0	1960	0	- 16	- 16	6756	+ 64	- 75	- 11
K	3625	- 22	- 52	- 74	75	0	0	0	1960	0	- 20	- 20	7005	+ 62	- 120	- 58
L	3283	- 9	- 79	- 88	88	0	0	0	1475	0	- 36	- 36	6912	+ 38	- 103	- 125
M	2678	- 4	- 158	- 162	309	0	- 17	- 17	2286	0	- 133	- 133	5837	+ 33	- 342	- 309
N	2081	+ 2	- 109	- 107	1206	0	- 62	- 62	2644	0	- 133	- 133	4875	+ 8	- 254	- 246
O	1775	- 1	- 90	- 91	1174	0	- 58	- 58	3021	0	- 151	- 151	3661	+ 1	- 183	- 182
18				- 17				- 6				- 35				- 38
17				- 16				- 6				- 33				- 37
16				- 16				- 5				- 31				- 40
15				- 15				- 4				- 27				- 43
14				- 16				- 6				- 32				- 37
13				- 29				- 13				- 49				- 23
12				- 21				- 11				- 23				+ 2
11				- 10				- 3				- 16				+ 10
10				- 1				+ 3				0				+ 8
9				+ 3				+ 6				+ 6				+ 8
8				+ 9				+ 10				+ 10				+ 13
7				+ 6				+ 6				+ 7				+ 9
6				+ 7				+ 7				+ 7				+ 8
5				+ 8				+ 8				+ 8				+ 9
4				+ 7				+ 7				+ 7				+ 8
3				+ 3				+ 3				+ 3				+ 4
2				+ 3				+ 3				+ 3				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total..				- 473				- 116				- 69				+ 572
Winnemucca, Nev., No. 115				Ely, Nev., No. 116				Guernsey, Wyo., No. 117				Pierre, S. Dak., No. 118				
A	4300	+ 2	0	+ 2	6435	+ 2	0	+ 2	4336	+ 2	0	+ 2	1490	+ 2	0	+ 2
B	4300	+ 68	0	+ 68	6435	+ 68	0	+ 68	4340	+ 68	0	+ 68	1490	+ 64	0	+ 64
C	4300	+ 159	- 3	+ 156	6437	+ 164	- 4	+ 160	4340	+ 157	- 1	+ 156	1490	+ 124	0	+ 124
D	4300	+ 282	- 6	+ 276	6487	+ 314	- 6	+ 308	4355	+ 282	- 6	+ 276	1490	+ 138	0	+ 138
E	4300	+ 328	- 8	+ 320	6625	+ 440	- 16	+ 424	4384	+ 331	- 8	+ 323	1490	+ 80	0	+ 80
F	4300	+ 230	- 10	+ 220	6800	+ 381	- 20	+ 361	4423	+ 225	- 10	+ 215	1490	+ 30	0	+ 30
G	4300	+ 120	- 12	+ 108	6875	+ 237	- 24	+ 213	4519	+ 121	- 13	+ 108	1490	+ 12	0	+ 12
H	4600	+ 83	- 21	+ 62	6835	+ 170	- 32	+ 138	4541	+ 79	- 18	+ 61	1490	+ 16	- 16	0
I	4425	+ 76	- 40	+ 36	6930	+ 142	- 60	+ 82	4616	+ 67	- 40	+ 27	1490	+ 20	- 20	0
J	4468	+ 35	- 48	- 13	7237	+ 73	- 79	- 6	4694	+ 40	- 48	- 8	1498	0	- 16	- 16
K	4445	+ 29	- 69	- 40	7745	+ 74	- 138	- 64	4750	+ 31	- 72	- 41	1597	0	- 20	- 20
L	4508	+ 28	- 107	- 79	7446	+ 33	- 170	- 137	4839	0	- 96	- 96	1703	0	- 41	- 41
M	5000	+ 14	- 294	- 280	6850	+ 37	- 396	- 359	5114	+ 12	- 305	- 293	1771	0	- 101	- 101
N	5156	+ 14	- 279	- 265	6531	+ 20	- 346	- 326	5400	+ 11	- 288	- 277	1956	0	- 95	- 95
O	5043	0	- 275	- 275	6196	0	- 301	- 301	5475	0	- 268	- 268	2107	0	- 108	- 108
18				- 55				- 59				- 54				- 22
17				- 54				- 57				- 55				- 22
16				- 57				- 57				- 56				- 23
15				- 56				- 56				- 54				- 26
14				- 54				- 51				- 52				- 26
13				- 77				- 79				- 84				- 42
12				- 32				- 39				- 48				- 27
11				- 8				- 17				- 33				- 26
10				+ 3				- 2				- 22				- 17
9				+ 4				0				- 6				- 8
8				+ 11				+ 11				+ 5				- 3
7				+ 8				+ 9				+ 7				+ 6
6				+ 8				+ 9				+ 9				+ 9
5				+ 9				+ 9				+ 10				+ 11
4				+ 8				+ 8				+ 8				+ 7
3				+ 4				+ 5				+ 5				+ 4
2				+ 4				+ 4				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				- 37				+ 202				- 163				- 132

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
Fort Dodge, Iowa, No. 119				Keithsburg, Ill., No. 120				Grand Rapids, Mich., No. 121				Angola, Ind., No. 122				
A	1116	+ 2	0	+ 2	547	+ 2	0	+ 2	774	+ 2	0	+ 2	1043	+ 2	0	+ 2
B	1116	+ 64	0	+ 64	517	+ 56	0	+ 56	774	+ 60	0	+ 60	1013	+ 64	0	+ 64
C	1116	+ 108	0	+ 108	550	+ 64	0	+ 64	774	+ 84	0	+ 84	1013	+ 104	0	+ 104
D	1116	+ 96	0	+ 96	550	+ 36	0	+ 36	774	+ 54	0	+ 54	1040	+ 90	0	+ 90
E	1116	+ 48	0	+ 48	550	+ 16	0	+ 16	774	+ 24	0	+ 24	1040	+ 40	0	+ 40
F	1116	+ 20	0	+ 20	550	0	0	0	774	+ 10	0	+ 10	1040	+ 20	0	+ 20
G	1116	0	0	0	550	0	0	0	774	0	0	0	1000	0	0	0
H	1116	+ 4	- 4	0	550	0	0	0	774	0	0	0	1000	0	0	0
I	1116	+ 5	- 5	0	550	0	0	0	730	0	0	0	1000	0	0	0
J	1116	0	- 16	- 16	550	0	- 16	- 16	737	0	- 16	- 16	1000	0	- 16	- 16
K	1116	0	- 20	- 20	550	0	- 20	- 20	737	0	- 20	- 20	1000	0	- 20	- 20
L	1110	0	- 24	- 24	550	0	- 24	- 24	690	0	- 24	- 24	971	0	- 24	- 24
M	1150	0	- 63	- 63	614	0	- 33	- 33	683	0	- 37	- 37	902	0	- 53	- 53
N	1103	0	- 54	- 54	662	0	- 32	- 32	711	0	- 39	- 39	744	0	- 36	- 36
O	1139	0	- 61	- 61	686	0	- 38	- 38	713	0	- 44	- 44	737	0	- 41	- 41
18				- 11				- 7				- 7				- 7
17				- 11				- 7				- 7				- 7
16				- 11				- 7				- 7				- 7
15				- 12				- 7				- 8				- 8
14				- 13				- 9				- 9				- 9
13				- 22				- 18				- 16				- 16
12				- 15				- 11				- 10				- 10
11				- 14				- 8				- 4				- 4
10				- 11				- 6				- 1				- 1
9				- 6				- 2				+ 1				+ 1
8				0				+ 3				+ 6				+ 6
7				+ 7				+ 7				+ 7				+ 7
6				+ 9				+ 8				+ 8				+ 8
5				+ 10				+ 10				+ 8				+ 8
4				+ 6				+ 7				+ 6				+ 6
3				+ 4				+ 5				+ 5				+ 5
2				+ 4				+ 3				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total...				+ 15				- 27				+ 31				+ 111
Albany, N. Y., No. 123				Port Jervis, N. Y., No. 124				Atlantic City, N. J., No. 125				Bridgehampton, N. Y., No. 126				
A	200	+ 2	0	+ 2	461	+ 2	0	+ 2	12	+ 2	0	+ 2	32	+ 2	0	+ 2
B	200	+ 40	0	+ 40	461	+ 56	0	+ 56	14	+ 2	0	+ 2	32	+ 8	0	+ 8
C	185	+ 13	0	+ 13	480	+ 52	0	+ 52	14	0	0	0	32	0	0	0
D	183	+ 6	0	+ 6	451	+ 23	0	+ 23	7	0	0	0	35	0	0	0
E	172	+ 7	0	+ 7	465	+ 9	0	+ 9	0	0	0	0	42	0	0	0
F	155	0	0	0	588	+ 4	0	+ 4	- 4	0	0	0	42	0	0	0
G	155	0	0	0	727	0	0	0	- 6	0	0	0	52	0	0	0
H	196	0	0	0	919	0	0	0	- 8	0	0	0	66	0	0	0
I	257	0	0	0	918	- 6	- 3	- 9	- 10	0	0	0	22	0	0	0
J	306	0	- 2	- 2	956	0	- 15	- 15	- 9	0	0	0	- 8	0	0	0
K	393	0	- 7	- 7	830	0	- 18	- 18	- 2	0	0	0	- 16	0	0	0
L	671	0	- 15	- 15	883	0	- 27	- 27	- 9	0	0	0	- 31	0	+ 1	+ 1
M	922	0	- 54	- 54	1007	0	- 58	- 58	+ 4	0	0	0	- 54	0	+ 3	+ 3
N	1215	0	- 63	- 63	888	0	- 49	- 49	- 21	0	0	0	4	0	0	0
O	1071	0	- 57	- 57	713	0	- 38	- 38	+ 15	0	0	0	75	0	- 1	- 1
18				- 8				- 7				+ 1				+ 1
17				- 8				- 7				+ 4				+ 4
16				- 8				- 4				+ 10				+ 10
15				- 6				- 2				+ 12				+ 12
14				- 4				0				+ 14				+ 14
13				+ 1				+ 7				+ 21				+ 21
12				+ 14				+ 14				+ 19				+ 19
11				+ 15				+ 17				+ 20				+ 20
10				+ 14				+ 14				+ 18				+ 18
9				+ 10				+ 10				+ 16				+ 16
8				+ 14				+ 14				+ 15				+ 15
7				+ 6				+ 6				+ 6				+ 6
6				+ 6				+ 6				+ 6				+ 6
5				+ 6				+ 6				+ 6				+ 6
4				+ 6				+ 6				+ 6				+ 6
3				+ 6				+ 6				+ 6				+ 6
2				+ 4				+ 4				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total...				- 60				+ 26				+ 185				+ 106

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Chatham, Mass., No. 127				Rockland, Me., No. 128				Lancaster, N. H., No. 129				Whitehall, N. Y., No. 130			
A	5	+1	0	+1	31	+2	0	+2	858	+2	0	+2	125	+2	0	+2
B	10	+2	0	+2	32	+8	0	+8	858	+60	0	+60	125	+28	0	+28
C	19	0	0	0	30	0	0	0	851	+90	0	+90	129	+8	0	+8
D	20	0	0	0	34	0	0	0	870	+68	0	+68	167	+4	0	+4
E	10	0	0	0	42	0	0	0	896	+32	-2	+30	200	+2	0	+2
F	4	0	0	0	51	0	0	0	920	+12	-3	+9	221	0	0	0
G	5	0	0	0	90	0	0	0	1021	+4	-4	0	298	0	0	0
H	-5	0	0	0	92	0	0	0	1081	+2	-5	-3	325	0	0	0
I	-10	0	0	0	51	0	0	0	1088	+10	-10	0	518	0	0	0
J	-6	0	0	0	63	0	0	0	1231	+2	-13	-11	666	0	-8	-8
K	-27	0	0	0	71	0	-1	-1	1470	+2	-24	-22	642	0	-12	-12
L	-48	0	+1	+1	1	0	0	0	1121	0	-33	-33	823	0	-19	-19
M	-83	0	+1	+1	-15	0	0	0	1557	0	-87	-87	1071	0	-60	-60
N	-159	0	+9	+9	-38	0	+2	+2	962	0	-52	-52	1088	0	-58	-58
O	-126	0	+7	+7	165	0	-8	-8	704	0	-38	-38	1071	0	-58	-58
18				0				-3				-5				-9
17				+1				-4				-5				-8
16				+5				-3				-5				-6
15				+10				-3				-5				-6
14				+16				-3				-4				-5
13				+37				+2				-8				-5
12				+33				+15				+3				+7
11				+27				+20				+10				+11
10				+21				+18				+14				+13
9				+13				+13				+11				+10
8				+18				+18				+13				+13
7				+6				+6				+6				+6
6				+6				+6				+6				+6
5				+6				+5				+6				+6
4				+6				+6				+6				+6
3				+6				+6				+6				+6
2				+4				+5				+5				+4
1				+1				+1				+1				+1
Total...				+240				+106				+68				-121
	Little Falls, N. Y., No. 131				Watertown, N. Y., No. 132				Southport, N. Y., No. 133				Erie, Pa., No. 134			
A	448	+2	0	+2	483	+2	0	+2	873	+2	0	+2	650	+2	0	+2
B	414	+56	0	+56	489	+56	0	+56	875	+60	0	+60	650	+58	0	+58
C	450	+53	0	+53	488	+58	0	+58	875	+94	0	+94	650	+78	0	+78
D	525	+24	0	+24	475	+29	0	+29	875	+69	0	+69	648	+48	0	+48
E	662	+7	0	+7	475	+8	0	+8	891	+32	0	+32	640	+16	0	+16
F	770	+2	-1	+1	470	+2	0	+2	996	+18	-4	+14	643	+10	0	+10
G	798	0	-2	-2	484	0	0	0	1038	+5	-5	0	666	0	0	0
H	775	+3	-4	-1	536	+2	-2	0	1136	+5	-6	-1	700	+7	-7	0
I	872	+2	-8	-6	600	+7	-7	0	1340	+7	-14	-7	752	+9	-9	0
J	914	0	-10	-10	619	0	-7	-7	1362	0	-16	-16	782	0	-8	-8
K	1102	0	-16	-16	670	0	-10	-10	1355	0	-20	-20	776	0	-13	-13
L	1254	0	-31	-31	665	0	-13	-13	1429	0	-34	-34	746	0	-18	-18
M	1179	0	-66	-66	714	0	-12	-12	1207	0	-68	-68	800	0	-44	-44
N	1188	0	-62	-62	706	0	-38	-38	1244	0	-65	-65	875	0	-47	-47
O	1050	0	-58	-58	786	0	-49	-49	1104	0	-60	-60	861	0	-51	-51
18				-10				-8				-9				-10
17				-10				-7				-8				-10
16				-7				-9				-8				-9
15				-6				-8				-7				-11
14				-6				-8				-7				-10
13				-5				-13				-5				-15
12				+8				-1				+7				-6
11				+9				+2				+8				-2
10				+12				+8				+11				+5
9				+9				+7				+8				+6
8				+13				+11				+12				+9
7				+6				+7				+6				+6
6				+6				+6				+6				+7
5				+7				+6				+7				+7
4				+6				+6				+6				+6
3				+6				+6				+6				+6
2				+4				+5				+4				+4
1				+1				+1				+1				+1
Total...				-66				+6				+38				+11

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
Parkersburg, W. Va., No. 135					Columbus, Ohio, No. 136				Indianapolis, Ind., No. 137				Springfield, Ill., No. 138			
A	606	+ 2	0	+ 2	760	+ 2	0	+ 2	713	+ 2	0	+ 2	600	+ 2	0	+ 2
B	615	+56	0	+56	760	+60	0	+60	710	+60	0	+60	600	+56	0	+56
C	618	+72	0	+72	755	+84	0	+84	710	+80	0	+80	600	+72	0	+72
D	612	+42	0	+42	757	+55	0	+55	710	+48	0	+48	600	+42	0	+42
E	631	+16	0	+16	752	+24	0	+24	700	+20	0	+20	596	+20	0	+20
F	622	+ 1	0	+ 1	758	+10	0	+10	700	+12	- 2	+10	594	+ 5	0	+ 5
G	665	+ 0	0	+ 0	750	+ 2	- 2	+ 0	700	+ 3	- 3	+ 0	595	+ 0	0	+ 0
H	709	+ 3	- 3	+ 0	761	+ 3	- 3	+ 0	750	+ 3	- 3	+ 0	593	+ 3	- 3	+ 0
I	742	+ 8	- 8	+ 0	780	+ 8	- 8	+ 0	750	+10	-10	+ 0	592	+ 5	- 5	+ 0
J	719	0	-16	-16	802	0	-11	-11	800	0	- 8	- 8	593	0	- 8	- 8
K	775	0	-20	-20	838	0	-15	-15	800	0	-10	-10	596	0	-10	-10
L	800	0	-24	-24	890	0	-24	-24	800	0	-24	-24	600	0	-12	-12
M	921	0	-52	-52	950	0	-56	-56	850	0	-50	-50	579	0	-26	-26
N	1000	0	-61	-61	994	0	-48	-48	794	0	-41	-41	581	0	-32	-32
O	1221	0	-68	-68	879	0	-56	-56	675	0	-34	-34	568	0	-30	-30
18				-14				- 8				- 7				- 6
17				-14				- 9				- 7				- 6
16				-13				-10				- 7				- 6
15				-12				- 9				- 7				- 7
14				-10				- 9				- 7				- 8
13				-13				-16				-16				-17
12				- 4				- 8				- 9				-10
11				+ 5				- 3				- 6				- 8
10				+ 8				+ 5				0				- 5
9				+ 7				+ 5				+ 5				- 1
8				+ 8				+ 7				+ 5				+ 3
7				+ 5				+ 6				+ 7				+ 7
6				+ 6				+ 7				+ 8				+ 8
5				+ 8				+ 9				+ 9				+10
4				+ 7				+ 7				+ 7				+ 7
3				+ 6				+ 5				+ 5				+ 5
2				+ 3				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				-58				+ 9				+34				+47
Lebanon, Mo., No. 139					Joplin, Mo., No. 140				Fort Smith, Ark., No. 141				Texarkana, Ark., No. 142			
A	1263	+ 2	0	+ 2	994	+ 2	0	+ 2	442	+ 2	0	+ 2	325	+ 2	0	+ 2
B	1260	+ 64	0	+ 64	995	+ 64	0	+ 64	450	+56	0	+56	325	+48	0	+48
C	1261	+116	0	+116	995	+104	0	+104	450	+52	0	+52	325	+36	0	+36
D	1260	+114	0	+114	992	+ 84	0	+ 84	450	+24	0	+24	318	+14	0	+14
E	1225	+ 70	- 4	+ 66	998	+ 43	- 3	+ 40	450	+ 8	0	+ 8	310	+ 8	0	+ 8
F	1230	+ 31	- 5	+ 26	1002	+ 19	- 3	+ 16	465	0	0	0	308	0	0	0
G	1233	+ 10	- 6	+ 4	998	+ 4	- 4	+ 0	479	0	0	0	316	0	0	0
H	1206	+ 6	- 6	+ 0	997	+ 5	- 5	+ 0	462	0	0	0	316	0	0	0
I	1145	+10	-10	+ 0	992	+10	-10	+ 0	455	+ 5	- 5	+ 0	310	0	0	0
J	1131	+ 3	-12	- 9	972	0	-16	- 16	512	+ 4	- 8	- 4	300	0	0	0
K	1145	0	-20	-20	955	0	-20	-20	552	0	- 7	- 7	285	0	- 6	- 6
L	1066	0	-24	-24	1000	0	-24	-24	622	0	-14	-14	367	0	- 8	- 8
M	1129	0	-63	-63	1029	0	-57	-57	871	0	-50	-50	351	0	-21	-21
N	1131	0	-55	-55	1038	0	-54	-54	1006	0	-52	-52	406	0	-28	-28
O	1032	0	-57	-57	1032	0	-62	-62	911	0	-47	-47	512	0	-33	-33
18				- 9				-12				- 8				- 5
17				- 9				-11				- 7				- 5
16				- 9				-11				- 7				- 5
15				- 7				-10				- 8				- 5
14				- 7				-10				- 8				- 5
13				-17				-17				-14				- 8
12				-11				-12				-11				- 5
11				-11				-13				-10				- 6
10				- 8				-11				- 8				- 6
9				- 4				- 5				- 4				- 3
8				+ 1				+ 1				+ 2				+ 3
7				+ 8				+ 8				+ 8				+ 8
6				+ 9				+ 9				+ 9				+ 9
5				+11				+11				+11				+11
4				+ 8				+ 7				+ 8				+ 8
3				+ 5				+ 5				+ 5				+ 5
2				+ 3				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+118				+10				-70				+ 7

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Hot Springs, Ark., No. 143				Alexandria, La., No. 144				Laurel, Miss., No. 145				Richmond, Va., No. 146			
A	620	+ 2	0	+ 2	76	+ 2	0	+ 2	250	+ 2	0	+ 2	97	+ 2	0	+ 2
B	620	+56	0	+56	76	+20	0	+20	250	+44	0	+ 44	100	+24	0	+24
C	620	+72	0	+72	76	+ 4	0	+ 4	250	+24	0	+ 24	85	+ 4	0	+ 4
D	640	+40	0	+40	76	+ 2	0	+ 2	250	+ 9	0	+ 9	93	+ 2	0	+ 2
E	678	+17	0	+17	76	0	0	0	250	+ 2	0	+ 2	90	0	0	0
F	665	+10	0	+10	76	0	0	0	250	0	0	0	100	0	0	0
G	658	+ 2	- 2	0	100	0	0	0	250	0	0	0	134	0	0	0
H	801	+ 3	- 3	0	100	0	0	0	250	0	- 1	- 1	144	0	0	0
I	804	0	- 6	- 6	100	0	0	0	250	0	- 2	- 2	152	0	0	0
J	809	0	- 5	- 5	100	0	0	0	250	0	- 3	- 3	156	0	0	0
K	658	0	-14	-14	100	0	0	0	300	0	- 5	- 5	168	0	0	0
L	804	0	-11	-11	100	0	0	0	300	0	- 7	- 7	156	0	0	0
M	807	0	-34	-34	64	0	0	0	250	0	-14	-14	158	0	- 8	- 8
N	562	0	-33	-33	75	0	0	0	172	0	- 9	- 9	187	0	-12	-12
O	632	0	-35	-35	89	0	0	0	147	0	- 5	- 5	314	0	-16	-16
18				- 6				- 1				- 1				- 5
17				- 6				- 1				- 1				- 6
16				- 6				- 1				0				- 7
15				- 6				+ 1				+ 1				- 7
14				- 6				+ 2				+ 2				- 2
13				- 9				+ 8				+ 9				+13
12				- 7				+ 8				+10				+18
11				- 6				+ 1				+ 6				+18
10				- 4				- 3				+ 4				+18
9				- 5				- 1				+ 1				+18
8				+ 2				+ 5				+ 5				+18
7				+ 2				+ 8				+ 7				+ 6
6				+ 9				+10				+ 9				+ 6
5				+11				+10				+10				+ 8
4				+ 7				+ 8				+ 8				+ 7
3				+ 5				+ 6				+ 6				+ 6
2				+ 3				+ 2				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+44				+91				+114				+96
	Emporia, Va., No. 147				Greenville, N. C., No. 148				Wilmington, N. C., No. 149				Cheraw, S. C., No. 150			
A	120	+ 2	0	+ 2	55	+ 2	0	+ 2	28	+2	0	+ 2	180	+ 2	0	+ 2
B	120	+28	0	+28	55	+14	0	+14	28	+8	0	+ 8	180	+36	0	+36
C	120	+ 4	0	+ 4	55	+ 4	0	+ 4		0	0	0	180	+12	0	+12
D	120	+ 1	0	+ 1	32	0	0	0		0	0	0	180	+ 6	0	+ 6
E	120	0	0	0	39	0	0	0		0	0	0	180	0	0	0
F	120	0	0	0	35	0	0	0		0	0	0	200	0	0	0
G	120	0	0	0	38	0	0	0		0	0	0	200	0	0	0
H	120	0	0	0	41	0	0	0		0	0	0	200	0	0	0
I	120	0	0	0	50	0	0	0		0	0	0	300	0	0	0
J	120	0	0	0	49	0	0	0		0	0	0	300	0	0	0
K	120	0	0	0	56	0	0	0		0	0	0	300	0	0	0
L	120	0	0	0	65	0	0	0		0	0	0	300	0	0	0
M	94	0	0	0	69	0	-4	- 4		0	0	0	286	0	-18	-18
N	149	0	-10	-10	64	0	-3	- 3		15	0	0	291	0	-16	-16
O	212	0	-10	-10	111	0	-5	- 5		-42	0	+ 4	315	0	-16	-16
18				- 3				- 1				+ 2				- 4
17				- 4				+ 1				+ 4				- 5
16				- 4				+ 3				+ 9				- 5
15				+ 5				+ 7				+13				+ 2
14				+ 7				+12				+21				+ 4
13				+15				+34				+34				+16
12				+20				+24				+29				+16
11				+21				+22				+26				+18
10				+17				+19				+20				+18
9				+12				+13				+13				+12
8				+12				+13				+13				+10
7				+ 5				+ 5				+ 5				+ 6
6				+ 6				+ 6				+ 6				+ 6
5				+ 8				+ 8				+ 8				+ 9
4				+ 7				+ 7				+ 7				+ 7
3				+ 6				+ 6				+ 6				+ 6
2				+ 3				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+149				+191				+234				+126

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Charlotte, N. C., No. 151				Asheville, N. C., No. 152				Cleveland, Tenn., No. 153				Winston-Salem, N. C., No. 154			
A	750	+ 2	0	+ 2	2199	+ 2	0	+ 2	864	+ 2	0	+ 2	932	+ 2	0	+ 2
B	750	+60	0	+ 60	2200	+ 68	0	+ 68	864	+60	0	+60	932	+64	0	+ 64
C	750	+84	0	+ 84	2200	+140	0	+140	864	+94	0	+94	932	+98	0	+ 98
D	725	+56	0	+ 56	2200	+196	- 4	+192	864	+70	- 1	+69	900	+78	0	+ 78
E	700	+24	0	+ 24	2200	+156	- 4	+152	870	+30	- 2	+28	900	+39	- 2	+ 37
F	705	+12	- 2	+ 10	2220	+ 79	- 5	+ 74	845	+13	- 3	+10	900	+13	- 3	+ 10
G	707	+ 2	- 2	0	2225	+ 41	-12	+ 29	872	+ 3	- 3	0	900	+ 3	- 3	0
H	702	+ 3	- 3	0	2162	+ 19	- 16	+ 3	834	+ 3	- 3	0	900	+ 3	- 3	0
I	701	+ 6	- 6	0	2265	+ 20	- 20	0	825	+ 8	- 8	0	900	+ 8	- 8	0
J	697	+ 1	- 8	- 7	2312	+ 5	- 21	- 16	853	0	-16	-16	900	0	-16	- 16
K	673	0	-11	-11	2590	+ 7	- 42	- 35	828	0	-20	-20	900	0	-20	- 20
L	688	0	-24	-24	2871	0	- 68	- 68	850	0	-24	-24	900	0	-24	- 24
M	595	0	-34	-34	2657	+ 5	-158	-153	1157	0	-67	-67	829	0	-16	- 46
N	669	0	-38	-38	1706	0	- 85	- 85	1394	0	-71	-71	925	0	-61	- 51
O	904	0	-50	-50	1415	0	- 74	- 74	1236	0	-65	-65	1146	0	-67	- 67
18				- 9				- 12				-10				- 10
17				- 9				-11				-10				- 10
16				- 9				-10				- 9				- 10
15				- 3				- 9				- 7				- 6
14				0				- 5				- 5				- 3
13				+ 7				- 7				- 7				- 3
12				+11				+ 2				0				+10
11				+14				+ 8				+ 5				+14
10				+16				+14				+10				+17
9				+11				+ 9				+ 6				+11
8				+ 9				+ 8				+ 6				+10
7				+ 6				+ 6				+ 6				+ 6
6				+ 6				+ 7				+ 7				+ 6
5				+ 9				+10				+10				+ 9
4				+ 7				+ 7				+ 7				+ 7
3				+ 6				+ 6				+ 6				+ 6
2				+ 3				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total..				+148				+256				+19				+124
	Knoxville, Tenn., No. 155				Bristol, Va., No. 156				Homestead, Fla., No. 157				Sebring, Fla., No. 158			
A	919	+ 2	0	+ 2	1685	+ 2	0	+ 2	14	+2	0	+ 2	112	+ 2	0	+ 2
B	919	+64	0	+64	1685	+ 68	0	+ 68	12	0	0	0	112	+26	0	+ 26
C	920	+96	0	+96	1685	+128	0	+128	14	0	0	0	115	+ 4	0	+ 4
D	920	+78	0	+78	1685	+156	0	+156	14	0	0	0	112	0	0	0
E	900	+38	- 2	+36	1700	+104	- 4	+100	14	0	0	0	100	0	0	0
F	890	+15	- 3	+12	1725	+ 55	- 5	+ 50	14	0	0	0	100	0	0	0
G	875	+ 6	- 3	+ 3	1779	+ 30	- 6	+ 24	14	0	0	0	100	0	0	0
H	903	+ 3	- 3	0	1846	+ 10	-10	0	14	0	0	0	100	0	0	0
I	905	+ 8	- 8	0	1865	+ 20	- 20	0	14	0	0	0	100	0	0	0
J	925	0	-16	-16	1825	0	- 16	- 16	14	0	0	0	100	0	0	0
K	925	0	-20	-20	1840	+ 3	- 29	- 26	2	0	0	0	100	0	0	0
L	1004	0	-24	-24	2100	0	- 51	- 51	3	0	0	0	100	0	0	0
M	1400	0	-79	-79	2371	+ 2	-139	-137	- 77	0	+ 4	+ 4	83	0	- 4	- 4
N	1719	0	-88	-88	2125	0	-110	-110	-312	0	+19	+19	68	0	- 4	- 4
O	1550	0	-86	-86	1575	0	- 87	- 87	-439	0	+21	+21	11	0	0	0
18				-13				-14				+ 5				+ 1
17				-12				-13				+ 4				+ 2
16				-11				-12				+ 4				+ 4
15				- 8				-10				+ 5				+ 6
14				- 6				- 6				+ 9				+ 9
13				- 9				- 8				+ 36				+ 29
12				- 1				+ 2				+41				+ 31
11				+ 5				+ 8				+47				+ 34
10				+11				+13				+27				+ 23
9				+ 7				+ 9				+15				+14
8				+ 6				+ 8				+16				+13
7				+ 6				+ 6				+ 6				+ 6
6				+ 7				+ 7				+ 6				+ 6
5				+10				+10				+10				+10
4				+ 7				+ 7				+ 8				+ 8
3				+ 6				+ 6				+ 6				+ 6
2				+ 3				+ 3				+ 2				+ 2
1				+ 1				+ 1				+ 1				+ 1
Total..				-13				+118				+292				+228

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Titusville, Fla., No. 159				Leesburg, Fla., No. 160				Cedar Keys, Fla., No. 161				Macon, Ga., No. 162			
A	8	+2	0	+2	100	+2	0	+2	8	+2	0	+2	326	+2	0	+2
B	8	0	0	0	95	+24	0	+24	8	0	0	0	332	+50	0	+50
C	10	0	0	0	90	+4	0	+4	4	0	0	0	326	+36	0	+36
D	10	0	0	0	80	+3	0	+3	4	0	0	0	300	+15	0	+15
E	10	0	0	0	80	0	0	0	2	0	0	0	300	+4	0	+4
F	10	0	0	0	80	0	0	0	2	0	0	0	300	0	0	0
G	10	0	0	0	80	0	0	0	2	0	0	0	300	0	-1	-1
H	10	0	0	0	80	0	0	0	2	0	0	0	350	0	-2	-2
I	10	0	0	0	80	0	0	0	2	0	0	0	350	0	-3	-3
J	10	0	0	0	80	0	0	0	2	0	0	0	400	0	-4	-4
K	10	0	0	0	80	0	0	0	2	0	0	0	400	0	-6	-6
L	15	0	0	0	80	0	0	0	2	0	0	0	400	0	-10	-10
M	6	0	0	0	92	0	-4	-4	-5	0	0	0	457	0	-26	-26
N	-35	0	0	0	59	0	-3	-3	9	0	0	0	481	0	-30	-30
O	-302	0	+17	+17	18	0	0	0	22	0	0	0	525	0	-30	-30
18				+4				0				0				-5
17				+5				0				0				-5
16				+5				+2				0				-5
15				+5				+6				+7				-3
14				+8				+8				+10				-2
13				+20				+24				+22				+1
12				+30				+26				+20				+6
11				+34				+28				+20				+11
10				+24				+21				+18				+16
9				+14				+14				+15				+10
8				+14				+12				+11				+8
7				+5				+5				+6				+7
6				+6				+6				+7				+7
5				+10				+10				+10				+10
4				+8				+8				+7				+7
3				+6				+6				+6				+6
2				+2				+2				+3				+3
1				+1				+1				+1				+1
Total..				+226				+206				+163				+67
	Albany, Ga., No. 163				Pensacola, Fla., No. 164				Opelika, Ala., No. 165				Huntsville, Ala., No. 166			
A	190	+2	0	+2	6	+1	0	+1	805	+2	0	+2	655	+2	0	+2
B	200	+40	0	+40	11	+2	0	+2	805	+60	0	+60	655	+58	0	+58
C	200	+18	0	+18	11	0	0	0	800	+88	0	+88	655	+76	0	+76
D	200	+6	0	+6	11	0	0	0	800	+63	0	+63	650	+48	0	+48
E	200	+1	0	+1		0	0	0	800	+28	0	+28	650	+16	0	+16
F	200	0	0	0		0	0	0	750	+12	-2	+10	630	+10	0	+10
G	200	0	0	0		0	0	0	754	+4	-3	+1	675	0	0	0
H	200	0	-1	-1		0	0	0	750	+3	-3	0	772	+3	-3	0
I	250	0	-2	-2		0	0	0	732	+7	-8	-1	762	+8	-8	0
J	260	0	-3	-3		0	0	0	687	0	-16	-16	738	0	-16	-16
K	300	0	-4	-4		0	0	0	650	0	-20	-20	715	0	-20	-20
L	300	0	-7	-7		0	0	0	610	0	-16	-16	742	0	-24	-24
M	261	0	-13	-13	21	0	0	0	557	0	-32	-32	839	0	-47	-47
N	208	0	-12	-12	-16	0	0	0	581	0	-31	-31	812	0	-43	-43
O	300	0	-15	-15	-158	0	+9	+9	532	0	-33	-33	711	0	-40	-40
18				-2				+1				-5				-8
17				-3				+3				-5				-7
16				-3				+3				-4				-8
15				+2				+6				-2				-6
14				+4				+8				0				-6
13				+8				+16				+2				-8
12				+8				+15				+4				-3
11				+10				+8				+7				-2
10				+16				+9				+12				+8
9				+11				+6				+8				+5
8				+9				+7				+7				+5
7				+6				+7				+6				+6
6				+7				+9				+7				+7
5				+10				+10				+10				+10
4				+7				+8				+7				+7
3				+6				+6				+6				+6
2				+3				+3				+3				+3
1				+1				+1				+1				+1
Total..				+107				+135				+167				+34

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Arkansas City, Ark., No. 167				Memphis, Tenn., No. 168				Mammoth Spring, Ark., No. 169				Hopkinsville, Ky., No. 170			
A	143	+ 2	0	+ 2	264	+ 2	0	+ 2	512	+ 2	0	+ 2	577	+ 2	0	+ 2
B	143	+32	0	+32	264	+44	0	+44	512	+56	0	+56	577	+56	0	+56
C	143	+10	0	+10	264	+28	0	+28	512	+60	0	+60	577	+68	0	+68
D	134	+ 3	0	+ 3	264	+ 6	0	+ 6	512	+30	0	+30	600	+36	0	+36
E	143	0	0	0	264	+ 4	0	+ 4	600	+16	0	+16	600	+16	0	+16
F	143	0	0	0	264	0	0	0	600	+ 5	0	+ 5	600	+ 5	0	+ 5
G	143	0	0	0	264	0	0	0	600	0	0	0	600	0	0	0
H	143	0	0	0	264	0	0	0	700	+ 3	- 3	0	600	+ 3	- 3	0
I	143	0	0	0	264	0	- 2	- 2	700	+ 2	- 6	- 4	600	+ 2	- 6	- 4
J	143	0	0	0	264	0	- 3	- 3	700	0	-11	-11	600	0	- 8	- 8
K	143	0	0	0	264	0	- 4	- 4	700	0	-14	-14	600	0	-10	-10
L	143	0	- 3	- 3	264	0	- 6	- 6	700	0	-17	-17	600	0	-12	-12
M	129	0	- 7	- 7	307	0	-15	-15	679	0	-40	-40	500	0	-28	-28
N	148	0	- 6	- 6	338	0	-20	-20	659	0	-38	-38	500	0	-32	-32
O	141	0	- 7	- 7	341	0	-19	-19	711	0	-40	-40	529	0	-29	-29
18				- 2				- 4				- 7				- 6
17				- 3				- 4				- 7				- 6
16				- 3				- 4				- 6				- 6
15				- 4				- 5				- 6				- 7
14				- 4				- 5				- 6				- 7
13				- 2				- 8				-13				-12
12				- 1				- 5				- 9				- 8
11				- 1				- 3				- 7				- 6
10				0				+ 1				- 4				+ 3
9				- 2				- 1				- 3				+ 2
8				+ 3				+ 3				+ 3				+ 4
7				+ 8				+ 7				+ 7				+ 7
6				+ 9				+ 8				+ 8				+ 8
5				+11				+10				+10				+10
4				+ 7				+ 7				+ 7				+ 7
3				+ 5				+ 5				+ 5				+ 5
2				+ 3				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total				+49				+22				-19				+50
	Danville, Ky., No. 171				Clifton Forge, Va., No. 172				Greenville, Ala., No. 173				Birmingham, Ala., No. 174			
A	983	+ 2	0	+ 2	1066	+ 2	0	+ 2	427	+ 2	0	+ 2	586	+ 2	0	+ 2
B	983	+ 64	0	+ 64	1066	+ 64	0	+ 64	427	+56	0	+56	590	+56	0	+56
C	983	+104	0	+104	1066	+108	0	+108	400	+52	0	+52	590	+72	0	+72
D	983	+ 84	0	+ 84	1066	+ 90	0	+ 90	400	+20	0	+20	590	+42	0	+42
E	983	+ 40	0	+ 40	1212	+ 49	- 2	+ 47	400	+ 8	0	+ 8	600	+16	0	+16
F	950	+19	- 3	+16	1320	+23	- 4	+19	400	0	- 1	- 1	624	+ 5	0	+ 5
G	948	+ 3	- 3	0	1350	+ 4	- 5	- 1	400	0	- 1	- 1	671	0	0	0
H	953	+ 5	- 5	0	1406	+ 6	- 8	- 2	300	0	- 2	- 2	668	+ 3	- 3	0
I	940	+10	-10	0	1515	+ 6	-14	- 8	300	0	- 2	- 2	685	+ 8	- 8	0
J	944	0	-16	-16	1850	+ 4	-20	-16	300	0	- 3	- 3	644	0	-15	-15
K	940	0	-20	-20	1920	+ 1	-31	-30	300	0	- 4	- 4	640	0	-17	-17
L	900	0	-24	-24	1946	0	-45	-45	300	0	- 7	- 7	615	0	-13	-13
M	879	0	-50	-50	1971	0	-115	-115	257	0	-15	-15	536	0	-28	-28
N	819	0	-42	-42	1888	0	-97	-97	181	0	-10	-10	531	0	-29	-29
O	907	0	-49	-49	1404	0	-75	-75	271	0	-12	-12	511	0	-25	-25
18				- 9				-11				- 2				- 5
17				- 9				-10				- 2				- 5
16				-10				-10				- 2				- 5
15				- 8				- 8				+ 1				- 5
14				- 6				- 7				+ 2				- 4
13				-11				- 8				+ 8				- 2
12				- 4				+ 5				+ 6				+ 1
11				+ 1				+11				+ 6				+ 4
10				+ 6				+16				+ 9				+ 9
9				+ 8				+10				+ 7				+ 6
8				+ 6				+10				+ 7				+ 5
7				+ 6				+ 5				+ 7				+ 7
6				+ 7				+ 6				+ 8				+ 8
5				+10				+ 8				+11				+11
4				+ 7				+ 7				+ 7				+ 7
3				+ 6				+ 6				+ 5				+ 5
2				+ 3				+ 3				+ 3				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total				+110				- 26				+163				+106

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
Lexington, Va., No. 175				Prestonsburg, Ky., No. 176				Traverse City, Mich., No. 177				Seney, Mich, No. 178				
A	1063	+ 2	0	+ 2	634	+ 2	0	+ 2	591	+ 2	0	+ 2	733	+ 2	0	+ 2
B	1063	+ 64	0	+ 64	634	+ 56	0	+ 56	591	+ 58	0	+ 58	730	+ 60	0	+ 60
C	1063	+ 108	0	+ 108	634	+ 76	0	+ 76	600	+ 72	0	+ 72	730	+ 84	0	+ 84
D	1063	+ 94	0	+ 94	750	+ 36	0	+ 36	580	+ 39	0	+ 39	730	+ 51	0	+ 51
E	1000	+ 46	- 2	+ 44	744	+ 16	0	+ 16	581	+ 16	0	+ 16	730	+ 26	- 2	+ 24
F	1030	+ 18	- 3	+ 15	860	+ 9	- 2	+ 7	572	+ 4	0	+ 4	700	+ 9	- 2	+ 7
G	1058	+ 4	- 4	0	883	+ 3	- 3	0	581	+ 0	0	0	700	+ 2	- 2	0
H	1094	+ 5	- 5	0	869	+ 4	- 4	0	609	+ 2	- 2	0	700	+ 3	- 3	0
I	1140	+ 10	- 10	0	885	+ 8	- 8	0	592	+ 5	- 5	0	700	+ 2	- 7	- 5
J	1312	+ 3	- 16	- 13	900	+ 6	- 16	- 10	609	+ 0	- 6	- 6	700	+ 1	- 10	- 9
K	1725	+ 2	- 20	- 18	880	+ 4	- 20	- 16	648	0	- 10	- 10	700	0	- 12	- 12
L	1725	0	- 43	- 43	988	0	- 24	- 24	704	0	- 17	- 17	692	0	- 16	- 16
M	1493	0	- 84	- 84	1050	0	- 59	- 59	743	0	- 41	- 41	625	0	- 35	- 35
N	1550	0	- 81	- 81	1106	0	- 56	- 56	644	0	- 33	- 33	500	0	- 28	- 28
O	1446	0	- 75	- 75	1296	0	- 69	- 69	636	0	- 37	- 37	539	0	- 27	- 27
18				- 11				- 14				- 6				- 6
17				- 10				- 14				- 6				- 7
16				- 10				- 13				- 6				- 7
15				- 7				- 10				- 7				- 7
14				- 6				- 8				- 8				- 8
13				- 8				- 10				- 16				- 16
12				+ 7				- 1				- 11				- 11
11				+ 13				+ 5				- 6				- 6
10				+ 16				+ 10				- 3				- 2
9				+ 11				+ 7				0				0
8				+ 10				+ 7				+ 5				+ 6
7				+ 5				+ 5				+ 6				+ 6
6				+ 6				+ 6				+ 7				+ 7
5				+ 8				+ 9				+ 7				+ 7
4				+ 7				+ 7				+ 6				+ 6
3				+ 6				+ 6				+ 5				+ 5
2				+ 3				+ 3				+ 5				+ 5
1				+ 1				+ 1				+ 1				+ 1
Total..				+ 54				- 45				+ 19				+ 69
Oconto, Wis., No. 179				Grand Rapids, Wis., No. 180				Winona, Minn., No. 181				Baldwin, Wis., No. 182				
A	594	+ 2	0	+ 2	1004	+ 2	0	+ 2	660	+ 2	0	+ 2	1122	+ 2	0	+ 2
B	594	+ 58	0	+ 58	1093	+ 64	0	+ 64	660	+ 58	0	+ 58	1122	+ 64	0	+ 64
C	594	+ 70	0	+ 70	1000	+ 104	0	+ 104	660	+ 76	0	+ 76	1122	+ 108	0	+ 108
D	600	+ 40	0	+ 40	1000	+ 84	0	+ 84	660	+ 48	0	+ 48	1120	+ 102	0	+ 102
E	600	+ 16	0	+ 16	1000	+ 40	0	+ 40	656	+ 20	0	+ 20	1120	+ 54	- 2	+ 52
F	600	+ 5	0	+ 5	1000	+ 19	- 2	+ 17	650	+ 7	- 2	+ 5	1100	+ 23	- 3	+ 20
G	600	+ 2	- 2	0	1000	+ 8	- 4	+ 4	775	+ 5	- 3	+ 2	1100	+ 10	- 4	+ 6
H	600	+ 3	- 3	0	1000	+ 5	- 5	0	931	+ 5	- 5	0	1100	+ 6	- 6	0
I	600	+ 6	- 6	0	1000	+ 9	- 9	0	985	+ 10	- 10	0	1100	+ 5	- 10	- 5
J	600	0	- 6	- 6	1000	0	- 12	- 12	988	0	- 10	- 10	1100	+ 2	- 12	- 10
K	590	0	- 10	- 10	975	0	- 16	- 16	985	0	- 16	- 16	1100	0	- 17	- 17
L	600	0	- 14	- 14	979	0	- 23	- 23	1004	0	- 24	- 24	1054	0	- 24	- 24
M	679	0	- 36	- 36	1029	0	- 56	- 56	993	0	- 56	- 56	921	0	- 53	- 53
N	688	0	- 37	- 37	969	0	- 48	- 48	1081	0	- 50	- 50	1006	0	- 49	- 49
O	900	0	- 53	- 53	1021	0	- 58	- 58	1096	0	- 59	- 59	1079	0	- 56	- 56
18				- 9				- 10				- 11				- 11
17				- 9				- 10				- 11				- 12
16				- 8				- 9				- 11				- 11
15				- 7				- 9				- 11				- 12
14				- 8				- 9				- 11				- 12
13				- 17				- 18				- 19				- 21
12				- 11				- 12				- 15				- 15
11				- 7				- 7				- 8				- 11
10				- 6				- 6				- 6				- 9
9				- 1				- 2				- 3				- 5
8				+ 3				+ 3				+ 3				0
7				+ 6				+ 6				+ 6				+ 6
6				+ 8				+ 8				+ 9				+ 9
5				+ 8				+ 9				+ 10				+ 10
4				+ 6				+ 6				+ 6				+ 6
3				+ 4				+ 4				+ 4				+ 4
2				+ 4				+ 4				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total..				- 7				+ 52				- 65				+ 61

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Cumberland, Wis., No. 183				Cambridge, Minn., No. 184				Brainerd, Minn., No. 185				Aberdeen, S. Dak., No. 186			
A	1246	+ 2	0	+ 2	994	+ 2	0	+ 2	1205	+ 2	0	+ 2	1299	+ 2	0	+ 2
B	1246	+ 64	0	+ 64	994	+ 64	0	+ 64	1205	+ 64	0	+ 64	1300	+ 64	0	+ 64
C	1246	+116	0	+116	994	+104	0	+104	1210	+116	0	+116	1300	+120	0	+120
D	1250	+114	0	+114	1000	+ 84	0	+ 84	1204	+108	0	+108	1300	+120	0	+120
E	1250	+ 66	- 2	+ 64	1000	+ 42	- 2	+ 40	1200	+ 62	- 2	+ 60	1300	+ 66	- 2	+ 64
F	1200	+ 24	- 4	+ 20	1000	+ 20	- 3	+ 17	1200	+ 23	- 3	+ 20	1300	+ 34	- 4	+ 30
G	1200	+ 10	- 4	+ 6	1000	+ 8	- 4	+ 4	1200	+ 10	- 4	+ 6	1305	+ 15	- 5	+ 10
H	1200	+ 6	- 6	0	1000	+ 5	- 5	0	1200	+ 12	- 6	+ 6	1305	+ 6	- 6	0
I	1200	+ 5	-11	- 6	1000	+ 9	- 9	0	1200	+ 5	-11	- 6	1304	+ 12	-12	0
J	1200	+ 3	-13	-10	1000	0	-12	-12	1200	+ 3	-13	-10	1314	0	-16	-16
K	1200	+ 2	-20	-18	1000	0	-10	-16	1200	+ 2	-20	-18	1332	0	-20	-20
L	1200	0	-29	-29	958	0	-24	-24	1200	0	-29	-29	1335	0	-32	-32
M	1100	0	-61	-61	971	0	-56	-56	1221	0	-68	-68	1354	0	-76	-76
N	1056	0	-53	-53	1050	0	-49	-49	1269	0	-65	-65	1606	0	-83	-83
O	1071	0	-58	-58	1100	0	-57	-57	1200	0	-70	-70	1586	0	-92	-92
18				-11				-11				-12				-15
17				-11				-11				-12				-15
16				-12				-12				-12				-16
15				-11				-13				-12				-16
14				-11				-13				-13				-21
13				-20				-20				-21				-34
12				-14				-15				-16				-23
11				-11				-12				-13				-21
10				-9				-9				-11				-16
9				-4				-5				-6				-8
8				0				0				-1				-3
7				+ 6				+ 6				+ 5				+ 6
6				+ 9				+ 9				+ 9				+ 9
5				+10				+10				+10				+11
4				+ 6				+ 6				+ 6				+ 7
3				+ 4				+ 4				+ 4				+ 4
2				+ 4				+ 4				+ 4				+ 5
1				+ 1				+ 1				+ 1				+ 1
Total.				+ 77				+ 20				+ 27				- 54
	Faith, S. Dak., No. 187				Marmarth, N. Dak., No. 188				Towner, N. Dak., No. 189				Crosby, N. Dak., No. 190			
A	2580	+ 2	0	+ 2	2696	+ 2	0	+ 2	1479	+ 2	0	+ 2	1962	+ 2	0	+ 2
B	2580	+ 68	0	+ 68	2700	+ 68	0	+ 68	1479	+ 64	0	+ 64	1968	+ 68	0	+ 68
C	2580	+148	0	+148	2700	+148	0	+148	1479	+124	0	+124	1970	+138	0	+138
D	2600	+221	- 3	+218	2700	+225	- 3	+222	1480	+140	- 2	+138	1970	+182	- 2	+180
E	2600	+198	- 6	+192	2700	+201	- 5	+196	1500	+ 82	- 2	+ 80	2000	+130	- 4	+126
F	2600	+108	- 8	+100	2700	+113	- 8	+105	1500	+ 39	- 4	+ 35	2000	+ 66	- 6	+ 60
G	2500	+ 47	- 9	+ 38	2700	+ 58	-10	+ 48	1500	+ 17	- 5	+ 12	2000	+ 31	- 7	+ 24
H	2500	+ 28	-12	+ 16	2700	+ 37	-13	+ 24	1500	+ 14	- 7	+ 7	2000	+ 16	-10	+ 6
I	2565	+ 25	-25	0	2800	+ 26	-26	0	1500	+ 14	-14	0	1980	+ 20	-20	0
J	2525	+ 11	-27	-16	2800	+ 10	-26	-16	1500	0	-16	-16	1969	+ 8	-20	-12
K	2500	+ 7	- 40	-33	2800	+ 10	- 46	-36	1500	0	-23	-23	1970	+ 4	-30	-26
L	2417	+ 6	- 59	-53	3033	+ 6	- 73	-67	1500	0	-36	-36	1988	+ 3	-45	-42
M	2293	+ 3	-132	-129	3193	+ 8	-188	-180	1629	0	-89	-89	1993	+ 2	-112	-110
N	2356	0	-117	-117	3000	+ 3	-158	-155	1775	0	-90	-90	2038	0	-104	-104
O	2589	0	-129	-129	2800	0	-135	-135	1721	0	-95	-95	2007	0	-100	-100
18				-29				-27				-17				-20
17				-29				-27				-16				-20
16				-28				-28				-16				-21
15				-30				-28				-18				-22
14				-31				-29				-19				-22
13				-49				-55				-36				-48
12				-31				-34				-23				-30
11				-27				-28				-19				-24
10				-18				-19				-17				-18
9				-7				-9				-11				-15
8				-1				0				-4				-2
7				+ 6				+ 6				+ 4				+ 5
6				+ 9				+ 9				+ 10				+10
5				+10				+10				+10				+ 9
4				+ 7				+ 7				+ 7				+ 7
3				+ 4				+ 4				+ 3				+ 3
2				+ 3				+ 3				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total.				+ 65				- 20				- 44				+ 8

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Crookston, Minn., No. 191				Poplar, Mont., No. 192				Miles City, Mont., No. 193				Huntley, Mont., No. 194			
A	854	+ 2	0	+ 2	1998	+ 2	0	+ 2	2351	+ 2	0	+ 2	3016	+ 2	0	+ 2
B	854	+62	0	+62	2000	+ 68	0	+ 68	2355	+ 68	0	+ 68	3020	+ 67	0	+ 67
C	854	+92	0	+92	1992	+138	0	+138	2355	+112	0	+112	3019	+154	0	+154
D	850	+69	0	+69	1992	+182	- 2	+180	2357	+207	0	+207	3018	+243	- 3	+240
E	850	+30	- 2	+28	1972	+136	- 4	+132	2375	+169	- 5	+164	2961	+232	- 8	+224
F	850	+12	- 2	+10	1968	+ 66	- 6	+ 60	2100	+ 84	- 7	+ 77	2990	+132	-10	+122
G	850	+ 6	- 3	+ 3	1978	+ 31	- 7	+ 24	2900	+ 43	-12	+ 31	3029	+ 72	-12	+ 60
H	850	+ 4	- 4	0	1985	+ 16	-10	+ 6	2700	+ 30	-16	+ 14	3075	+ 46	-16	+ 30
I	850	+ 8	- 8	0	2019	+ 20	-20	0	2800	+ 12	-20	- 8	3120	+ 24	-27	- 3
J	888	+ 1	- 9	- 8	2074	+ 6	-22	-16	2800	+ 9	-29	-20	3200	+ 15	-33	-18
K	895	0	-14	-14	2105	+ 6	-32	-26	2825	+ 6	-46	-40	3355	+ 8	-47	-39
L	925	0	-23	-23	2204	+ 5	-53	-48	2879	+ 6	-70	-64	3529	+10	-85	-75
M	950	0	-56	-56	2221	0	-124	-124	3021	+ 9	-180	-171	3664	+10	-218	-208
N	1056	0	-53	-53	2100	0	-120	-120	3156	0	-162	-162	3750	0	-192	-192
O	1229	0	-69	-69	2529	0	-117	-117	3257	0	-156	-156	4575	0	-219	-219
18				-12				-26				-31				-48
17				-12				-26				-31				-49
16				-13				-26				-34				-49
15				-13				-28				-36				-47
14				-14				-28				-37				-44
13				-25				-57				-64				-73
12				-15				-35				-38				-43
11				-14				-28				-31				-32
10				-14				-20				-20				-19
9				- 8				-12				- 8				- 6
8				- 4				+ 1				+ 3				+ 4
7				+ 4				+ 5				+ 5				+ 6
6				+10				+10				+10				+ 9
5				+10				+ 9				+ 9				+ 9
4				+ 7				+ 7				+ 7				+ 7
3				+ 3				+ 3				+ 3				+ 4
2				+ 4				+ 4				+ 4				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total				-62				- 87				-204				-222
	Lander, Wyo., No. 195				Faribault, Minn., No. 196				St. James, Minn., No. 197				Edgemont, S. Dak., No. 198			
A	5365	+ 2	0	+ 2	989	+ 2	0	+ 2	1083	+ 2	0	+ 2	3499	+ 2	0	+ 2
B	5370	+ 67	0	+ 67	989	+ 64	0	+ 64	1083	+ 64	0	+ 64	3495	+ 66	0	+ 66
C	5370	+164	- 4	+160	1000	+103	0	+103	1080	+108	0	+108	3472	+157	- 1	+156
D	5372	+306	- 6	+300	988	+ 84	0	+ 84	1072	+ 95	0	+ 95	3475	+256	- 5	+251
E	5376	+391	- 8	+383	1000	+ 42	- 3	+ 39	1075	+ 49	- 2	+ 47	3481	+273	- 8	+265
F	5400	+308	-20	+288	1025	+ 18	- 3	+ 15	1082	+ 23	- 3	+ 20	3504	+166	-10	+156
G	5483	+189	-24	+165	1016	+ 7	- 4	+ 3	1079	+ 9	- 4	+ 5	3543	+ 82	-12	+ 70
H	5569	+137	-32	+105	1042	+ 4	- 5	- 1	1069	+ 4	- 4	0	3578	+ 46	-16	+ 30
I	5815	+ 97	-43	+ 54	1075	+ 8	- 9	- 1	1088	+ 9	- 9	0	3640	+ 45	-30	+ 15
J	6125	+ 58	- 66	- 8	1103	0	-11	-11	1100	+ 1	-11	-10	3725	+ 22	-40	-18
K	6470	+ 47	-109	- 62	1112	0	-18	-18	1115	0	-16	-16	3820	+ 15	- 60	- 45
L	6875	+ 22	-158	-136	1096	0	-26	-26	1129	0	-27	-27	3838	+ 18	- 94	- 76
M	7279	+ 15	-425	-410	1079	0	-59	-59	1086	0	-60	-60	4100	+ 14	-245	-231
N	7138	+ 8	-373	-365	1050	0	-53	-53	1156	0	-57	-57	4288	+ 5	-225	-220
O	7096	0	-341	-341	1021	0	-56	-56	1225	0	-61	-61	4150	+ 6	-208	-202
18				- 68				-11				-12				-41
17				- 68				-11				-12				-41
16				- 71				-12				-12				-41
15				- 66				-13				-12				-44
14				- 61				-13				-13				-44
13				- 88				-21				-23				- 69
12				-51				-15				-15				-40
11				-37				-11				-13				-31
10				-17				- 9				-11				- 20
9				0				- 5				- 6				- 6
8				+ 8				0				- 1				+ 3
7				+ 7				+ 6				+ 6				+ 6
6				+ 9				+ 9				+ 9				+ 9
5				+ 9				+10				+10				+10
4				+ 8				+ 6				+ 6				+ 7
3				+ 5				+ 4				+ 4				+ 4
2				+ 3				+ 4				+ 4				+ 3
1				+ 1				+ 1				+ 1				+ 1
Total				-275				+ 4				+19				-115

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Dawson, Minn., No. 199				Cokato, Minn., No. 200				Wasta, S. Dak., No. 201				Moorcroft, Wyo., No. 202			
A	1059	+ 2	0	+ 2	1059	+ 2	0	+ 2	2317	+ 2	0	+ 2	4249	+ 2	0	+ 2
B	1060	+ 64	0	+ 64	1060	+ 64	0	+ 64	2320	+ 68	0	+ 68	4250	+ 68	0	+ 68
C	1052	+106	0	+106	1052	+106	0	+106	2320	+144	0	+144	4239	+162	- 2	+160
D	1058	+ 93	0	+ 93	1058	+ 90	0	+ 90	2320	+198	0	+198	4236	+282	- 6	+276
E	1050	+ 47	- 2	+ 45	1044	+ 42	- 2	+ 40	2355	+165	- 5	+160	4250	+322	- 8	+314
F	1056	+ 23	- 3	+ 20	1048	+ 23	- 3	+ 20	2400	+ 88	- 6	+ 82	4300	+222	-10	+212
G	1076	+ 9	- 4	+ 5	1048	+ 9	- 4	+ 5	2400	+ 42	- 8	+ 34	4300	+120	-12	+108
H	1081	+ 6	- 5	+ 1	1053	+ 5	- 5	0	2400	+ 21	-11	+ 10	4300	+ 72	-16	+ 56
I	1094	+ 9	- 9	0	1048	+ 9	- 9	0	2500	+ 18	-20	- 2	4300	+ 70	-40	+ 30
J	1097	+ 2	-12	-10	1041	+ 5	-11	- 6	2500	+ 7	-24	-17	4300	+ 40	-48	- 8
K	1102	0	-18	-18	1040	+ 2	-16	-14	2500	+ 5	-40	-35	4320	+ 21	-62	- 41
L	1129	0	-27	-27	1042	0	-24	-24	2400	+ 6	-62	-56	4321	+ 20	-107	- 87
M	1200	0	-66	-66	1036	0	-57	-57	2586	0	-151	-151	4657	+ 19	-272	-253
N	1331	0	-65	-65	1044	0	-53	-53	2862	+ 2	-149	-147	4588	+ 5	-240	-235
O	1350	0	-71	-71	1121	0	-56	-56	3082	0	-156	-156	4321	0	-214	-214
18				-13				-12				-31				-44
17				-12				-12				-32				-44
16				-13				-13				-32				-41
15				-14				-12				-34				-45
14				-16				-14				-35				-45
13				-27				-22				-55				-68
12				-18				-15				-33				-39
11				-16				-13				-29				-31
10				-15				-11				-18				-19
9				-7				-6				-6				-6
8				-2				-1				+1				+2
7				+6				+6				+6				+6
6				+9				+9				+9				+9
5				+10				+10				+10				+10
4				+6				+6				+7				+7
3				+4				+4				+4				+4
2				+4				+4				+3				+3
1				+1				+1				+1				+1
Total..				-32				+26				-130				+50
	Duluth, Minn., No. 203				Osage, Iowa, No. 204				Randolph, Nebr., No. 205				Valentine, Nebr., No. 206			
A	708	+ 2	0	+ 2	1167	+ 2	0	+ 2	1689	+ 2	0	+ 2	2576	+ 2	0	+ 2
B	705	+60	0	+60	1170	+ 64	0	+ 64	1684	+ 68	0	+ 68	2576	+ 68	0	+ 68
C	708	+80	0	+80	1170	+112	0	+112	1688	+132	0	+132	2576	+148	0	+148
D	752	+46	0	+46	1200	+102	0	+102	1659	+158	- 2	+156	2576	+219	- 3	+216
E	806	+22	- 2	+20	1200	+ 56	- 3	+ 53	1700	+107	- 4	+103	2575	+191	- 5	+186
F	834	+12	- 2	+10	1200	+ 23	- 4	+ 19	1700	+ 50	- 5	+ 45	2690	+106	- 8	+ 98
G	871	+ 4	- 3	+ 1	1200	+ 11	- 4	+ 7	1700	+ 18	- 6	+ 12	2575	+ 48	-12	+ 36
H	900	+ 2	- 5	- 3	1200	+ 7	- 6	+ 1	1700	+ 10	- 8	+ 2	2600	+ 32	-12	+ 20
I	932	+ 5	- 8	- 3	1180	+ 11	-11	0	1700	+ 12	-12	0	2630	+ 23	-23	0
J	969	+ 1	-11	-10	1150	+ 1	-11	-10	1631	+ 5	-16	-11	2638	+ 12	-28	-16
K	965	+ 1	-15	-14	1130	+ 1	-18	-17	1620	+ 4	-25	-21	2685	+ 11	-44	-33
L	1071	0	-25	-25	1142	+ 3	-27	-24	1617	+ 2	-39	-37	2762	+ 6	-66	-60
M	1093	0	-65	-65	1129	0	-64	-64	1514	+ 2	-88	-86	2721	+ 5	-157	-152
N	1162	0	-59	-59	1056	0	-52	-52	1512	0	-79	-79	2644	+ 5	-139	-134
O	1186	0	-67	-67	968	0	-56	-56	1539	0	-86	-86	2496	+ 3	-125	-122
18				-11				-10				-16				-25
17				-11				-10				-17				-25
16				-11				-10				-17				-25
15				-12				-11				-20				-28
14				-11				-12				-21				-28
13				-18				-20				-36				-49
12				-15				-14				-22				-29
11				-11				-11				-20				-26
10				-10				-8				-14				-17
9				-6				-4				-6				-6
8				-1				+2				+2				0
7				+5				+6				+7				+6
6				+9				+9				+9				+9
5				+9				+10				+10				+11
4				+6				+6				+7				+7
3				+4				+4				+4				+4
2				+4				+4				+4				+4
1				+1				+1				+1				+1
Total..				-103				+69				+53				+40

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Wheeling, W. Va., No. 207				Leon, Iowa, No. 208				Laurel, Md., No. 209				Harrisburg, Pa., No. 210			
A	674	+ 2	0	+ 2	1127	+ 2	0	+ 2	176	+ 2	0	+ 2	340	+ 2	0	+ 2
B	676	+59	0	+59	1130	+ 63	0	+ 63	180	+36	0	+36	344	+52	0	+52
C	676	+78	0	+78	1114	+108	0	+108	168	+16	0	+16	344	+38	0	+38
D	662	+48	0	+48	1067	+ 96	0	+ 96	162	+ 3	0	+ 3	347	+13	0	+13
E	694	+18	0	+18	1100	+ 56	- 2	+ 54	173	+ 1	0	+ 1	318	+ 9	0	+ 9
F	808	+ 9	- 2	+ 7	1100	+ 24	- 3	+ 21	206	+ 1	- 1	0	333	+ 1	- 1	0
G	873	+ 5	- 3	+ 2	1100	+ 9	- 4	+ 5	232	0	- 1	- 1	389	+ 1	- 1	0
H	978	+ 3	- 5	- 2	1100	+ 8	- 5	+ 3	251	0	- 1	- 1	386	+ 1	- 2	- 1
I	1002	+ 2	- 9	- 7	1100	+ 6	- 9	- 3	261	0	- 2	- 2	472	0	- 4	- 4
J	1059	+ 1	-12	-11	1100	+ 2	-11	- 9	262	0	- 3	- 3	542	0	- 6	- 6
K	1070	+ 1	-17	-16	1100	+ 2	-18	-16	270	0	- 4	- 4	582	0	- 9	- 9
L	1112	+ 2	-27	-25	1082	+ 2	-26	-24	265	0	- 6	- 6	604	0	-14	-14
M	1100	+ 2	-65	-63	1057	+ 1	-58	-57	186	0	-11	-11	686	0	-39	-39
N	1013	0	-51	-51	1012	0	-52	-52	262	0	-13	-13	762	0	-38	-38
O	1196	0	-60	-60	943	0	-50	-50	413	0	-21	-21	759	0	-38	-38
18				-13				- 9				- 7				-10
17				-13				- 9				- 8				-10
16				-13				- 9				- 8				- 9
15				-11				-10				- 8				- 7
14				-10				-11				- 4				- 4
13				-13				-20				+ 6				+ 3
12				- 3				-13				+14				+11
11				+ 4				-13				+18				+14
10				+ 8				-12				+17				+14
9				+ 7				- 6				+10				+ 9
8				+ 8				0				+12				+12
7				+ 6				+ 8				+ 6				+ 6
6				+ 6				+ 9				+ 6				+ 6
5				+ 8				+11				+ 7				+ 7
4				+ 7				+ 7				+ 6				+ 6
3				+ 6				+ 5				+ 6				+ 6
2				+ 3				+ 3				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total..				-34				+ 73				+73				+24
	Pittsburg, Pa., No. 211				Rockville, Md., No. 212				Upper Marlboro, Md., No. 213				Fairfax, Va., No. 214			
A	772	+ 2	0	+ 2	422	+ 2	0	+ 2	38	+ 2	0	+ 2	378	+ 2	0	+ 2
B	772	+60	0	+60	424	+56	0	+56	40	+12	0	+12	372	+53	0	+53
C	778	+87	0	+87	429	+50	0	+50	35	+ 1	0	+ 1	350	+40	0	+40
D	777	+61	- 1	+60	425	+22	0	+22	32	0	0	0	361	+16	0	+16
E	850	+26	- 2	+24	418	+ 8	0	+ 8	69	0	0	0	359	+10	- 1	+ 9
F	865	+13	- 3	+10	401	+ 3	- 1	+ 2	90	0	0	0	352	+ 2	- 1	+ 1
G	925	+ 4	- 3	+ 1	381	+ 1	- 1	0	94	0	0	0	358	+ 1	- 1	0
H	966	+ 4	- 5	- 1	385	+ 1	- 2	- 1	100	0	- 1	- 1	345	+ 1	- 2	- 1
I	990	+ 4	- 8	- 4	372	0	- 3	- 3	121	0	- 1	- 1	302	0	- 2	- 2
J	1031	+ 2	-11	- 9	365	0	- 4	- 4	124	0	- 1	- 1	275	0	- 3	- 3
K	1050	+ 1	-17	-16	368	0	- 6	- 6	140	0	- 2	- 2	262	0	- 4	- 4
L	1075	0	-26	-26	360	0	- 9	- 9	90	0	- 2	- 2	210	0	- 5	- 5
M	986	0	-58	-58	246	0	-14	-14	61	0	- 3	- 3	278	0	-16	-16
N	1200	0	-61	-61	342	0	-17	-17	157	0	- 8	- 8	370	0	-19	-19
O	1236	0	-62	-62	497	0	-25	-25	310	0	-16	-16	520	0	-26	-26
18				-11				- 7				- 6				- 7
17				-12				- 8				- 7				- 8
16				-13				- 8				- 8				- 8
15				-10				- 8				- 6				- 8
14				- 9				- 4				- 1				- 5
13				-11				+ 2				+ 7				0
12				- 1				+12				+15				+12
11				+ 4				+17				+19				+17
10				+ 9				+17				+17				+17
9				+ 7				+11				+11				+11
8				+ 9				+12				+12				+12
7				+ 6				+ 6				+ 6				+ 6
6				+ 6				+ 6				+ 6				+ 6
5				+ 8				+ 7				+ 7				+ 7
4				+ 7				+ 6				+ 6				+ 6
3				+ 6				+ 6				+ 6				+ 6
2				+ 3				+ 4				+ 4				+ 4
1				+ 1				+ 1				+ 1				+ 1
Total..				+ 5				+133				+71				+114

Mean elevations and corrections for topography and isostatic compensation, separate zones, for United States stations—Contd.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Crisfield, Md., No. 215				Fredericksburg, Va., No. 216				Dover, Del., No. 217				North Tamarack, Mich., No. 218				Hagerstown, Md., No. 219			
A	4	+1	0	+1	52	+2	0	+2	38	+2	0	+2	1215	+2	0	+2	544	+2	0	+2
B	6	0	0	0	60	+15	0	+15	42	+10	0	+10	1215	+64	0	+64	551	+56	0	+56
C	4	0	0	0	54	+2	0	+2	40	+1	0	+1	1212	+114	0	+114	556	+64	0	+64
D	4	0	0	0	47	0	0	0	38	0	0	0	1212	+111	-1	+110	559	+36	-1	+35
E	4	0	0	0	47	0	0	0	30	0	0	0	1207	+60	-3	+57	559	+17	-1	+16
F	2	0	0	0	62	0	0	0	31	0	0	0	1198	+24	-4	+20	556	+4	-2	+2
G	1	0	0	0	98	0	0	0	32	0	0	0	1148	+8	-4	+4	560	+2	-2	0
H	1	0	0	0	138	0	-1	-1	28	0	0	0	1034	+8	-5	+3	556	+1	-3	-2
I	-4	0	0	0	154	0	-1	-1	29	0	0	0	825	+7	-7	0	547	+1	-5	-4
J	-3	0	0	0	169	0	-2	-2	28	0	0	0	743	+1	-8	-7	553	0	-6	-6
K	-2	0	0	0	168	0	-3	-3	27	0	-1	-1	659	0	-11	-11	692	0	-11	-11
L	-1	0	0	0	181	0	-4	-4	28	0	-1	-1	632	0	-15	-15	771	0	-18	-18
M	-3	0	0	0	152	0	-9	-9	27	0	-1	-1	508	0	-30	-30	807	0	-47	-47
N	-6	0	0	0	297	0	-15	-15	36	0	-12	-12	572	0	-30	-30	769	0	-40	-40
O	-26	0	+1	+1	470	0	-24	-24	92	0	-5	-5	596	0	-30	-30	923	0	-46	-46
18				+4				-5				-2				-8				-10
17				+5				-7				-2				-10				-9
16				+8				-7				+1				-10				-9
15				+10				-7				+3				-9				-7
14				+12				-4				+6				-9				-6
13				+25				+4				+13				-16				-1
12				+23				+14				+16				-12				+9
11				+23				+17				+19				-8				+14
10				+18				+18				+18				-6				+16
9				+13				+12				+12				-2				+10
8				+14				+12				+14				+3				+11
7				+6				+6				+6				+6				+6
6				+6				+6				+6				+8				+6
5				+7				+8				+6				+8				+7
4				+7				+7				+6				+6				+6
3				+6				+6				+6				+4				+6
2				+3				+3				+4				+4				+4
1				+1				+1				+1				+1				+1
Total.				+192				+43				+126				+201				+55

MEAN ELEVATIONS AND CORRECTIONS FOR TOPOGRAPHY AND ISOSTATIC COMPENSATION FOR SEPARATE ZONES AT SELECTED STATIONS IN EUROPE.

No doubt the Geodetic Survey of Canada will publish the data for the separate zones at stations in that country. The publication of the "Survey of India"^a does not give the effect of topography and compensation for the separate zones in India.

For the purpose of testing the gravity height formula (see pp. 93 to 96) a number of European stations were reduced for topography and compensation by the Hayford method. The depth of compensation used was 113.7 km., the one on which the reduction tables in Special Publication No. 10 are based.

It is believed that the elevations of the topography and the corrections for the separate zones as given in the following table are of sufficient interest and value for the purposes of further investigations to warrant their publication here. As in the preceding table the corrections given in the following table are in units of the fourth decimal place in dynes. Figures printed in italics represent values interpolated from surrounding stations according to methods explained in Special Publication No. 10, pages 58 to 65, or represent values found to be identical with those for a station very close by.

^a See Survey of India, Professional Paper No. 15, "The pendulum operations in India and Burma, 1908 to 1913," by Capt. H. J. Couchman, R. E., Deputy Superintendent, Survey of India, Dehra Dun, India, 1915.

Mean elevations and corrections for topography and isostatic compensation, separate zones, for selected stations in Europe.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Stillfserjoch, Austria (Stelvio Pass), No. 1				Franzenhöhe, Austria, No. 2				Schneekoppe, Germany, No. 3				Alter Bruch, Germany, No. 4			
A	9055	+ 2	0	+ 2	7178	+ 2	0	+ 2	5266	+ 2	0	+ 2	3010	+ 2	0	+ 2
B	9050	+ 70	- 4	+ 66	7180	+ 68	0	+ 68	5250	+ 62	0	+ 62	3000	+ 62	0	+ 62
C	9080	+164	- 8	+156	7180	+164	- 4	+160	5110	+145	- 4	+141	2980	+148	0	+148
D	9160	+342	-12	+330	7410	+513	- 6	+507	4700	+262	- 6	+256	2980	+231	0	+231
E	8845	+509	-16	+493	7500	+450	-16	+434	4190	+333	- 8	+325	2990	+226	- 8	+218
F	8990	+509	-28	+481	8140	+373	-26	+347	4050	+266	-10	+256	3140	+126	-10	+116
G	8560	+369	-30	+339	8410	+259	-31	+228	3630	+150	-12	+138	3440	+ 61	-12	+ 49
H	8210	+296	-42	+254	8750	+190	-45	+145	3400	+ 98	-16	+ 82	3190	+ 28	-16	+ 12
I	7430	+251	-66	+185	7840	+164	-71	+ 93	2910	+ 80	-28	+ 52	2540	+ 35	-22	+ 13
J	7140	+140	-74	+ 66	7440	+ 90	-79	+ 11	2300	+ 35	-22	+ 13	2380	+ 20	-24	- 4
K	7280	+115	-121	- 6	7130	+ 77	-118	- 41	2070	+ 16	-20	- 4	1950	+ 9	-21	- 12
L	7300	+ 74	-174	-100	7230	+ 52	-172	-120	1860	+ 11	-38	-27	1700	+ 0	-34	- 34
M	5990	+ 60	-339	-279	5990	+ 45	-343	-298	1150	+ 14	-63	-49	1130	+ 13	-65	- 52
N	4220	+ 23	-222	-199	4220	+ 23	-223	-200	840	0	-44	-44	860	0	-45	- 45
O	2880	0	-140	-140	2880	0	-140	-140	880	0	-51	-51	900	0	-51	- 51
18				- 27				- 27				- 8				- 8
17				- 26				- 26				- 7				- 7
16				- 26				- 26				- 7				- 7
15				- 26				- 26				- 8				- 8
14				- 21				- 21				- 8				- 8
13				- 20				- 20				- 20				- 20
12				- 4				- 4				- 12				- 12
11				0				0				- 8				- 8
10				+ 1				+ 1				- 4				- 4
9				0				0				+ 2				+ 2
8				+ 6				+ 6				+ 4				+ 4
7				+ 4				+ 4				+ 4				+ 4
6				+ 2				+ 2				+ 2				+ 2
5				0				0				0				0
4				+ 3				+ 3				+ 3				+ 3
3				+ 5				+ 5				+ 5				+ 5
2				+ 5				+ 5				+ 5				+ 5
1				+ 1				+ 1				+ 1				+ 1
Total..				+1525				+873				+1096				+597
	Brocken, Germany, No. 5				Scharfenstein, Germany, No. 6				Naye, Switzerland, No. 7				Villeneuve, Switzerland, No. 8			
A	3740	+ 2	0	+ 2	2044	+ 2	0	+ 2	6520	+ 2	0	+ 2	1230	+ 2	0	+ 2
B	3740	+ 68	0	+ 68	2020	+ 61	0	+ 61	6530	+ 59	0	+ 59	1250	+ 62	0	+ 62
C	3700	+154	0	+154	1990	+133	0	+133	6430	+157	- 4	+153	1250	+111	0	+111
D	3560	+258	- 6	+252	2025	+181	0	+181	5920	+257	- 6	+251	1200	+109	0	+109
E	3240	+278	- 8	+270	2050	+143	- 7	+136	5410	+385	-11	+374	1270	+ 55	0	+ 55
F	2876	+167	-10	+157	2078	+ 70	- 8	+ 62	4710	+319	-15	+304	1720	+ 19	- 4	+ 15
G	2450	+ 85	-12	+ 73	2090	+ 33	- 9	+ 24	4300	+201	-16	+185	2360	- 10	- 7	- 17
H	2320	+ 49	-16	+ 33	2100	+ 18	-16	+ 2	4100	+140	-22	+118	2820	- 14	-16	- 30
I	1980	+ 52	-20	+ 32	1780	+ 18	-14	+ 4	3820	+111	-30	+ 81	3180	- 22	-25	- 47
J	1580	+ 21	-16	+ 5	1460	- 1	-15	-16	3390	+ 56	-35	+ 21	3420	- 8	-35	- 38
K	1170	0	-10	-10	1170	0	-13	-13	3950	+ 55	-64	- 9	3730	- 19	-57	- 76
L	900	0	-18	-18	900	0	-18	-18	4310	+ 38	-102	-64	4290	- 15	-95	-110
M	660	+ 5	-35	-30	660	0	-35	-35	4710	+ 30	-273	-243	4310	- 14	-251	-265
N	600	0	-31	-31	600	0	-31	-31	5080	+ 17	-269	-252	5080	+ 1	-272	-271
O	700	0	-38	-38	700	0	-38	-38	2700	0	-139	-139	2700	0	-139	-139
18				- 6				- 6				- 25				- 25
17				- 6				- 6				- 21				- 24
16				- 7				- 7				- 25				- 25
15				- 6				- 6				- 21				- 21
14				- 7				- 7				- 16				- 16
13				- 15				- 13				- 18				- 18
12				- 16				- 15				- 6				- 6
11				- 6				- 6				+ 1				+ 1
10				- 3				- 3				+ 1				+ 1
9				+ 3				+ 3				+ 2				+ 2
8				+ 6				+ 6				+ 5				+ 5
7				+ 4				+ 4				+ 5				+ 5
6				+ 2				+ 2				+ 4				+ 4
5				0				0				+ 1				+ 1
4				+ 3				+ 3				+ 3				+ 3
3				+ 5				+ 5				+ 4				+ 4
2				+ 5				+ 5				+ 5				+ 5
1				+ 1			+ 1	+ 1				+ 1				+ 1
Total..				+879				+414				+738				-742

Mean elevations and corrections for topography and isostatic compensation, separate zones, for selected stations in Europe—
Continued.

Zone	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation	Elevation in feet	Topography	Compensation	Topography and compensation
	Chaumont, Switzerland, No. 9				Neuenburg, Switzerland (Neuchâtel) No. 10				Gornergrat, Switzerland, No. 11				Riffelberg, Switzerland, No. 12			
A	3340	+ 2	0	+ 2	1600	+ 2	0	+ 2		+ 2	0	+ 2	8420	+ 2	0	+ 2
B	3350	+ 58	0	+ 58	1570	+ 61	0	+ 61		+ 61	0	+ 61	8400	+ 60	0	+ 60
C	3330	+146	0	+146	1540	+122	0	+122		+164	- 4	+160	8340	+156	- 4	+152
D	3270	+241	- 5	+236	1530	+148	0	+148		+323	-12	+311	8250	+326	- 9	+317
E	3080	+243	- 8	+235	1640	+ 86	- 2	+ 84		+504	-17	+487	8100	+480	-16	+464
F	2580	+144	- 8	+136	1810	+ 33	- 4	+ 34		+538	-30	+508	7590	+457	-23	+434
G	2180	+ 64	- 8	+ 56	1970	+ 16	- 6	+ 10		+402	-31	+371	7980	+336	-30	+306
H	2060	+ 35	-15	+ 20	1840	+ 11	-12	+ 1		+333	-44	+289	8660	+269	-45	+224
I	2310	+ 40	-22	+ 18	1960	+ 7	-17	+ 10		+306	-94	+212	9940	+216	-88	+128
J	2540	+ 22	-30	- 8	2430	+ 5	-27	-22		+180	-107	+ 73	10 390	+121	-108	+ 13
K	2510	+ 14	-36	-22	2480	- 10	-35	-45		+137	-146	- 9	8730	+105	-146	- 41
L	2500	+ 1	-61	-60	2520	+ 2	-63	-61		+ 80	-177	- 97	7410	+ 65	-175	-110
M	2760	+ 6	-162	-156	2760	+ 2	-162	-160		+ 82	-328	-246	5770	+ 63	-339	-276
N	3120	+ 10	-170	-160	3120	+ 4	-166	-162		+ 26	-243	-217	4550	+ 25	-244	-219
O	2960	0	-150	-150	2960	0	-150	-150		+ 2	-162	-160	2920	0	-142	-142
18				-24				-24				-32				-32
17				-24				-24				-31				-31
16				-22				-22				-23				-23
15				-20				-20				-17				-17
14				-21				-21				-11				-11
13				-23				-23				-11				-11
12				-6				-6				-6				-6
11				+ 4				+ 4				+ 3				+ 3
10				+ 2				+ 2				+ 1				+ 1
9				+ 1				+ 1				+ 3				+ 3
8				+ 5				+ 5				+ 8				+ 8
7				+ 5				+ 5				+ 6				+ 6
6				+ 4				+ 4				+ 4				+ 4
5				+ 1				+ 1				+ 1				+ 1
4				+ 3				+ 3				+ 3				+ 3
3				+ 4				+ 4				+ 4				+ 4
2				+ 5				+ 5				+ 5				+ 5
1				+ 1				+ 1				+ 1				+ 1
Total..				+246				-255				+1653				+1217
	Zermatt, Switzerland, No. 13				Belalp, Switzerland, No. 14				Brig, Switzerland, No. 15				Eggishorn, Switzerland, No. 16			
A	5260	+ 2	0	+ 2	6095	+ 2	0	+ 2	2240	+ 2	0	+ 2	7180	+ 2	0	+ 2
B	5260	+ 68	0	+ 68	6090	+ 52	0	+ 52	2250	+ 64	0	+ 64	7130	+ 64	0	+ 64
C	5280	+104	- 4	+100	6770	+142	- 4	+138	2270	+139	0	+139	7010	+145	- 4	+141
D	5490	+296	- 6	+290	6530	+289	- 6	+283	2440	+189	0	+189	6900	+293	- 6	+287
E	6230	+346	-14	+332	6310	+421	-13	+408	2680	+149	- 8	+141	6990	+442	-15	+427
F	7044	+233	-21	+212	6530	+388	-29	+359	3070	+ 72	-10	+ 62	6590	+371	-20	+351
G	7910	+116	-28	+ 88	6710	+262	-25	+237	4030	+ 17	-14	+ 3	6070	+247	-20	+227
H	8700	+ 60	-43	+ 17	6810	+175	-32	+143	5100	- 24	- 25	- 49	6240	+190	-31	+159
I	9380	+ 25	-81	-56	6990	+137	-60	+ 77	6250	- 56	- 52	-108	7120	+162	-62	+100
J	10 500	+ 6	-111	-105	6990	+ 86	-74	+ 12	6900	- 34	- 75	-109	8030	+ 84	-86	- 2
K	8860	+ 25	-149	-124	7480	+ 68	-125	- 57	7170	- 33	-119	-152	8140	+ 68	-136	- 68
L	7720	+ 19	-182	-163	6900	+ 51	-162	-111	7290	- 29	-169	-198	6210	+ 45	-140	- 95
M	6220	+ 22	-343	-321	5820	+ 40	-340	-300	5860	- 15	-343	-358	5370	+ 45	-317	-272
N	4770	+ 9	-246	-237	4250	+ 24	-230	-206	4250	+ 8	-226	-218	4060	+ 20	-218	-198
O	2920	0	-142	-142	3210	0	-157	-157	3210	0	-157	-157	3330	0	-159	-159
18				-32				-26				-26				-26
17				-31				-25				-25				-25
16				-25				-22				-22				-22
15				-17				-20				-20				-20
14				-11				-14				-14				-14
13				-11				-16				-16				-16
12				-6				-7				-7				-7
11				+ 3				+ 1				+ 1				+ 1
10				+ 1				+ 1				+ 1				+ 1
9				+ 3				+ 1				+ 1				+ 1
8				+ 8				+ 6				+ 6				+ 6
7				+ 5				+ 5				+ 5				+ 5
6				+ 4				+ 4				+ 4				+ 4
5				+ 1				+ 1				+ 1				+ 1
4				+ 3				+ 3				+ 3				+ 3
3				+ 4				+ 4				+ 4				+ 4
2				+ 5				+ 5				+ 5				+ 5
1				+ 1				+ 1				+ 1				+ 1
Total..				- 74				+791				-847				+856

Mean elevations and corrections for topography and isostatic compensation, separate zones, for selected stations in Europe—Con.

Zone	Elevation in feet	Topog- raphy	Com- pen- sation	Topog- raphy and compen- sation
Fiesch, Switzerland, No. 17.				
A	3440	+ 2	0	+ 2
B	3510	+ 50	0	+ 50
C	3510	+153	0	+153
D	3640	+253	- 6	+247
E	4020	+248	- 8	+240
F	4640	+132	- 13	+119
G	5220	+ 55	- 18	+ 37
H	6070	+ 12	- 32	- 20
I	6850	- 8	- 58	- 66
J	8020	- 16	- 85	-101
K	7920	- 20	-132	-152
L	6370	+ 5	-149	-144
M	5370	- 4	-318	-322
N	4060	+ 7	-221	-214
O	3330	0	-159	-159
18				- 26
17				- 25
16				- 22
15				- 20
14				- 14
13				- 16
12				- 7
11				+ 1
10				+ 1
9				+ 1
8				+ 6
7				+ 5
6				+ 4
5				+ 1
4				+ 3
3				+ 4
2				+ 5
1				+ 1
Total....				-428

PRINCIPAL FACTS FOR 219 STATIONS IN THE UNITED STATES.

The names of the observers, with the dates on which the observations were made, are given with the summaries of observations at the gravity stations, on pages 144 to 176.

Since the preceding report on gravity investigations (Special Publication No. 12, 1912) 94 stations have been established in the United States. At all of these stations the Mendenhall half-second pendulums were used. A description of the apparatus and of the method of determining the period of the pendulums is given in Appendix 5, Report for 1901, by G. R. Putnam, and in Appendix 1, Report for 1894. Since 1909 the flexure of the pendulum case and pier has been determined by means of the interferometer, designed and made by E. G. Fischer, chief of the instrument section of the United States Coast and Geodetic Survey. This instrument and its use are described by W. H. Burger in Appendix 6 of the Report for 1910.

Previous to 1913 the chronometer rates were determined by local observations on the stars with a portable astronomical transit. Since that date the rates of the chronometers have been determined from time transmitted by noon signals sent from the Naval Observatory at Washington over the wires of the Western Union Telegraph Company and the Postal Telegraph Company. As only the rates were required, and not the chronometer corrections, the effect of transmission time was eliminated, as it proved to be nearly the same for each day at any one station. Before making use of the Naval Observatory time it was carefully tested at the base station at the Survey office. It was also tested on the field by reoccupying four stations. The tests proved entirely satisfactory, as the results agreed closely with those previously obtained when the chronometers were rated by star observations.

An improvement was made by having a thick felt-and-leather cover for the pendulum case. This made the temperature in the case much more uniform, and no doubt added to the accuracy of the results. This covering is shown in figures 3 and 4.

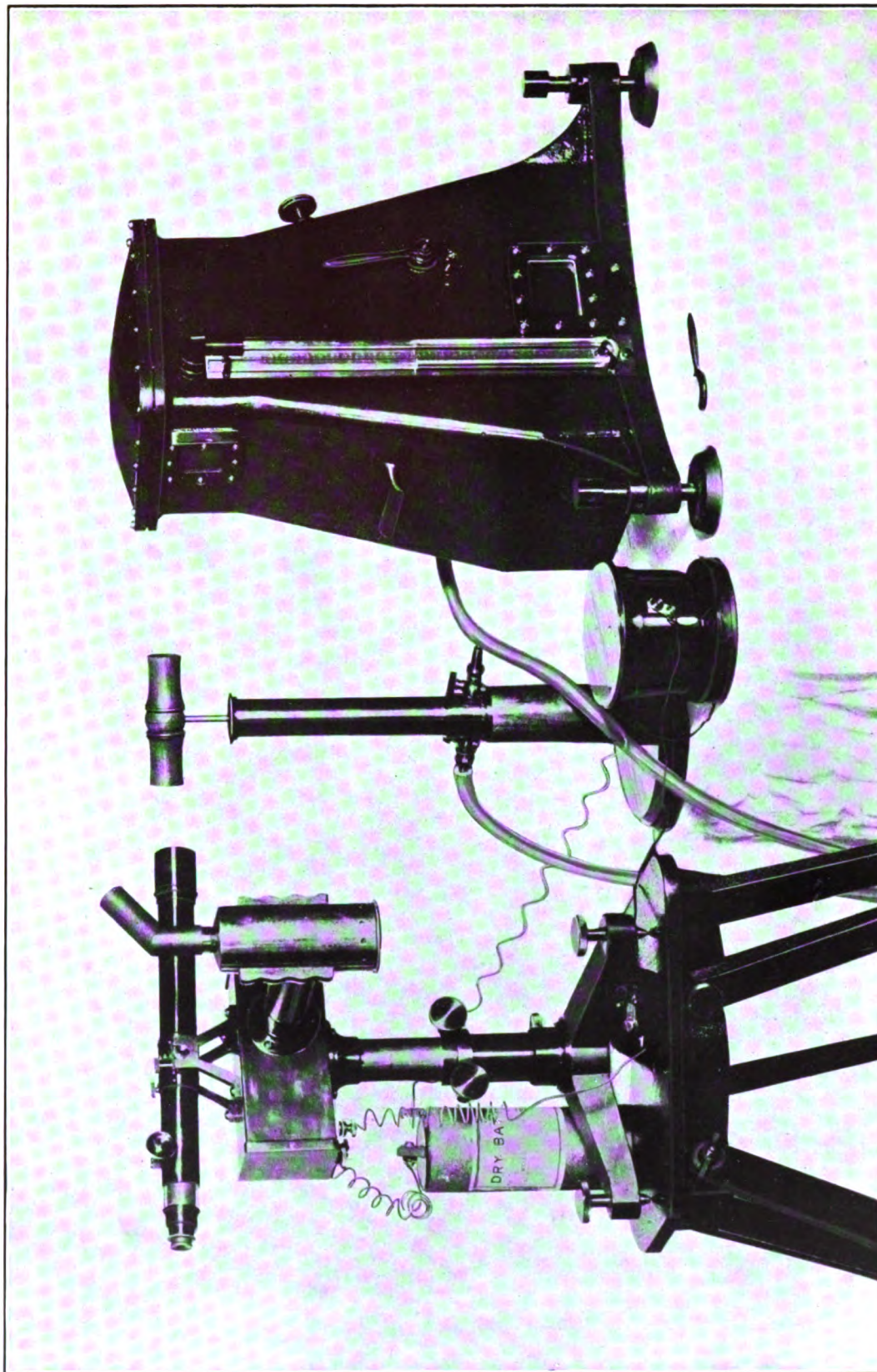


FIG. 1.—ORIGINAL FORM OF THE MENDENHALL HALF-SECOND PENDULUM APPARATUS.

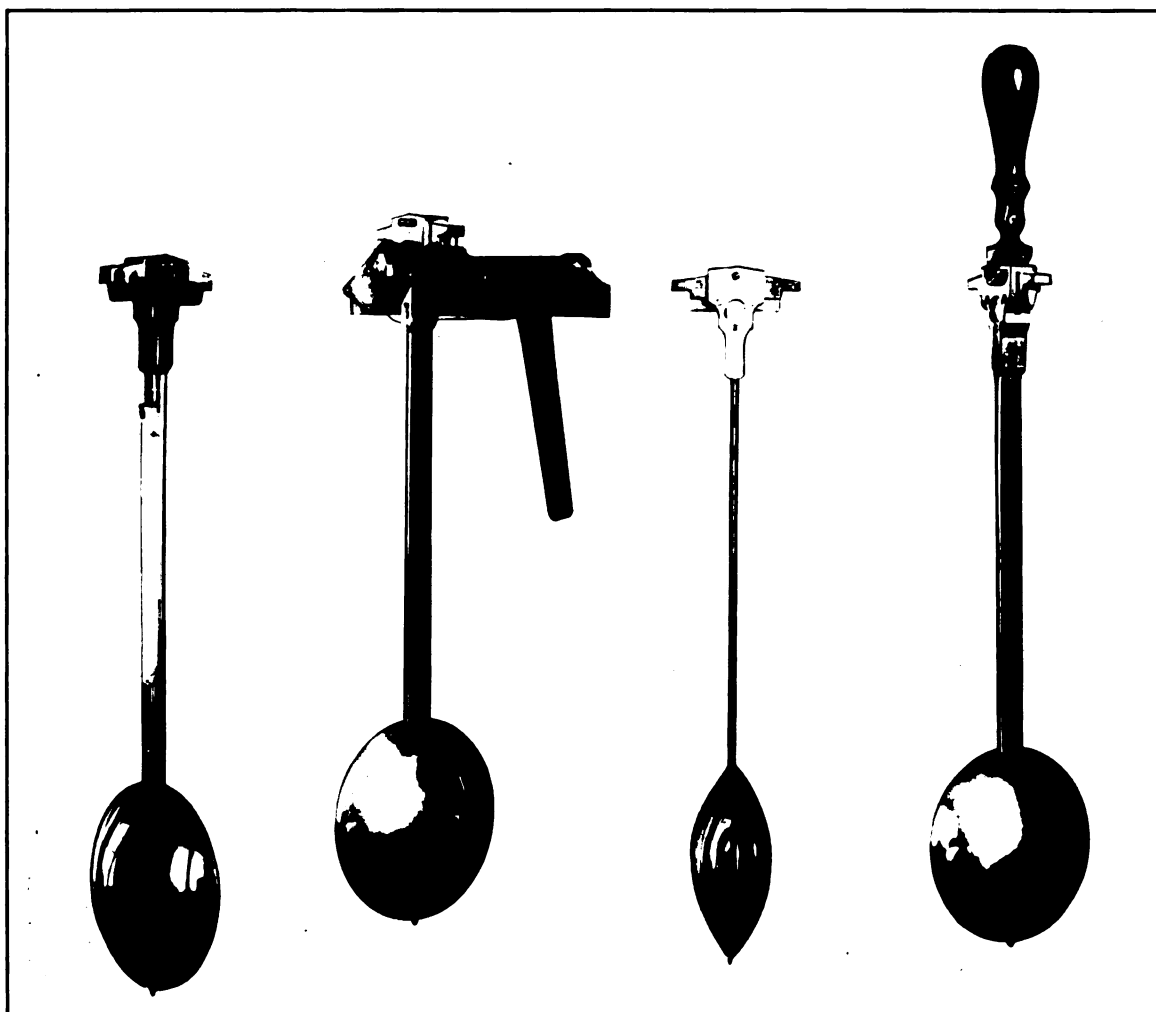


FIG. 2.—MENDENHALL HALF-SECOND PENDULUMS AS ORIGINALLY CONSTRUCTED WITH KNIFE-EDGE ATTACHED TO HEAD OF PENDULUM AND DIVIDED INTO TWO PARTS.



FIG. 3.—PRESENT PENDULUM APPARATUS SHOWING VERTICAL FORM OF TELESCOPE, ELECTRIC ILLUMINATION FOR OBSERVING SLIT, AND THE FELT-AND-LEATHER CASE FOR CONTROLLING THE TEMPERATURE.



FIG. 4.—FELT-AND-LEATHER CASE FOR TEMPERATURE CONTROL PARTLY REMOVED FROM PENDULUM RECEIVER.

Another improvement was made by changing the telescope of the flash apparatus to the vertical instead of the horizontal position, as formerly, by the use of a prism. (See fig. 3.) With the telescope vertical the observer is able to work with greater comfort, as the case is always mounted only a few inches above the floor of the room in which observations are made.

During the work at the 94 recent stations, only one of the six pendulums used gave trouble. This was pendulum No. B4. The trouble was eliminated by strengthening the connection between the stem and bob by an additional rivet.

In most cases three pendulums were used at each station. Each pendulum was swung for three periods of approximately eight hours each between two consecutive noon time-signals. The exceptions to this general rule occurred when in Mr. Powell's work on the field in the spring of 1915 pendulum No. B4 showed great irregularities. He continued that season with the other two pendulums of the set. He swung one of the pendulums for two days, or six periods of eight hours each, and the other for three such periods, making nine periods in all, the number ordinarily obtained when using three pendulums.

The pendulums were standardized at the Coast and Geodetic Survey office at Washington between each two seasons. The results of the standardizations are given on page 141.

Complete computations have been made for 219 gravity stations in the United States by three methods of reduction and the results are shown in the following table.

The theoretical value in dynes of gravity at sea level was computed by Helmert's formula of 1901 for the Potsdam system, namely:

$$\gamma_0 = 978.030 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi)$$

The correction in dynes for elevation of station was computed by the formula $-0.0003086H$, in which H is the elevation in meters. It should be carefully noted that with the sign as given this is the reduction from sea level to the station, a correction to the theoretical value not to the observed value. This correction takes account of the increased distance of the station from the attracting mass, as if the station were in the air and there were no irregularities in the earth's surface (or topography).

The corrections for topography and compensation by the Hayford method were computed with the reduction tables shown on pages 30 to 47 of Special Publication No. 10, and the resultant effect was applied as a correction to the theoretical value at sea level.

These corrections are often applied to the observed values and the results are compared with the theoretical value of gravity at sea level. The method employed in this publication and in Special Publications Nos. 10 and 12 appears to be the more logical one.

The computed value of gravity, g_0 , at the station is the theoretical value of gravity at sea level, γ_0 , corrected for elevation and for topography and compensation. It is therefore directly comparable with g , the observed value of gravity at the station. The column $g-g_0$, therefore, represents the departures of the observed values from computed values based upon the Helmert formula of 1901, upon the usual reduction for elevation, and upon the Hayford reductions that take account of topography and compensation.

All observed values, g , in the following table depend upon relative determinations with the half-second pendulums and are based on 980.112 dynes as the value of gravity at the Coast and Geodetic Survey office at Washington. This value depends upon the absolute determination of the value of gravity at Potsdam,^a Germany, and upon the adjustment of the net of base stations throughout the world. (See pp. 25 and 244 of third volume, by Dr. E. Borrass in 1911, of the Report of the Sixteenth General Conference of the International Geodetic Association at London and Cambridge in 1909.) The observations used in the adjustment to connect Washington with stations in Europe were made by G. R. Putnam in 1900.^b

^a Bestimmung der absoluten Grösse der Schwerkraft zu Potsdam mit Reversionspendeln, von Prof. F. Kühnen und Prof. Dr. Ph. Furtwängler, p. 380.

^b Determination of Relative Value of Gravity in Europe and the United States in 1900, G. R. Putnam, Appendix 5, Coast and Geodetic Survey Report, 1901, pp. 354-355.

Principal facts for 219 gravity stations in the United States.

Number and name of station	Latitude ϕ	Longitude λ	Elevation H	Theoretical gravity γ_0	Correction for elevation	Correction for topography and compensation	Computed gravity at station γ_s	Observed gravity at station γ	$\delta\gamma$
			Meters	Dynes.	Dynes.	Dynes.	Dynes.	Dynes.	Dynes.
1. Key West, Fla.	24 33.6	81 48.4	1	978.922	0.000	+0.035	978.957	978.970	+0.013
2. West Palm Beach, Fla.	26 42.8	80 02.8	2	979.073	-.001	+0.031	979.103	979.129	+0.026
3. Punta Gorda, Fla.	26 56.2	82 03	1	979.089	0.000	+0.020	979.109	979.127	+0.018
4. Apalachicola, Fla.	29 43.5	84 58.8	4	979.300	-.001	+0.015	979.314	979.322	+0.008
5. New Orleans, La.	29 57.0	90 04.2	2	979.317	-.001	+0.013	979.329	979.324	-.005
6. Rayville, La.	32 28	91 45	26	979.519	-.008	+0.008	979.519	979.543	+0.024
7. Galveston, Tex.	29 18.2	94 47.5	3	979.267	-.001	+0.007	979.273	979.272	-.001
8. Point Isabel, Tex.	26 04.7	97 12.4	8	979.028	-.002	+0.015	979.041	979.076	+0.035
9. Laredo, Tex.	27 30.5	99 31.2	129	979.131	-.040	+0.003	979.094	979.082	-.012
10. Austin, Tex. (capitol)	30 16.5	97 44.3	170	979.343	-.052	-.003	979.288	979.288	0.000
11. Austin, Tex. (university)	30 17.2	97 44.2	189	979.344	-.058	-.001	979.285	979.283	-.002
12. McAlester, Okla.	34 56.2	95 46.2	210	979.725	-.074	+0.001	979.652	979.636	-.016
13. Little Rock, Ark.	34 45.0	92 16.4	89	979.709	-.027	+0.001	979.683	979.721	+0.038
14. Columbia, Tenn.	35 36.7	87 02.5	207	979.783	-.064	+0.006	979.725	979.759	+0.034
15. Atlanta, Ga.	33 45.0	84 23.3	324	979.625	-.100	+0.014	979.539	979.524	-.015
16. McCormick, S. C.	33 54.8	82 18.0	163	979.639	-.050	+0.012	979.601	979.624	+0.023
17. Charleston, S. C.	32 47.2	79 56.0	6	979.545	-.002	+0.016	979.559	979.546	-.013
18. Beaufort, N. C.	34 43.1	76 39.8	1	979.706	0.000	+0.036	979.742	979.729	-.013
19. Charlottesville, Va.	38 02.0	78 30.3	166	979.992	-.051	+0.002	979.943	979.938	-.005
20. Deer Park, Md.	39 25.0	79 19.8	770	980.114	-.238	+0.041	979.917	979.935	+0.018
21. Washington, D. C. (Coast and Geodetic Survey Office)	38 53.2	77 00.5	14	980.067	-.004	+0.004	980.067	980.112	+0.045
22. Washington, D. C. (Smithsonian Institution)	38 53.3	77 01.5	10	980.067	-.003	+0.003	980.067	980.114	+0.047
23. Baltimore, Md.	39 17.8	76 37.3	30	980.103	-.009	+0.006	980.100	980.097	-.003
24. Philadelphia, Pa.	39 57.1	75 11.7	16	980.162	-.005	+0.009	980.166	980.196	+0.030
25. Princeton, N. J.	40 21.0	74 39.5	64	980.196	-.020	+0.013	980.189	980.178	-.011
26. Hoboken, N. J.	40 44	74 02	11	980.232	-.003	+0.008	980.237	980.269	+0.032
27. New York, N. Y.	40 48.5	73 57.7	38	980.238	-.012	+0.011	980.237	980.267	+0.030
28. Worcester, Mass.	42 16.5	71 48.5	170	980.370	-.052	+0.018	980.336	980.324	-.012
29. Boston, Mass.	42 21.6	71 03.8	22	980.377	-.007	+0.013	980.383	980.396	+0.013
30. Cambridge, Mass.	42 22.8	71 07.8	14	980.379	-.004	+0.010	980.385	980.398	+0.013
31. Calais, Me.	45 11.2	67 16.9	38	980.633	-.012	+0.010	980.631	980.631	0.000
32. Ithaca, N. Y.	42 27.1	76 29.0	247	980.386	-.076	+0.005	980.315	980.300	-.015
33. Cleveland, Ohio	41 30.4	81 36.6	210	980.301	-.065	0.000	980.236	980.241	+0.005
34. Cincinnati, Ohio	39 05.3	84 25.3	245	980.089	-.076	+0.002	980.015	980.004	-.011
35. Terre Haute, Ind.	39 28.7	87 29.8	151	980.119	-.047	+0.001	980.073	980.072	-.001
36. Chicago, Ill.	41 47.4	87 38.1	182	980.326	-.056	+0.007	980.277	980.278	+0.001
37. Madison, Wis.	43 04.6	89 24.0	270	980.442	-.083	+0.003	980.362	980.365	+0.003
38. St. Louis, Mo.	38 38.0	90 12.2	154	980.045	-.048	+0.001	979.998	980.001	+0.003
39. Kansas City, Mo.	39 05.8	94 35.4	278	980.085	-.086	-.001	979.998	979.990	-.008
40. Ellsworth, Kans.	38 43.7	98 13.5	469	980.053	-.145	-.004	979.904	979.926	+0.022
41. Wallace, Kans.	38 54.7	101 35.4	1005	980.069	-.310	0.000	979.759	979.755	-.004
42. Colorado Springs, Colo.	38 50.7	104 49.0	1841	980.064	-.508	-.007	979.489	979.490	+0.001
43. Pikes Peak, Colo.	38 50.3	105 02.0	4293	980.063	-1.325	+0.187	978.925	978.954	+0.029
44. Denver, Colo.	39 40.6	104 56.9	1638	980.137	-.505	-.015	979.617	979.609	-.008
45. Gunnison, Colo.	38 32.6	106 56.0	2340	980.037	-.722	-.001	979.314	979.342	+0.028
46. Grand Junction, Colo.	39 04.2	108 33.9	1398	980.083	-.431	-.051	979.601	979.633	+0.032
47. Green River, Utah	38 59.4	110 09.9	1243	980.076	-.384	-.043	979.649	979.636	-.013
48. Pleasant Valley Junction, Utah	39 50.8	111 00.8	2191	980.152	-.676	+0.024	979.500	979.512	+0.012
49. Salt Lake City, Utah	40 46.1	111 53.8	1322	980.234	-.408	-.041	979.785	979.843	+0.058
50. Grand Canyon, Wyo.	44 43.3	110 29.7	2386	980.591	-.736	+0.038	979.893	979.899	+0.006
51. Norris Geyser Basin, Wyo.	44 44.2	110 42.0	2276	980.592	-.702	+0.031	979.921	979.950	+0.029
52. Lower Geyser Basin, Wyo.	44 33.4	110 48.1	2200	980.576	-.679	+0.028	979.925	979.932	+0.007
53. Seattle, Wash. (university)	47 39.0	122 18.3	58	980.856	-.018	-.020	980.818	980.733	-.085
54. San Francisco, Cal.	37 47.5	122 25.7	114	979.970	-.035	+0.045	979.980	979.965	-.015
55. Mount Hamilton, Cal.	37 20.4	121 38.6	1282	979.931	-.396	+0.120	979.655	979.660	+0.005
56. Seattle, Wash. (high school)	47 36.5	122 19.8	74	980.851	-.023	-.018	980.810	980.725	-.085
57. Iron River, Mich.	46 05.4	88 38.4	458	980.714	-.141	+0.014	980.587	980.633	+0.046
58. Ely, Minn.	47 48.6	92 01.0	448	980.870	-.138	+0.008	980.740	980.771	+0.031
59. Pembina, N. Dak.	48 58.1	97 14.9	243	980.974	-.075	-.009	980.890	980.917	+0.027
60. Mitchell, S. Dak.	43 41.8	98 01.8	408	980.498	-.126	-.006	980.366	980.376	+0.009
61. Sweetwater, Tex.	32 28.4	100 24.1	655	979.519	-.202	+0.009	979.326	979.305	-.021
62. Kerrville, Tex.	30 01.3	99 07.6	498	979.323	-.154	+0.013	979.182	979.221	+0.039
63. El Paso, Tex.	31 46.3	106 29.0	1146	979.462	-.354	+0.001	979.109	979.124	+0.015
64. Nogales, Ariz.	31 21.3	110 56.6	1181	979.429	-.364	+0.038	979.103	979.061	-.042
65. Yuma, Ariz.	32 43.3	114 37.0	54	979.539	-.017	-.010	979.512	979.529	+0.017
66. Compton, Cal.	33 53.4	118 13.2	20	979.636	-.006	0.000	979.630	979.588	-.042
67. Goldfield, Nev.	37 42.2	117 14.5	1716	979.963	-.529	+0.027	979.461	979.456	-.005
68. Yavapai, Ariz.	36 03.9	112 07.1	2179	979.821	-.672	+0.034	979.183	979.192	+0.009
69. Grand Canyon, Ariz.	36 05.3	112 06.8	849	979.823	-.262	-.096	979.465	979.463	-.002
70. Gallup, N. Mex.	35 31.8	108 44.2	1990	979.775	-.614	+0.014	979.175	979.170	-.005
71. Las Vegas, N. Mex.	35 35.8	105 12.1	1960	979.781	-.605	+0.017	979.193	979.204	+0.011
72. Shamrock, Tex.	35 12.8	100 11.4	708	979.748	-.218	+0.007	979.577	979.577	0.000
73. Denison, Tex.	33 45.3	98 32.8	230	979.625	-.071	-.001	979.553	979.566	+0.013
74. Minneapolis, Minn.	44 58.7	93 13.9	256	980.614	-.070	-.005	980.530	980.597	+0.067
75. Lead, S. Dak.	44 21.1	103 45.6	1590	980.557	-.491	+0.044	980.110	980.170	+0.060

Principal facts for 219 gravity stations in the United States—Continued.

Number and name of station	Latitude ϕ	Longitude λ	Elevation H	Theoretical gravity γ_0	Correction for elevation	Correction for topography and compensation	Computed gravity at station γ_s	Observed gravity at station γ	$\gamma - \gamma_s$
	$^{\circ}$	$^{\circ}$	Meters	Dynes	Dynes	Dynes	Dynes	Dynes	Dynes
76. Bismarck, N. Dak.	46 48.5	100 47.0	516	980.779	-.159	-.005	980.615	980.625	+0.010
77. Hinsdale, Mont.	48 23.8	107 05.3	661	980.923	-.204	-.017	980.702	980.739	+0.037
78. Sandpoint, Idaho	48 16.4	116 33.3	637	980.911	-.197	-.044	980.670	980.680	+0.010
79. Boise, Idaho	43 37.2	116 12.3	821	980.491	-.253	-.042	980.196	980.212	+0.016
80. Astoria, Oreg.	46 11.3	123 50.2	1	980.724	.000	+0.008	980.732	980.727	-.005
81. Sisson, Cal.	41 18.3	122 19.6	1018	980.282	-.323	+0.015	979.974	979.972	-.002
82. Rock Springs, Wyo.	41 35.1	109 13.2	1910	980.308	-.589	-.001	979.718	979.739	+0.021
83. Paxton, Nebr.	41 07.4	101 21.3	932	980.266	-.288	+0.002	979.980	979.982	+0.002
84. Washington, D. C. (Bureau of Standards)	38 56.3	77 04.0	103	980.070	-.032	+0.012	980.050	980.095	+0.045
85. North Hero, Vt.	44 49.1	73 17.5	35	980.569	-.011	-.009	980.579	980.588	+0.009
86. Lake Placid, N. Y.	44 17.5	73 50.1	571	980.551	-.176	+0.032	980.407	980.421	+0.014
87. Potsdam, N. Y.	44 40.1	74 58.8	130	980.586	-.040	-.004	980.542	980.571	+0.029
88. Wilson, N. Y.	43 18.4	78 49.6	87	980.462	-.027	-.002	980.433	980.431	-.002
89. Alpena, Mich.	45 03.8	83 27.0	178	980.622	-.055	.000	980.567	980.555	-.012
90. Virginia Beach, Va.	36 50.5	75 58.4	4	979.888	-.001	+0.025	979.912	979.872	-.040
91. Durham, N. C.	36 00.2	78 53.5	126	979.816	-.039	+0.014	979.791	979.835	+0.044
92. Ferdinand, Fla.	30 40.2	81 27.7	3	979.374	-.001	+0.017	979.390	979.408	+0.018
93. Wilmer, Ala.	30 49.2	88 20.5	69	979.380	-.021	+0.018	979.343	979.347	+0.006
94. Aliceville, Ala.	33 07.6	88 10.8	61	979.572	-.019	+0.008	979.561	979.552	-.009
95. New Madrid, Mo.	36 35.5	89 31.6	79	979.867	-.024	+0.001	979.844	979.853	+0.009
96. Mena, Ark.	34 35.2	94 14.6	368	979.695	-.114	+0.015	979.596	979.552	-.044
97. Nacogdoches, Tex.	31 36.2	94 37.8	92	979.448	-.028	+0.008	979.427	979.421	-.006
98. Alpine, Tex.	30 21.5	103 39.7	1359	979.349	-.420	+0.033	978.962	978.991	+0.029
99. Farwell, Tex.	34 23.2	103 01.8	1250	979.678	-.388	+0.011	979.301	979.293	-.008
100. Guymon, Okla.	36 40.7	101 28.7	949	979.874	-.293	-.001	979.580	979.571	-.009
101. Helenwood, Tenn.	36 25.9	84 32.6	422	979.853	-.130	+0.015	979.738	979.786	+0.048
102. Cloudland, Tenn.	36 06.2	82 07.9	1800	979.824	-.583	+0.130	979.371	979.383	+0.012
103. Hughes, Tenn.	36 08.5	82 07.2	994	979.827	-.306	+0.053	979.574	979.553	-.021
104. Charleston, W. Va.	38 20.9	81 37.7	194	980.019	-.057	+0.010	979.952	979.936	-.016
105. State College, Pa.	40 47.9	77 51.8	358	980.237	-.110	+0.010	980.137	980.124	-.013
106. Fort Kent, Me.	47 14.9	68 36.0	160	980.818	-.049	+0.001	980.770	980.765	-.005
107. Prentice, Wis.	45 32.6	90 17.8	469	980.665	-.145	+0.010	980.530	980.562	+0.032
108. Fergus Falls, Minn.	46 17.2	96 05.0	366	980.732	-.113	+0.001	980.620	980.622	+0.002
109. Sheridan, Wyo.	44 48.0	106 58.7	1150	980.568	-.355	-.031	980.212	980.252	+0.040
110. Boulder, Mont.	46 14.2	112 07.3	1493	980.727	-.461	-.007	980.259	980.252	-.007
111. Skykomish, Wash.	47 42.4	121 22.3	280	980.860	-.086	-.047	980.727	980.707	-.020
112. Olympia, Wash.	47 03.4	122 52.7	10	980.802	-.006	-.012	980.784	980.825	+0.041
113. Heppner, Oreg.	45 21.4	119 33.2	598	980.648	-.185	-.007	980.456	980.437	-.019
114. Truckee, Cal.	39 19.6	120 11.4	1805	980.105	-.557	+0.057	979.605	979.585	-.020
115. Winnemucca, Nev.	40 58.4	117 43.8	1311	980.253	-.404	-.004	979.845	979.844	-.001
116. Ely, Nev.	39 14.9	114 53.4	1962	980.099	-.605	+0.020	979.514	979.501	-.013
117. Guernsey, Wyo.	42 16.1	104 44.0	1322	980.369	-.408	-.016	979.945	979.989	+0.044
118. Pierre, S. Dak.	44 21.9	100 20.8	454	980.558	-.140	-.013	980.405	980.427	+0.022
119. Fort Dodge, Iowa	42 30.8	94 11.4	340	980.391	-.105	+0.002	980.288	980.311	+0.023
120. Keithsburg, Ill.	41 06.4	90 57	167	980.265	-.051	-.003	980.211	980.211	0.000
121. Grand Rapids, Mich.	42 58.0	85 40.8	236	980.432	-.073	+0.003	980.362	980.372	+0.010
122. Angola, Ind.	41 37.7	85 00.6	318	980.312	-.098	+0.011	980.225	980.244	+0.019
123. Albany, N. Y.	42 39.1	73 46.1	61	980.404	-.019	-.006	980.379	980.344	-.035
124. Port Jervis, N. Y.	41 22.4	74 41.1	141	980.288	-.044	+0.003	980.247	980.222	-.025
125. Atlantic City, N. J.	39 21.9	74 25.0	3	980.110	-.001	+0.018	980.127	980.112	-.015
126. Bridgehampton, N. Y.	40 56.0	72 18.4	10	980.249	-.003	+0.020	980.266	980.252	-.014
127. Chatham, Mass.	41 40.7	69 57.3	2	980.316	-.001	+0.024	980.339	980.333	-.006
128. Rockland, Me.	44 06.3	69 06.9	9	980.535	-.003	+0.011	980.543	980.536	-.007
129. Lancaster, N. H.	44 29.5	71 34.3	261	980.570	-.081	+0.007	980.496	980.486	-.010
130. Whitehall, N. Y.	43 33.0	73 23.8	38	980.484	-.012	-.012	980.460	980.429	-.031
131. Little Falls, N. Y.	43 02.7	74 51.2	137	980.439	-.042	-.007	980.390	980.374	-.016
132. Watertown, N. Y.	43 58.3	75 54.6	147	980.522	-.045	+0.001	980.478	980.461	-.017
133. Southport, N. Y.	42 03.7	76 48.6	266	980.351	-.082	+0.004	980.273	980.251	-.022
134. Erie, Pa.	42 07.8	80 04.8	198	980.357	-.061	+0.001	980.297	980.278	-.019
135. Parkersburg, W. Va.	39 16.0	81 33.7	185	980.101	-.057	-.006	980.038	980.022	-.016
136. Columbus, Ohio	39 57.8	82 59.4	231	980.163	-.071	+0.001	980.093	980.089	-.004
137. Indianapolis, Ind.	39 45.9	86 08.8	217	980.145	-.067	+0.003	980.081	980.090	+0.009
138. Springfield, Ill.	39 47.7	89 39.5	183	980.148	-.056	+0.005	980.097	980.089	-.008
139. Lebanon, Mo.	37 41.1	92 39.1	385	979.962	-.119	+0.012	979.855	979.874	+0.019
140. Joplin, Mo.	37 05.4	94 30.8	303	979.910	-.094	+0.001	979.817	979.841	+0.024
141. Fort Smith, Ark.	35 23.3	94 25.5	135	979.763	-.042	-.007	979.714	979.706	-.008
142. Texarkana, Ark.	33 25.5	94 02.5	99	979.598	-.031	+0.001	979.568	979.587	+0.019
143. Hot Springs, Ark.	34 30.1	93 03.6	190	979.688	-.059	+0.004	979.633	979.639	+0.006
144. Alexandria, La.	31 18.6	92 26.0	24	979.425	-.007	+0.009	979.427	979.429	+0.002
145. Laurel, Miss.	31 41.5	89 02.3	77	979.456	-.024	+0.011	979.443	979.465	+0.022
146. Richmond, Va.	37 32.2	77 26.1	30	979.948	-.009	+0.010	979.949	979.960	+0.011
147. Emporia, Va.	36 40.2	77 31	37	979.873	-.011	+0.015	979.877	979.898	+0.021
148. Greenville, N. C.	35 36.8	77 22.3	17	979.783	-.005	+0.019	979.797	979.787	-.010
149. Wilmington, N. C.	34 14.2	77 56.6	9	979.646	-.003	+0.023	979.686	979.663	-.023
150. Cheraw, S. C.	34 42.0	79 54	55	979.705	-.017	+0.013	979.701	979.711	+0.010

Principal facts for 219 gravity stations in the United States—Continued.

Number and name of station	Latitude ϕ	Longitude λ	Elevation H	Theoretical gravity γ_0	Correction for elevation	Correction for topography and compensation	Computed gravity at station g_0	Observed gravity at station g	$g-g_0$
			Meters	Dynes	Dynes	Dynes	Dynes	Dynes	Dynes
151. Charlotte, N. C.	35 13.8	80 50.8	228	979.749	-0.070	+0.015	979.694	979.727	+0.033
152. Asheville, N. C.	35 35.9	82 33.3	670	979.781	-0.207	+0.026	979.600	979.603	+0.003
153. Cleveland, Tenn.	35 09.4	84 52.9	263	979.743	-0.081	+0.012	979.664	979.649	-0.015
154. Winston-Salem, N. C.	36 06.1	80 17	284	979.834	-0.088	+0.012	979.748	979.718	-0.030
155. Knoxville, Tenn.	35 57.7	83 55	280	979.812	-0.086	-0.001	979.725	979.712	-0.013
156. Bristol, Va.	36 35.4	82 12	514	979.866	-0.159	+0.012	979.719	979.712	-0.007
157. Homestead, Fla.	25 28.4	80 28.9	4	978.985	-0.001	+0.029	979.013	978.985	-0.028
158. Sebring, Fla.	27 30.2	81 27	34	979.131	-0.010	+0.023	979.144	979.135	-0.009
159. Titusville, Fla.	28 36.7	80 48.4	3	979.214	-0.001	+0.023	979.236	979.243	+0.007
160. Leesburg, Fla.	28 48.6	81 53	30	979.229	-0.009	+0.021	979.241	979.235	-0.006
161. Cedar Keys, Fla.	29 08.3	83 02.1	2	979.255	-0.001	+0.016	979.270	979.257	-0.013
162. Macon, Ga.	32 49.8	83 38	99	979.549	-0.031	+0.007	979.525	979.552	+0.027
163. Albany, Ga.	31 34.3	84 09	58	979.446	-0.018	+0.011	979.439	979.449	+0.010
164. Pensacola, Fla.	30 24.5	87 12.9	2	979.353	-0.001	+0.014	979.366	979.360	-0.006
165. Opelika, Ala.	32 38.5	85 22.8	245	979.533	-0.076	+0.017	979.474	979.456	-0.018
166. Huntsville, Ala.	34 43.8	86 35.2	200	979.707	-0.062	+0.003	979.648	979.633	-0.015
167. Arkansas City, Ark.	33 36.5	91 12.2	44	979.613	-0.014	+0.005	979.604	979.600	-0.004
168. Memphis, Tenn.	35 08.8	90 03.3	80	979.742	-0.025	+0.002	979.719	979.740	+0.021
169. Mammoth Spring, Ark.	36 29.3	91 27	156	979.857	-0.048	-0.002	979.807	979.828	+0.021
170. Hopkinsville, Ky.	36 51.6	87 28	176	979.889	-0.054	+0.006	979.841	979.855	+0.014
171. Danville, Ky.	37 38.9	84 46.4	300	979.958	-0.093	+0.011	979.876	979.855	-0.021
172. Clifton Forge, Va.	37 49.1	79 49.6	325	979.973	-0.100	-0.003	979.870	979.844	-0.026
173. Greenville, Ala.	31 49.4	86 38	130	979.466	-0.040	+0.016	979.442	979.439	-0.003
174. Birmingham, Ala.	33 30.8	86 48.8	179	979.605	-0.055	+0.011	979.561	979.536	-0.025
175. Lexington, Va.	37 47.2	79 26.6	324	979.970	-0.100	+0.005	979.875	979.859	-0.016
176. Prestonsburg, Ky.	37 40.6	82 45.6	193	979.961	-0.060	-0.004	979.897	979.881	-0.016
177. Traverse City, Mich.	44 45.8	85 37.2	180	980.595	-0.056	+0.002	980.541	980.550	+0.009
178. Seney, Mich.	46 20.8	85 57.6	223	980.738	-0.069	+0.007	980.676	980.685	+0.009
179. Oconto, Wis.	44 53.2	87 52.0	181	980.606	-0.056	-0.001	980.549	980.532	-0.017
180. Grand Rapids, Wis.	44 23.6	89 46	306	980.561	-0.094	+0.005	980.472	980.438	-0.034
181. Winona, Minn.	44 03.2	91 38.4	201	980.530	-0.062	-0.006	980.462	980.485	+0.023
182. Baldwin, Wis.	44 57.8	92 23	342	980.613	-0.106	+0.006	980.513	980.471	-0.042
183. Cumberland, Wis.	45 32.4	92 00	380	980.665	-0.117	+0.008	980.556	980.515	-0.041
184. Cambridge, Minn.	45 34.0	93 11	303	980.667	-0.094	+0.002	980.575	980.556	-0.019
185. Brainerd, Minn.	46 21.3	94 12.1	367	980.739	-0.113	+0.003	980.629	980.649	+0.020
186. Aberdeen, S. Dak.	45 27.5	98 29.0	396	980.657	-0.122	-0.005	980.530	980.550	+0.020
187. Faith, S. Dak.	45 01.3	102 04	786	980.618	-0.243	+0.006	980.381	980.404	+0.023
188. Marmarth, N. Dak.	46 18.4	103 53	822	980.734	-0.254	-0.002	980.478	980.521	+0.043
189. Townier, N. Dak.	48 20.3	100 26	451	980.917	-0.139	-0.004	980.774	980.814	+0.040
190. Crosby, N. Dak.	48 54.7	103 19	598	980.969	-0.185	+0.001	980.785	980.810	+0.025
191. Crookston, Minn.	47 46.2	96 36	260	980.866	-0.080	-0.006	980.780	980.799	+0.019
192. Poplar, Mont.	48 06.8	105 12	608	980.897	-0.188	-0.009	980.700	980.727	+0.027
193. Miles City, Mont.	46 24.2	105 50	718	980.743	-0.222	-0.020	980.501	980.539	+0.038
194. Huntley, Mont.	45 54.0	108 19.6	919	980.697	-0.284	-0.022	980.391	980.410	+0.019
195. Lander, Wyo.	42 50.0	108 43	1635	980.420	-0.505	-0.028	979.887	979.914	+0.027
196. Fairbault, Minn.	44 17.8	93 15	301	980.553	-0.093	.000	980.460	980.504	+0.044
197. St. James, Minn.	43 58.6	94 36	330	980.523	-0.102	+0.002	980.423	980.437	+0.014
198. Edgemont, S. Dak.	43 17.7	103 49.2	1066	980.462	-0.329	-0.012	980.121	980.183	+0.062
199. Dawson, Minn.	44 55.8	96 01	323	980.610	-0.100	-0.003	980.507	980.532	+0.025
200. Cokato, Minn.	45 04.5	94 12	319	980.623	-0.098	+0.003	980.528	980.542	+0.014
201. Wasta, S. Dak.	44 04.2	102 25	706	980.532	-0.218	-0.013	980.301	980.339	+0.038
202. Moorcroft, Wyo.	44 15.5	104 58	1295	980.549	-0.400	+0.005	980.154	980.183	+0.029
203. Duluth, Minn.	46 47.0	92 06.4	216	980.777	-0.067	-0.010	980.700	980.758	+0.058
204. Osage, Iowa	43 16.8	92 47	356	980.460	-0.110	+0.007	980.357	980.339	-0.018
205. Randolph, Nebr.	42 23.0	97 19	515	980.380	-0.159	+0.005	980.226	980.236	+0.010
206. Valentine, Nebr.	42 52.3	100 31	785	980.423	-0.242	+0.004	980.185	980.211	+0.026
207. Wheeling, W. Va.	40 04.0	80 43.4	205	980.172	-0.063	-0.003	980.106	980.085	-0.021
208. Leon, Iowa	40 44.6	93 43	344	980.232	-0.106	+0.007	980.133	980.133	.000
209. Laurel, Md.	39 06.3	76 51.0	54	980.086	-0.017	+0.007	980.076	980.118	+0.042
210. Harrisburg, Pa.	40 16.0	76 53.1	104	980.190	-0.032	+0.002	980.160	980.139	-0.021
211. Pittsburg, Pa.	40 27.4	80 00.6	235	980.206	-0.073	.000	980.133	980.118	-0.015
212. Rockville, Md.	39 04.9	77 08.8	129	980.084	-0.040	+0.013	980.057	980.111	+0.054
213. Upper Marlboro, Md.	38 49.0	76 45.2	12	980.061	-0.004	+0.007	980.064	980.085	+0.021
214. Fairfax, Va.	38 47.7	77 19.6	115	980.059	-0.035	+0.011	980.035	980.079	+0.044
215. Crisfield, Md.	37 58.8	75 50.7	1	979.987	.000	+0.019	980.006	979.985	-0.021
216. Fredericksburg, Va.	38 18.1	77 27.5	16	980.015	-0.005	+0.004	980.014	980.027	+0.013
217. Dover, Del.	39 09.7	75 32.0	12	980.092	-0.004	+0.013	980.101	980.099	-0.002
218. North Tamarack, Mich.	47 15.8	88 27.6	370	980.821	-0.114	+0.020	980.727	980.766	+0.039
219. Hagerstown, Md.	39 38.5	77 43.5	166	980.134	-0.051	+0.006	980.089	980.048	-0.041

GRAVITY FORMULA OF 1912.

In Special Publication No. 12 a new formula was derived which it was believed more nearly represented the conditions in the United States than did the Helmert formula of 1901. The new formula was found to be

$$\gamma_0 = 978.038 (1 + 0.005304 \sin^2 \phi - 0.000007 \sin^2 2 \phi)$$

(See p. 25, Special Publication No. 12.)

The formula advocated by the writer in that publication was the above formula modified by making the second term 0.005302, the same value as in Helmert's formula. The adopted 1912 formula is then

$$\gamma_0 = 978.038 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2 \phi)$$

The investigations made in 1912 were based upon the values of gravity in the United States computed by this formula.

In the preceding table the mean value of $g - g_0$ is +0.005 dyne and the probable error of a single value is ± 0.016 dyne. The residuals for the two Seattle stations (Nos. 53 and 56) are each -0.085 dyne, which is more than five times the probable error of a single value. This evidently indicates a very abnormal condition in the earth's crust near Seattle, and, it is believed, these two values should not be considered in taking means for the purpose of correcting the Helmert formula.

After rejecting the Seattle stations, the mean with regard to sign of $g - g_0$ is $+0.006 \pm 0.0011$ dyne. As this is more than five times its own probable error, it is believed it represents a real error in the first term of the Helmert formula. In 1912 the mean value of $g - g_0$, after rejecting Seattle, was +0.008 dyne. This was the value also found by a least square solution. As the 1912 formula would be modified by only 0.002 dyne if the mean from the above table were applied as a correction to the Helmert formula, it was thought better not to change from the 1912 value.

Later on in this volume (pp. 122 to 129) there are given various gravity formulas derived from stations in the United States and other countries from several groupings and upon different assumptions.

The 1912 anomalies used frequently in this volume were computed by the 1912 formula which is given above, the depth of compensation being 113.7 km.

The 1916 anomalies were computed by the 1916 formula for the United States and with a depth of 60 km. This formula is shown on page 123. For convenience it is inserted below.

Formula of 1916:

$$\gamma_0 = 978.040 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2 \phi)$$

A plus sign of an anomaly means that at the station in question the observed intensity of gravity is in excess of that which would occur if the assumed conditions were true as to densities of the topography, and if the compensation were complete, uniformly distributed to the depth of compensation, and directly under the topographic features. If the anomaly is negative, the observed gravity is less than it would be if the ideal conditions obtained. A part of the anomaly is due to errors in the assumed densities, to departures from the depth of compensation with which the effect of the compensation is computed, and to erroneous values for the terms in the gravity formula. Errors in the assumed elevation of the station and in the contour maps used to compute the corrections for topography and isostatic compensation also cause a small part of the anomaly, as do also errors in the observations to determine the periods of the pendulums, and slight changes in the pendulums between standardizations.

An elaborate discussion of the various sources of error is given on pages 86 to 96 of Special Publication No. 10. It is shown that the average probable error of a computed value of gravity is ± 0.003 dyne. It is not believed to be necessary to repeat that discussion of errors in this volume. The only modification of the statements made in Special Publication No. 10 that seems to be needed is discussed in connection with the correction for elevation, pages 93-96.

PRINCIPAL FACTS FOR 42 STATIONS IN CANADA.

The Geodetic Survey of Canada has recently been actively engaged in establishing gravity stations within its area, and in response to a request from the Superintendent of the United States Coast and Geodetic Survey the Director of the Canadian Survey generously placed at the author's disposal the unpublished data regarding the 42 Canadian stations. These data are given in the following table. They are used in computing gravity formulas (see pp. 113 to 131) and in the gravity anomaly maps (fig. 11, in the pocket at the end of the volume) and in a study of the relations between the anomalies and the geologic formation.

The observations and the reduction for topography and isostatic compensation were made by F. A. McDiarmid, of the Geodetic Survey of Canada.

The observed values are on the Potsdam system, and the computed values are based upon Helmert's formula of 1901 and the gravity reduction tables given on pages 30 to 47 of Special Publication No. 10. The data are therefore similar to those for the United States stations given on pages 50-52 of this volume.

Principal facts for 42 stations in Canada.

Number and name of station	Latitude ϕ	Longitude λ	Elevation H	Theoretical gravity γ_0	Correc- tion for elevation	Correc- tion for topogra- phy and compen- station	Com- puted gravity at sta- tion γ_s	Observed gravity at sta- tion γ	$\gamma - \gamma_s$	Hayford anomaly, 1912
	$^{\circ} \quad ' \quad ''$	$^{\circ} \quad ' \quad ''$	Meters	Dynes	Dynes	Dynes	Dynes	Dynes	Dynes	Dynes
1. Ottawa.....	45 23 39	5 02 52	83	980.651	-0.026	0.000	980.625	980.615	-0.010	-0.018
2. Maniwaki.....	46 22 28	5 03 55	169	980.740	-0.052	-0.001	980.687	980.685	-0.002	-0.010
3. Kingston.....	44 14 37	5 05 55	79	980.547	-0.024	+0.008	980.531	980.527	-0.004	-0.012
4. Roberval.....	48 30 54	4 48 54	107	980.933	-0.033	-0.015	980.885	980.865	-0.020	-0.028
5. Tadoussac.....	48 08 25	4 38 52	12	980.900	-0.004	-0.004	980.892	980.901	+0.009	+0.001
6. Portneuf.....	46 42 32	4 47 35	59	980.770	-0.018	+0.005	980.757	980.760	+0.003	-0.005
7. St. Jerome.....	45 46 34	4 56 00	107	980.686	-0.033	+0.006	980.659	980.678	+0.019	+0.011
8. Ste. Anne de Bellevue.....	45 24 27	4 55 46	34	980.653	-0.010	+0.003	980.646	980.660	+0.014	+0.006
9. Mattawa.....	46 18 43	5 14 49	170	980.734	-0.052	-0.013	980.669	980.647	-0.022	-0.030
10. Liskeard.....	47 30 34	5 18 41	194	980.843	-0.060	-0.004	980.779	980.785	+0.006	-0.002
11. Cochrane.....	49 03 44	5 24 05	277	980.983	-0.085	-0.004	980.894	980.880	-0.014	-0.022
12. Sault Ste. Marie.....	46 30 26	5 37 18	186	980.752	-0.057	-0.005	980.690	980.677	-0.013	-0.021
13. Chapleau.....	47 50 27	5 33 37	430	980.872	-0.133	+0.012	980.751	980.763	+0.012	+0.004
14. Port Arthur.....	48 26 00	5 56 52	189	980.926	-0.058	-0.014	980.854	980.817	-0.037	-0.045
15. Rose Point.....	45 19 02	5 20 10	183	980.644	-0.056	+0.001	980.589	980.603	+0.014	+0.006
16. Whithy.....	43 52 43	5 15 46	84	980.514	-0.026	-0.004	980.484	980.458	-0.026	-0.034
17. Woodstock, Ontario.....	43 08 33	5 23 08	299	980.448	-0.093	-0.002	980.353	980.349	-0.004	-0.012
18. Windsor.....	42 19 16	5 32 10	178	980.373	-0.055	-0.000	980.318	980.338	+0.020	+0.012
19. St. John.....	45 16 03	4 24 20	33	980.640	-0.010	+0.016	980.646	980.660	+0.014	+0.006
20. Moncton.....	46 05 04	4 19 09	14	980.713	-0.004	+0.014	980.723	980.725	+0.002	-0.006
21. Charlottetown.....	46 13 55	4 12 30	8	980.727	-0.002	+0.013	980.738	980.730	-0.008	-0.016
22. Sydney.....	46 08 21	4 00 47	12	980.719	-0.004	+0.014	980.729	980.728	-0.001	-0.009
23. Truro.....	45 21 40	4 13 06	18	980.649	-0.006	+0.014	980.657	980.659	+0.002	-0.006
24. Halifax.....	44 40 47	4 14 15	9	980.587	-0.003	+0.008	980.592	980.571	-0.021	-0.029
25. Yarmouth.....	43 50 07	4 24 29	9	980.510	-0.003	+0.014	980.521	980.540	+0.019	+0.011
26. Woodstock, New Brunswick.....	46 09 02	4 30 18	56	980.720	-0.017	+0.008	980.711	980.696	-0.015	-0.023
27. Edmundston.....	47 22 11	4 33 18	148	980.830	-0.046	-0.010	980.774	980.771	-0.003	-0.011
28. Bathurst.....	47 37 10	4 22 36	5	980.853	-0.002	-0.000	980.851	980.833	-0.018	-0.026
29. Perce.....	48 31 33	4 16 51	6	980.935	-0.002	-0.002	980.931	980.947	+0.016	+0.008
30. Kenora.....	49 46 00	6 18 00	330	981.046	-0.102	+0.018	980.962	980.971	+0.009	+0.001
31. Winnipeg.....	49 54 23	6 28 32	231	981.057	-0.071	+0.002	980.988	980.987	-0.001	-0.009
32. Brandon.....	49 50 54	6 39 47	366	981.053	-0.113	-0.002	980.938	980.953	+0.015	+0.007
33. Moose Jaw.....	50 21 26	7 02 07	541	981.101	-0.167	+0.003	980.937	980.940	+0.003	-0.005
34. Medicine Hat.....	50 02 25	7 22 40	664	981.070	-0.205	-0.002	980.863	980.865	+0.002	-0.006
35. Calgary.....	51 02 43	7 36 15	1044	981.160	-0.322	-0.022	980.816	980.820	+0.004	-0.004
36. Banff.....	51 10 53	7 42 18	1376	981.172	-0.425	-0.012	980.735	980.750	+0.015	+0.007
37. Field.....	51 23 42	7 45 59	1239	981.190	-0.382	-0.060	980.748	980.745	-0.003	-0.011
38. Revelstoke.....	50 59 48	7 52 47	453	981.155	-0.140	-0.080	980.935	980.900	-0.035	-0.043
39. Kamloops.....	50 40 42	8 01 18	352	981.127	-0.109	-0.073	980.945	980.914	-0.031	-0.039
40. North Bend.....	49 52 17	8 05 48	152	981.055	-0.047	-0.122	980.886	980.886	-0.000	-0.008
41. Glacier.....	51 15 44	7 49 58	1248	981.179	-0.385	-0.066	980.728	980.738	+0.010	+0.002
42. Vancouver.....	49 16 49	8 12 27	6	981.002	-0.002	-0.046	980.954	980.946	-0.008	-0.016

PRINCIPAL FACTS FOR 73 STATIONS IN INDIA.

In the office of the Survey of India the Hayford reductions have been made for 73 stations in that country. The data regarding them are published in a report of the Survey of India, title of which is given in a footnote on page 45.

The corrections for elevations as given in the Indian report were computed by the formula:

$$\text{Correction for elevation} = -\frac{2gH}{R}$$

in which a mean value of the radius of the earth, R , is taken as 20,900,000 feet. H is the elevation of the station in feet. These corrections are given in the column headed "Correction for elevation, Indian," in the table following. In the column headed "Correction for elevation, U. S. C. & G. S." are given the corrections computed by the formula:

$$\text{Correction for elevation} = -0.0003086 H$$

in which H is the elevation of the station in meters. The maximum difference is 0.006 dyne at station No. 95, Sandakphu. The results by the second formula have been used in the discussions in this volume, as this formula is somewhat more accurate in theory.^a

The reductions for topography and compensation were computed in much the same way as is done by the United States Coast and Geodetic Survey. For zones 18 to 1 the methods and constants are identical. For the inner zones which are lettered from A to O a slightly different gravitation constant was used. It is 657×10^{-10} for C. G. S. units, while the one used by the United States Coast and Geodetic Survey is 667.3×10^{-10} . The depth of compensation used is 70 miles, 112.65 km., instead of 113.7 km. The compensation was distributed from sea level instead of from the surface of the earth. For ocean areas the Indian Survey distributed the compensation from the bottom to a depth of 70 miles (112.65 km.) below the surface of the water, while the United States Coast and Geodetic Survey distributes the compensation from the ocean bottom to a depth of 113.7 km. below the ocean bottom.

These changes in the method of computing the topography and the compensation do not make any differences which need be considered in our discussions. We may consider the India data similar to those which we have for the United States, Canada, and Europe, all of which are based upon identical methods and constants.

In the fourth column from the last in the following table are given the gravity anomalies based upon the Hayford reduction and the Helmert formula of 1901 with 978.030 as the first term and with the Indian corrections for elevation of station. In next to the last column are given the anomalies which are similar in every way to those just mentioned except that the United States correction for elevation is applied instead of the Indian correction. The theoretical values of gravity at sea level as computed with the Helmert formula are given in the fifth column.

The observed values given in the following table are based upon the value of 979.063 dynes for Dehra Dun. The value of gravity at that station as given in the latest report of the International Geodetic Association is 979.065 dynes.

^a"Ueber die Reduction der auf der physischen Erdoberfläche beobachteten Schwereschleunigungen auf ein gemeinsames Niveau" by Helmert, Sitzungsberichte der Königlich Preussischen Akademie der Wissenschaften, volumes for 1902, p. 843, and 1903, p. 650.

Principal facts for 73 stations in India.

Number and name of station	Latitude ϕ	Longitude λ	Elevation H	Theoretical gravity γ_0	Correction elevation (Indian) Dynes	Correction for topography and compensation Dynes	Computed gravity at station γ_s	Observed gravity at station γ	$\gamma - \gamma_s$ (Indian) Dynes	Correction for elevation (U. S. C. & G. S.) Dynes	$\gamma - \gamma_s$ (U. S. C. & G. S.) Dynes	Hayford anomaly, 1912 Dynes
1. Agra.....	27 10 20	78 01 07	163	979.107	-0.050	-0.018	979.039	979.056	+0.017	-0.050	+0.017	+0.009
2. Allahabad.....	27 53 32	78 00 31	187	979.160	-0.057	-0.021	979.082	979.075	-0.007	-0.058	-0.006	-0.014
3. Amgaon.....	25 25 55	81 55	88	978.982	-0.027	-0.021	978.934	978.943	+0.009	-0.027	+0.009	+0.001
4. Amraoti.....	21 21 31	80 28	315	978.715	-0.097	-0.001	978.617	978.614	-0.003	-0.097	-0.003	-0.011
5. Arrah.....	20 55 50	77 45 40	342	978.689	-0.105	-0.001	978.583	978.609	+0.026	-0.106	+0.027	+0.019
6. Asigarh.....	25 34 10	84 39	57	978.992	-0.018	-0.028	978.946	978.918	-0.028	-0.018	-0.028	-0.036
7. Badnur.....	21 28 10	76 17 50	633	978.721	-0.194	+0.027	978.554	978.584	+0.030	-0.195	+0.031	+0.023
8. Bilaspur.....	21 54 10	77 54 10	641	978.898	-0.197	+0.018	978.569	978.607	+0.038	-0.198	+0.039	+0.031
9. Bhopal.....	23 15 58	77 25	497	978.835	-0.153	+0.007	978.689	978.711	+0.022	-0.153	+0.022	+0.014
10. Bina.....	22 03 53	82 12	268	978.758	-0.082	-0.008	978.668	978.681	+0.013	-0.083	+0.014	+0.006
11. Buxar.....	24 10 41	78 11 46	413	978.896	-0.127	-0.000	978.769	978.795	+0.026	-0.127	+0.026	+0.018
12. Chatra.....	25 34 42	83 59	63	978.992	-0.019	-0.026	978.947	978.933	-0.014	-0.019	-0.014	-0.022
13. Colaba.....	24 12 40	88 23 27	20	978.898	-0.006	-0.019	978.873	978.878	+0.005	-0.006	+0.005	-0.003
14. Cuttack.....	18 53 45	72 48 47	10	978.571	-0.003	-0.000	978.568	978.631	+0.063	-0.003	+0.063	+0.055
15. Daltonganj.....	20 29 05	85 52 01	28	978.682	-0.009	-0.000	978.653	978.659	+0.006	-0.009	+0.006	-0.002
16. Damoh.....	24 02 05	84 04	215	978.896	-0.066	-0.018	978.802	978.827	+0.025	-0.066	+0.025	+0.017
17. Dehra Dun.....	23 49 54	79 26	370	978.873	-0.114	-0.005	978.754	978.758	+0.004	-0.114	+0.004	-0.004
18. Dholpur.....	30 19 29	78 03 15	682	979.347	-0.210	-0.080	979.057	979.063	+0.006	-0.210	+0.006	-0.002
19. Ellichpur.....	26 42 01	77 54 47	176	979.072	-0.054	-0.015	979.003	978.999	-0.004	-0.054	-0.005	-0.013
20. Gaya.....	21 18 20	77 30 40	401	978.711	-0.123	-0.001	978.587	978.618	+0.031	-0.124	+0.032	+0.024
21. Gesupur.....	24 47 42	85 00	110	978.938	-0.034	-0.023	978.881	978.884	+0.003	-0.034	+0.003	-0.005
22. Goana.....	28 33 02	77 42 03	211	979.210	-0.065	-0.025	979.120	979.125	+0.005	-0.065	+0.005	-0.003
23. Gorakhpur.....	24 38 48	77 19 13	478	978.928	-0.147	+0.007	978.788	978.807	+0.019	-0.148	+0.020	+0.012
24. Gwalior.....	26 44 58	83 23	78	979.076	-0.024	-0.046	979.006	978.936	-0.070	-0.024	-0.070	-0.078
25. Hathras.....	26 13 57	78 12 49	201	979.039	-0.062	-0.012	978.965	978.958	-0.007	-0.062	-0.007	-0.015
26. Hoshangabad.....	27 36 52	78 03 22	179	979.139	-0.055	-0.020	979.064	979.075	+0.011	-0.055	+0.011	+0.003
27. Jacobabad.....	22 45 00	77 43 50	305	978.802	-0.094	-0.010	978.698	978.719	+0.021	-0.094	+0.021	+0.013
28. Jaisalmer.....	28 16 34	68 27 05	56	979.189	-0.017	-0.024	979.148	979.186	+0.038	-0.017	+0.038	+0.030
29. Jalandhar.....	31 00 00	75 33 50	232	978.693	-0.071	-0.009	978.613	978.633	+0.020	-0.071	+0.020	+0.012
30. Jammu.....	26 31 16	88 44 13	82	979.060	-0.025	-0.093	978.942	978.922	-0.020	-0.025	-0.020	-0.028
31. Japla.....	24 31 58	84 00	144	978.920	-0.044	-0.022	978.854	978.856	+0.002	-0.044	+0.002	-0.006
32. Jhansi.....	25 07 02	78 33 43	262	978.983	-0.080	-0.007	978.896	978.910	+0.014	-0.081	+0.015	+0.007
33. Jubbulpore.....	23 08 54	79 59	447	978.828	-0.137	-0.002	978.689	978.719	+0.030	-0.138	+0.031	+0.023
34. Kailana.....	29 30 55	77 39 06	247	979.284	-0.076	-0.047	979.161	979.154	-0.007	-0.076	-0.007	-0.015
35. Kailanpur.....	24 07 11	77 39 17	537	978.892	-0.165	+0.011	978.738	978.777	+0.039	-0.166	+0.040	+0.032
36. Katni.....	23 50 25	80 26	382	978.873	-0.117	-0.006	978.750	978.757	+0.007	-0.118	+0.008	-0.000
37. Khandwa.....	21 49 30	76 21 30	309	978.743	-0.095	-0.003	978.645	978.692	+0.047	-0.095	+0.047	+0.039
38. Khurja.....	28 14 19	77 51 53	198	979.186	-0.061	-0.024	979.101	979.082	-0.019	-0.061	-0.019	-0.027
39. Khatnapur.....	25 02 26	88 28 29	34	978.955	-0.011	-0.027	978.917	978.956	+0.039	-0.011	+0.039	+0.031
40. Lalitpur.....	24 41 29	78 24 26	365	978.931	-0.112	-0.003	978.816	978.814	-0.002	-0.113	-0.001	-0.009
41. Madras.....	13 04 08	80 14 54	6	978.294	-0.002	+0.040	978.332	978.279	-0.053	-0.002	-0.053	-0.061
42. Malhar.....	24 15 38	80 48	354	978.902	-0.109	-0.006	978.787	978.784	-0.003	-0.109	-0.003	-0.011
43. Majhauri Raj.....	26 17 46	83 58	67	979.043	-0.021	-0.037	978.985	978.928	-0.057	-0.021	-0.057	-0.065
44. Mhow.....	22 33 10	75 45 40	580	978.789	-0.178	+0.024	978.635	978.620	-0.015	-0.179	-0.014	-0.022
45. Mian Mir.....	31 31 37	74 22 32	216	979.442	-0.066	-0.033	979.343	979.383	+0.040	-0.067	+0.041	+0.033
46. Moghal Sarai.....	25 17 03	83 06	78	978.972	-0.024	-0.024	978.924	978.919	-0.005	-0.024	-0.005	-0.013
47. Monghyr.....	25 22 53	86 28	47	978.979	-0.014	-0.031	978.934	978.909	-0.025	-0.014	-0.025	-0.033
48. Montgomery.....	30 39 47	73 06 18	170	979.373	-0.052	-0.019	979.302	979.321	+0.019	-0.052	+0.019	+0.011
49. Mortakka.....	22 13 20	76 02 50	176	978.768	-0.054	-0.016	978.698	978.703	+0.005	-0.054	+0.005	-0.003
50. Mukhtara.....	22 23 40	75 58 40	282	978.779	-0.087	-0.009	978.683	978.664	-0.019	-0.087	-0.019	-0.027
51. Mussoorie (Camel's Back).....	30 27 35	78 04 32	2110	979.357	-0.649	+0.032	978.740	978.793	+0.053	-0.651	+0.055	+0.047
52. Muttra.....	27 29 25	77 41 48	171	979.129	-0.053	-0.019	979.057	979.072	+0.015	-0.053	+0.015	+0.007
53. Muzaffarpur.....	26 07 05	85 25	55	979.031	-0.017	-0.038	978.976	978.934	-0.042	-0.017	-0.042	-0.050
54. Ootacamund.....	11 24 37	76 42 03	2254	978.232	-0.692	+0.183	977.723	977.735	+0.012	-0.696	+0.016	+0.008
55. Pathankot.....	32 16 33	75 39 03	332	979.503	-0.101	-0.088	979.314	979.237	-0.076	-0.102	-0.075	-0.083
56. Pendra.....	22 46 41	82 00	608	978.804	-0.187	+0.013	978.630	978.638	+0.008	-0.188	+0.009	+0.001
57. Quetta.....	30 12 15	67 00 41	1682	979.337	-0.517	+0.024	978.844	978.851	+0.007	-0.519	+0.009	+0.001
58. Raipur.....	21 13 56	81 41	304	978.707	-0.093	+0.001	978.615	978.612	-0.003	-0.094	-0.002	-0.010
59. Rajpur.....	30 24 12	78 05 47	1012	979.353	-0.311	-0.086	978.976	979.002	+0.026	-0.312	+0.027	+0.019
60. Ranchi.....	23 23 05	85 19	661	978.843	-0.203	+0.021	978.661	978.691	+0.030	-0.204	+0.031	+0.023
61. Roorkee.....	29 52 20	77 53 59	264	979.311	-0.081	-0.057	979.173	979.129	-0.044	-0.081	-0.044	-0.052
62. Salem.....	11 40 05	78 09 10	289	978.241	-0.089	+0.012	978.164	978.116	-0.048	-0.089	-0.048	-0.056
63. Sandakphu.....	27 06 08	88 00 15	3586	979.102	-1.101	+0.141	978.142	978.190	+0.048	-1.107	+0.054	+0.046
64. Sasaram.....	24 57 21	83 59	104	978.949	-0.032	-0.023	978.894	978.903	+0.009	-0.032	+0.009	+0.001
65. Saugor.....	23 51 47	78 48	536	978.875	-0.165	+0.010	978.720	978.731	+0.011	-0.165	+0.011	+0.003
66. Seoni.....	22 05 29	77 29	619	978.780	-0.190	+0.016	978.586	978.622	+0.036	-0.191	+0.037	+0.029
67. Shahpur.....	22 11 30	77 54 10	392	978.766	-0.120	-0.006	978.640	978.663	+0.023	-0.121	+0.024	+0.016
68. Sibi.....	29 32 46	67 52 31	132	979.286	-0.040	-0.067	979.179	979.119	-0.059	-0.041	-0.058	-0.066
69. Siliguri.....	26 41 47	88 24 50	118	979.072	-0.036	-0.110	978.926	978.887	-0.039	-0.036	-0.039	-0.047
70. Sipri.....	25 25 52	77 39 25	467	978.982	-0.144	+0.009	978.847	978.876	+0.029	-0.144	+0.029	+0.021
71. Ujjain.....	23 11 00	75 47	491	978.830	-0.151	+0.009	978.688	978.677	-0.011	-0.152	-0.010	-0.018
72. Umaria.....	23 31 37	80 54	457	978.853	-0.140	-0.002	978.711	978.740	+0.029	-0.141	+0.030	+0.022
73. Yercaud.....	11 46 56	78 12 29	1369	978.245	-0.420	+0.116	977.941	977.908	-0.033	-0.422	-0.031	-0.039

^a The anomalies for stations 24, 83, and 100 are reproduced as given in the original source, although the data as taken from there to three decimals of a dyne and repeated here give an anomaly differing by 0.001 dyne. It is supposed that the discrepancy is due to additional decimals used in the computation but omitted in the published statement. The anomalies in other columns correspond to the values given in this column.

PRINCIPAL FACTS FOR 40 STATIONS NOT IN THE UNITED STATES PROPER, CANADA, OR INDIA.

The following table contains the principal facts for 40 stations outside of Canada, India, and the United States proper. The data for stations Nos. 1 to 36, inclusive, except the correction for topography and compensation and the resulting g_c , were obtained from the reports of the International Geodetic Association. The correction for topography and compensation of Nos. 1 to 27 was computed by the United States Coast and Geodetic Survey for depth of compensation of 113.7 km. in the usual way, and for Nos. 28 to 36 it was computed by Mr. Niethammer from Hayford's tables, and is taken from the "Procès Verbal de la 56me séance de la commission géodésique Suisse," Neuchâtel, 1910. Stations 37 to 40 are from a publication of the Royal Italian Geodetic Commission, "Determinazioni di Gravità relativa compiute nel 1912," by Reina and Cassinis, Rome, 1913. The correction for topography and isostatic compensation is there computed for a depth of 120 km. and contains the error noted in the footnote on page 98 of this publication. The error has been corrected and an approximate allowance made to change the depth to 113.7 km. The combined effect of these two changes was to reduce the anomaly in each case by 0.001 dyne.

The theoretical gravity throughout the table is based on Helmert's formula of 1901, Potsdam system.

It is intended that the several tables of principal facts (pp. 50 to 57) shall contain data for all well-observed gravity stations on land known to this Survey for which corrections, by Hayford's method, for topography and isostatic compensation have been computed for the depth 113.7 km. In the Comptes Rendus de la 17me Conférence géodésique de l'Association Géodésique Internationale, IIme Volume (Rapports Speciaux) pages 41 and 404, are given lists of corrections for topography and compensation for stations chiefly in Africa that are not included in this publication owing to lack of information as to the assumptions and methods underlying the computation.

Principal facts for 40 stations not in the United States proper, Canada, or India.

Number and name of station	Latitude ϕ	Longitude λ	Elevation H	Theoretical gravity γ_0	Correc- tion for eleva- tion	Correc- tion for topogra- phy and compen- sation	Com- puted gravity at station g_c	Observed gravity at station g	$g-g_c$	Hayford anomaly, 1912
			Meters	Dynes	Dynes	Dynes	Dynes	Dynes	Dynes	Dynes
1. St. Jostfjell (Stelvio Pass), Austria...	46 31.8	10 27.4	2760	980.755	-0.852	+0.152	980.055	980.045	-0.010	-0.018
2. Frauenthal, Austria...	46 32.0	10 29.0	2188	980.755	-0.675	+0.087	980.167	980.153	-0.014	-0.022
3. Schneekoppe, Germany...	50 44.2	15 44.6	1605	981.132	-0.495	+0.110	980.747	980.770	+0.023	+0.021
4. Alte Hirsch, Germany...	50 45.7	15 44.6	917	981.134	-0.283	+0.060	980.911	980.930	+0.019	+0.011
5. Brocken, Germany...	51 48.0	10 37.0	1140	981.226	-0.352	+0.088	980.962	981.015	+0.053	+0.045
6. Scharfenstein, Germany...	51 50.0	10 36.0	623	981.229	-0.192	+0.041	981.078	981.130	+0.052	+0.044
7. Naye, Switzerland...	46 26.0	6 58.7	1987	980.746	-0.613	+0.074	980.207	980.233	+0.026	+0.018
8. Villeneuve, Switzerland...	46 24.1	6 55.7	376	980.743	-0.116	+0.074	980.553	980.572	+0.019	+0.011
9. Chaumont, Switzerland...	47 01.4	6 57.1	1018	980.799	-0.314	+0.025	980.510	980.554	+0.044	+0.036
10. Neuenburg (Neuchâtel), Switzerland...	47 00.1	6 57.3	487	980.797	-0.150	+0.026	980.621	980.653	+0.032	+0.024
11. Gornergrat, Switzerland...	45 50.0	7 46.8	3016	980.705	-0.931	+0.165	979.939	979.992	+0.053	+0.045
12. Riffelberg, Switzerland...	45 50.6	7 45.3	2566	980.705	-0.792	+0.122	980.035	980.090	+0.055	+0.047
13. Zermatt, Switzerland...	46 01.5	7 45.0	1603	980.708	-0.495	+0.007	980.206	980.250	+0.044	+0.036
14. Belalp, Switzerland...	46 22.9	7 59.6	2132	980.741	-0.658	+0.079	980.162	980.172	+0.010	+0.012
15. Brig, Switzerland...	46 19.7	8 00.4	683	980.737	-0.211	+0.085	980.441	980.437	-0.004	-0.012
16. Eggishorn, Switzerland...	46 25.2	8 06.8	2187	980.745	-0.675	+0.086	980.156	980.169	+0.013	+0.005
17. Fiesch, Switzerland...	46 24.2	8 08.1	1049	980.743	-0.324	+0.043	980.376	980.376	0.000	0.000
18. St. Maurice, Switzerland...	46 13.0	7 00.2	422	980.726	-0.130	+0.091	980.505	980.512	+0.007	+0.001
19. Honolulu, Hawaiian Islands*	21 18.1	157 51.8	6	978.711	-0.002	+0.162	978.871	978.946	+0.075	+0.067
20. Mauna Kea, Hawaiian Islands*	19 49.2	155 28.8	3981	978.623	-1.229	+0.469	977.863	978.069	+0.206	+0.198
21. Hachinohe, Japan...	40 31	141 30	21	980.212	-0.006	+0.049	980.255	980.359	+0.104	+0.096
22. St. Georges, Bermuda*	32 21	64 40	2	979.509	-0.001	+0.218	979.726	979.806	+0.080	+0.072
23. Jamestown, St. Helena*	-15 55	5 43.7	10	978.418	-0.003	+0.177	978.502	978.712	+0.210	+0.112
24. Sorvagen, Norway...	67 53.6	13 02	19	982.478	-0.006	+0.016	982.488	982.622	+0.134	+0.126
25. Kala-i-Chumb, Turkestan...	38 27.3	70 46.5	1345	980.029	-0.415	+0.096	979.528	979.462	-0.066	-0.074
26. St. Paul Island, Alaska*	57 07.3	170 16.6	10	981.682	-0.003	+0.041	981.720	981.726	+0.006	+0.002
27. St. Michael, Alaska*	63 28.5	162 02.4	1	982.178	-0.000	+0.004	982.174	982.192	+0.018	+0.010
28. Sitten, Switzerland...	46 14.1	7 21.5	514	980.728	-0.159	+0.082	980.487	980.480	-0.007	-0.015
29. Visp, Switzerland...	46 17.6	7 53.0	649	980.733	-0.200	+0.090	980.443	980.441	-0.002	-0.010
30. Iselle, Switzerland...	46 12.5	8 12.1	630	980.725	-0.194	+0.105	980.426	980.430	+0.004	+0.004
31. Gsteig, Switzerland...	46 23.2	7 16.2	1185	980.742	-0.366	+0.001	980.375	980.395	+0.021	+0.013
32. Simplon Hospice, Switzerland...	46 14.9	8 01.9	1998	980.729	-0.617	+0.076	980.188	980.202	+0.014	+0.006
33. Grand St. Bernard, Switzerland...	45 52.1	7 10.4	2473	980.694	-0.763	+0.131	980.062	980.072	+0.010	+0.002
34. Sanetsch, Switzerland...	46 19.3	7 17.2	2041	980.736	-0.630	+0.085	980.191	980.211	+0.020	+0.012
35. Chaurion, Switzerland...	45 56.3	7 22.9	2435	980.700	-0.751	+0.113	980.062	980.107	+0.045	+0.037
36. Schwarzssee, Switzerland...	45 50.5	7 42.7	2582	980.705	-0.797	+0.125	980.033	980.090	+0.057	+0.049
37. Rome, Italy...	41 53.5	12 29.7	49	980.335	-0.015	+0.012	980.308	980.367	+0.059	+0.051
38. Florence (Arcetri), Italy...	43 45.2	11 15.2	184	980.503	-0.057	+0.023	980.423	980.491	+0.068	+0.060
39. Leghorn, Italy...	43 32.0	10 18.5	6	980.483	-0.002	+0.018	980.463	980.534	+0.071	+0.063
40. Genoa, Italy...	44 29.2	8 55	98	980.569	-0.030	+0.029	980.510	980.557	+0.047	+0.039

* This station is in west longitude.

Chapter III.—COMPARISON OF APPARENT ANOMALIES AT STATIONS IN THE UNITED STATES BY THE HAYFORD AND OLD METHODS OF REDUCTION.

In the following tables $g_0'' - \gamma_0$ and $g_0 - \gamma_0$ have the same meanings as in the reports of the International Geodetic Association.

The quantity $g_0'' - \gamma_0$ is the apparent anomaly when the Helmert formula of 1901 and the Bouguer reduction are used. The Bouguer formula has been very generally applied in reducing pendulum observations to the level of the sea. This formula is $dg = + \frac{2gH}{r} \left(1 - \frac{3\delta}{4\Delta} \right)$ where dg is the correction to observed gravity, g is gravity at sea level, H is elevation above sea level, r is radius of the earth, δ is density of matter lying above sea level, and Δ is mean density of the earth. The first term takes account of the distance from the earth's center, and the second term of the vertical attraction of the matter lying between sea level and the station, on the supposition that the latter is located on an indefinitely extended horizontal plain. Wherever the topography about a station departs materially from this condition of a horizontal plain a third term must be added to the above formula, being a correction to the second term or to observed gravity on account of such irregularities. The Bouguer reduction thus takes no account of isostatic compensation and neglects all curvature of the sea-level surface, the topography being treated as if it were standing on a plain of indefinite extent.

The quantity $g_0 - \gamma_0$ is the apparent anomaly when the Helmert formula of 1901 is used in connection with the so-called reduction to sea level in free air only ($0.0003086 H$). This reduction ignores both the topography and the isostatic compensation. It takes account simply of the increased distance of the station from the earth's center when the station is above sea level.

A comparison of the anomalies by the Hayford method, on the one hand, with those by the two older methods, as shown in the columns headed $g_0'' - \gamma_0$, and $g_0 - \gamma_0$, on the other hand, will therefore show the merits of the Hayford method of reduction in comparison with the Bouguer and the free-air methods.

This comparison of the Hayford method with the Bouguer and free-air reductions is made because the Bouguer reduction postulates a total lack of compensation and a consequent high rigidity of the earth's crust while the free-air method assumes that each piece of topography is completely compensated for at zero depth. Besides, the Bouguer and free-air methods are those which have been most generally used.

The Hayford anomalies in the following table are based upon the Coast and Geodetic Survey formula of 1912 in which the first term is 978.038.

Anomalies by Hayford, Bouguer, and free-air reductions.

Number and name of station	Anomaly			Number and name of station	Anomaly		
	Hayford, 1912	Bouguer ($g_o'' - \gamma_o$)	In free air ($g_o - \gamma_o$)		Hayford, 1912	Bouguer ($g_o'' - \gamma_o$)	In free air ($g_o - \gamma_o$)
1. Key West, Fla.	+0.005	+0.048	+0.048	76. Bismarek, N. Dak.	+0.002	-0.052	+0.005
2. West Palm Beach, Fla.	+0.018	+0.057	+0.057	77. Hinsdale, Mont.	+0.029	-0.053	+0.020
3. Punta Gorda, Fla.	+0.010	+0.038	+0.038	78. Sandpoint, Idaho.	+0.002	-0.105	-0.034
4. Apalachicola, Fla.	+0.000	+0.023	+0.023	79. Boise, Idaho.	+0.008	-0.117	-0.026
5. New Orleans, La.	-0.013	+0.008	+0.008	80. Astoria, Oreg.	-0.013	+0.003	+0.003
6. Rayville, La.	+0.016	+0.029	+0.032	81. Sisson, Cal.	-0.010	-0.103	+0.013
7. Galveston, Tex.	-0.009	+0.006	+0.006	82. Rock Springs, Wyo.	+0.013	-0.191	+0.020
8. Point Isabel, Tex.	+0.027	+0.049	+0.050	83. Paxton, Nebr.	-0.006	-0.099	+0.004
9. Laredo, Tex.	-0.020	-0.022	-0.009	84. Washington, D. C. (Bureau of Standards)	+0.037	+0.046	+0.057
10. Austin, Tex. (capitol)	-0.008	-0.021	-0.003	85. North Hero, Vt.	+0.001	-0.004	+0.000
11. Austin, Tex. (university)	-0.010	-0.023	-0.003	86. Lake Placid, N. Y.	+0.006	-0.017	+0.046
12. McAlester, Okla.	-0.027	-0.045	-0.018	87. Potsdam, N. Y.	+0.021	+0.011	+0.025
13. Little Rock, Ark.	+0.030	+0.030	+0.039	88. Wilson, N. Y.	-0.010	-0.014	-0.004
14. Columbia, Tenn.	+0.026	+0.017	+0.040	89. Alpena, Mich.	-0.020	-0.032	-0.012
15. Atlanta, Ga.	-0.023	-0.036	-0.001	90. Virginia Beach, Va.	-0.048	-0.015	-0.015
16. McCormick, S. C.	+0.015	+0.017	+0.035	91. Durham, N. C.	+0.036	+0.045	+0.058
17. Charleston, S. C.	-0.021	+0.003	+0.003	92. Fernandina, Fla.	+0.010	+0.036	+0.035
18. Beaufort, N. C.	-0.021	+0.023	+0.023	93. Wilmer, Ala.	-0.044	-0.027	-0.018
19. Charlottesville, Va.	-0.013	-0.021	-0.003	94. Aliceville, Ala.	-0.017	-0.010	-0.001
20. Deer Park, Md.	+0.010	-0.019	+0.059	95. New Madrid, Mo.	+0.001	+0.001	+0.010
21. Washington, D. C. (Coast and Geodetic Survey Office)	+0.037	+0.048	+0.049	96. Mena, Ark.	-0.052	-0.066	-0.029
22. Washington, D. C. (Smithsonian Institution)	+0.039	+0.049	+0.050	97. Nacogdoches, Tex.	-0.012	-0.005	+0.004
23. Baltimore, Md.	-0.011	+0.000	+0.003	98. Alpine, Tex.	+0.021	-0.088	+0.062
24. Philadelphia, Pa.	+0.022	+0.037	+0.039	99. Farwell, Tex.	-0.016	-0.132	+0.003
25. Princeton, N. J.	-0.019	-0.004	+0.002	100. Guymon, Okla.	-0.017	-0.110	-0.010
26. Hoboken, N. J.	+0.024	+0.039	+0.040	101. Helenwood, Tenn.	+0.040	+0.015	+0.063
27. New York, N. Y.	+0.022	+0.037	+0.041	102. Cloudland, Tenn.	+0.004	-0.042	+0.142
28. Worcester, Mass.	-0.020	-0.014	+0.006	103. Hughes, Tenn.	-0.029	-0.074	+0.032
29. Boston, Mass.	+0.005	+0.024	+0.026	104. Charleston, W. Va.	-0.024	-0.045	-0.026
30. Cambridge, Mass.	+0.005	+0.022	+0.023	105. State College, Pa.	-0.021	-0.038	-0.003
31. Calais, Me.	-0.008	+0.006	+0.010	106. Fort Kent, Me.	-0.013	-0.021	-0.004
32. Ithaca, N. Y.	-0.023	-0.033	-0.010	107. Prentice, Wis.	+0.024	-0.005	+0.042
33. Cleveland, Ohio.	-0.003	-0.016	+0.005	108. Fergus Falls, Minn.	-0.006	-0.034	+0.003
34. Cincinnati, Ohio.	-0.019	-0.034	-0.009	109. Sheridan, Wyo.	+0.032	-0.116	+0.009
35. Terre Haute, Ind.	-0.009	-0.016	+0.000	110. Boulder, Mont.	-0.015	-0.181	-0.014
36. Chicago, Ill.	-0.007	-0.012	+0.008	111. Skykomish, Wash.	-0.028	-0.087	-0.067
37. Madison, Wis.	-0.005	-0.024	+0.006	112. Olympia, Wash.	+0.033	+0.026	+0.029
38. St. Louis, Mo.	-0.005	-0.014	+0.004	113. Heppner, Oreg.	-0.027	-0.093	-0.026
39. Kansas City, Mo.	-0.016	-0.038	-0.009	114. Truckee, Cal.	-0.028	-0.162	+0.037
40. Ellsworth, Kans.	+0.014	-0.029	+0.016	115. Winnemucca, Nev.	-0.009	-0.150	-0.005
41. Wallace, Kans.	-0.012	-0.105	-0.004	116. Ely, Nev.	-0.021	-0.207	+0.007
42. Colorado Springs, Colo.	-0.007	-0.188	-0.006	117. Guernsey, Wyo.	+0.036	-0.113	+0.028
43. Pikes Peak, Colo.	+0.021	-0.204	+0.216	118. Pierre, S. Dak.	+0.014	-0.039	+0.009
44. Denver, Colo.	-0.016	-0.182	-0.023	119. Fort Dodge, Iowa.	+0.015	-0.011	+0.025
45. Gunnison, Colo.	+0.020	-0.229	+0.027	120. Keithsburg, Ill.	-0.008	-0.018	-0.003
46. Grand Junction, Colo.	+0.024	-0.158	-0.019	121. Grand Rapids, Mich.	+0.002	-0.008	+0.013
47. Green River, Utah.	-0.021	-0.180	-0.056	122. Angola, Ind.	+0.011	-0.001	+0.030
48. Pleasant Valley Junction, Utah.	+0.004	-0.187	+0.036	123. Albany, N. Y.	-0.043	-0.048	-0.041
49. Salt Lake City, Utah.	+0.010	-0.146	-0.023	124. Port Jervis, N. Y.	-0.033	-0.035	-0.022
50. Grand Canyon, Wyo.	-0.002	-0.208	+0.044	125. Atlantic City, N. J.	-0.023	+0.008	+0.003
51. Norris Geyser Basin, Wyo.	+0.021	-0.177	+0.060	126. Bridgehampton, N. Y.	-0.022	+0.005	+0.006
52. Lower Geyser Basin, Wyo.	-0.001	-0.193	+0.035	127. Chatham, Mass.	-0.014	+0.018	+0.018
53. Seattle, Wash. (university)	-0.093	-0.111	-0.105	128. Rockland, Me.	-0.015	+0.003	+0.004
54. San Francisco, Cal.	-0.023	+0.019	+0.030	129. Lancaster, N. H.	-0.018	-0.031	-0.003
55. Mount Hamilton, Cal.	-0.003	+0.003	+0.125	130. Whitehall, N. Y.	-0.039	-0.047	-0.043
56. Seattle, Wash. (high school)	-0.093	-0.111	-0.103	131. Little Falls, N. Y.	-0.024	-0.038	-0.023
57. Iron River, Mich.	+0.038	+0.009	+0.060	132. Watertown, N. Y.	-0.025	-0.032	-0.016
58. Ely, Minn.	+0.023	-0.010	+0.039	133. Southport, N. Y.	-0.030	-0.047	-0.018
59. Pembina, N. Dak.	+0.019	-0.008	+0.018	134. Erie, Pa.	-0.027	-0.040	-0.018
60. Mitchell, S. Dak.	+0.001	-0.040	+0.003	135. Parkersburg, W. Va.	-0.024	-0.042	-0.023
61. Sweetwater, Tex.	-0.029	-0.084	-0.012	136. Columbus, Ohio.	-0.012	-0.028	-0.003
62. Kerrville, Tex.	+0.031	-0.003	+0.052	137. Indianapolis, Ind.	+0.001	-0.012	+0.012
63. El Paso, Tex.	+0.007	-0.111	+0.016	138. Springfield, Ill.	-0.016	-0.023	-0.003
64. Nogales, Ariz.	-0.050	-0.132	-0.004	139. Lebanon, Mo.	+0.011	-0.012	+0.031
65. Yuma, Ariz.	+0.009	+0.001	+0.007	140. Joplin, Mo.	+0.016	-0.009	+0.025
66. Compton, Cal.	-0.050	-0.041	-0.042	141. Fort Smith, Ark.	-0.016	-0.030	-0.015
67. Goldfield, Nev.	-0.013	-0.166	+0.022	142. Texarkana, Ark.	+0.011	+0.009	+0.020
68. Yavapai, Ariz.	+0.001	-0.162	+0.043	143. Hot Springs, Ark.	+0.018	+0.009	+0.030
69. Grand Canyon, Ariz.	-0.010	-0.173	-0.008	144. Alexandria, La.	-0.006	+0.008	+0.011
70. Gallup, N. Mex.	-0.013	-0.211	+0.009	145. Laurel, Miss.	+0.014	+0.025	+0.033
71. Las Vegas, N. Mex.	+0.003	-0.189	+0.028	146. Richmond, Va.	+0.003	+0.018	+0.021
72. Shamrock, Tex.	+0.032	-0.031	+0.047	147. Emporia, Va.	+0.013	+0.032	+0.036
73. Denison, Tex.	+0.005	-0.012	+0.012	148. Greenville, N. C.	-0.018	+0.007	+0.009
74. Minneapolis, Minn.	+0.059	+0.034	+0.062	149. Wilmington, N. C.	-0.031	-0.001	-0.000
75. Lead, S. Dak.	+0.052	-0.072	+0.104	150. Cheraw, S. C.	+0.002	+0.017	+0.023

Anomalies by Hayford, Bouguer, and free-air reductions—Continued.

Number and name of station	Anomaly			Number and name of station	Anomaly		
	Hayford, 1912	Bouguer ($g_0'' - \gamma_0$)	In free air ($g_0 - \gamma_0$)		Hayford, 1912	Bouguer ($g_0'' - \gamma_0$)	In free air ($g_0 - \gamma_0$)
151. Charlotte, N. C.	+0.025	+0.023	+0.048	186. Aberdeen, S. Dak.	+0.012	-0.029	+0.015
152. Asheville, N. C.	-0.005	-0.045	+0.029	187. Faith, S. Dak.	+0.015	-0.058	+0.029
153. Cleveland, Tenn.	-0.023	-0.041	-0.013	188. Marmarth, N. Dak.	+0.035	-0.061	+0.041
154. Winston-Salem, N. C.	-0.038	-0.049	-0.018	189. Towner, N. Dak.	+0.032	-0.014	+0.036
155. Knoxville, Tenn.	-0.021	-0.045	-0.014	190. Crosby, N. Dak.	+0.017	-0.041	+0.026
156. Bristol, Va.	-0.015	-0.052	+0.005	191. Crookston, Minn.	+0.011	-0.016	+0.013
157. Homestead, Fla.	-0.036	+0.001	+0.001	192. Poplar, Mont.	+0.019	-0.050	+0.018
158. Sebring, Fla.	-0.017	+0.011	+0.014	193. Miles City, Mont.	+0.030	-0.061	+0.018
159. Titusville, Fla.	-0.001	+0.030	+0.030	194. Huntley, Mont.	+0.011	-0.105	-0.003
160. Leesburg, Fla.	-0.014	+0.012	+0.015	195. Lander, Wyo.	+0.019	-0.182	-0.001
161. Cedar Keys, Fla.	-0.021	+0.003	+0.003	196. Faribault, Minn.	+0.036	+0.011	+0.044
162. Macon, Ga.	+0.019	+0.023	+0.034	197. St. James, Minn.	+0.006	-0.020	+0.016
163. Albany, Ga.	+0.002	+0.015	+0.021	198. Edgemont, S. Dak.	+0.064	-0.067	+0.050
164. Pensacola, Fla.	-0.014	+0.008	+0.008	199. Dawson, Minn.	+0.017	-0.014	+0.020
165. Opelika, Ala.	-0.026	-0.028	-0.001	200. Cokato, Minn.	+0.006	-0.019	+0.017
166. Huntsville, Ala.	-0.023	-0.034	-0.012	201. Wasta, S. Dak.	+0.030	-0.052	+0.025
167. Arkansas City, Ark.	-0.012	-0.004	+0.001	202. Moorcroft, Wyo.	+0.021	-0.109	+0.034
168. Memphis, Tenn.	+0.013	+0.015	+0.023	203. Duluth, Minn.	+0.050	+0.025	+0.048
169. Mammoth Spring, Ark.	+0.013	+0.002	+0.019	204. Osage, Iowa	-0.026	-0.050	-0.011
170. Hopkinsville, Ky.	+0.006	+0.001	+0.020	205. Randolph, Nebr.	+0.002	-0.042	+0.015
171. Danville, Ky.	-0.030	-0.043	-0.010	206. Valentine, Nebr.	+0.018	-0.058	+0.030
172. Clifton Forge, Va.	-0.034	-0.085	-0.029	207. Wheeling, W. Va.	-0.029	-0.047	-0.024
173. Greenville, Ala.	-0.011	-0.001	+0.013	208. Leon, Iowa	-0.008	-0.031	+0.007
174. Birmingham, Ala.	-0.033	-0.034	-0.014	209. Laurel, Md.	+0.034	+0.043	+0.049
175. Lexington, Va.	-0.024	-0.047	-0.011	210. Harrisburg, Pa.	-0.029	-0.031	-0.019
176. Prestonsburg, Ky.	-0.024	-0.042	-0.020	211. Pittsburg, Pa.	-0.023	-0.041	-0.015
177. Traverse City, Mich.	+0.001	-0.009	+0.011	212. Rockville, Md.	+0.046	+0.053	+0.067
178. Seney, Mich.	+0.001	-0.008	+0.016	213. Upper Marlboro, Md.	+0.013	+0.027	+0.028
179. Oconto, Wis.	-0.025	-0.038	-0.018	214. Fairfax, Va.	+0.036	+0.042	+0.055
180. Grand Rapids, Wis.	-0.042	-0.063	-0.029	215. Crisfield, Md.	-0.029	-0.002	-0.002
181. Winona, Minn.	+0.015	-0.006	+0.017	216. Fredericksburg, Va.	+0.005	+0.015	+0.017
182. Baldwin, Wis.	-0.050	-0.074	-0.036	217. Dover, Del.	-0.010	+0.010	+0.011
183. Cumberland, Wis.	-0.049	-0.074	-0.033	218. North Tamarack, Mich.	+0.031	+0.019	+0.059
184. Cambridge, Minn.	-0.027	-0.051	-0.017	219. Hagerstown, Md.	-0.049	-0.053	-0.035
185. Brainerd, Minn.	+0.012	-0.018	+0.023				

The mean values of the anomalies with and without regard to sign are shown in the following table:

	Anomaly		
	Hayford, 1912	Bouguer	In free air
Mean with regard to sign 219 stations.....	-0.003	-0.037	+0.012
Mean without regard to sign 219 stations.....	.020	.050	.026
Mean with regard to sign 217 stations (Seattle stations omitted).....	-0.002	-0.036	+0.013
Mean without regard to sign 217 stations (Seattle stations omitted).....	.019	.049	.025

The mean without regard to sign is much larger by the free air and the Bouguer than the Hayford reductions and for the Bouguer it is so large as to show that the condition upon which it is based, namely, that of a rigid earth, is very far from the truth.

There are only two Hayford anomalies greater than 0.059 dyne, and those are at Seattle, Wash., at stations so close together that they should be considered really only one station. The maximum free-air anomaly is at Pikes Peak, Colo. (No. 43), and is +0.216 dyne. The maximum Bouguer anomaly is -0.229 at Gunnison, Colo. (No. 45).

The following table gives for the three methods the number of anomalies which fall within certain limits:

Number of anomalies of different magnitudes.

Limits of anomalies in dynes	Number of anomalies			Limits of anomalies in dynes	Number of anomalies		
	Hayford, 1912	Bouguer	In free air		Hayford, 1912	Bouguer	In free air
0.200 to 0.300.....	0	5	1	0.050 to 0.060.....	8	13	11
.100 to .200.....	0	31	5	.040 to .050.....	8	29	18
.090 to .100.....	2	2	1	.030 to .040.....	28	26	25
.080 to .090.....	0	3	0	.020 to .030.....	54	24	40
.070 to .080.....	0	4	0	.010 to .020.....	69	37	52
.060 to .070.....	0	5	7	.000 to .010.....	50	38	59

An inspection of the data in this table shows that the anomalies by the Hayford 1912 method are distributed in fair agreement with the law of distribution of accidental errors. There is no indication of any decided systematic error for those anomalies. On the other hand, the distribution of the anomalies by each of the older methods of reduction departs greatly from the law of distribution of accidental errors and indicates that there are substantial systematic errors present.

GRAVITY ANOMALY MAPS.

The 1912 Hayford anomalies for the 219 stations in the United States and the 42 stations in Canada are shown in figure 11. The contours were drawn mechanically. The whole area covered by the stations was laid out in triangles, each triangle having as its apexes three contiguous stations. In all cases where there was a choice those stations were selected which gave most nearly an equiangular triangle. The points on the contours were determined by interpolations along the triangle sides between the stations at their ends. There are several places where sharp angles in the contours were taken out and the contours rounded, but these are of very minor importance.

The map shows no relations between the anomalies and the topography except for coast topography, but it does seem to show some relation between the anomalies and the geologic formation. Along the coast where the geologic formation is generally Cenozoic the anomaly areas are mostly negative. The large area of Paleozoic formation which extends westward from Pennsylvania is mostly negative, while the large Mesozoic and pre-Cambrian areas in the Dakotas, Minnesota, and in Montana and Wyoming tend to be positive. (See fig. 17.)

Figure 15 shows the gravity anomaly contours in the vicinity of the District of Columbia. These are so intricate that they could not be shown well on the small scale of figure 11.

Figure 12 shows the 1916 Hayford anomalies and the gravity contours for the 219 stations in the United States, and figure 16 the 1916 anomalies and contours for the area surrounding the District of Columbia. These two maps differ very little from figures 11 and 15 showing the 1912 contours.

Figure 13 shows the Bouguer anomalies at the 219 stations in the United States and the anomaly contours. Little comment is needed in regard to this map. It was constructed in the same way as the 1912 and 1916 Hayford anomaly maps. It shows in a very impressive manner the close relations between the Bouguer anomalies and the character of the topography.

Figure 14 shows the free-air anomaly contours for the United States. This shows in a striking manner the relation between the free-air anomalies and the elevations of the stations.

Figures 13 and 14 seem to prove conclusively that the earth's crust is not rigid and also that it is not highly plastic. On the other hand, figures 11 and 12 for the Hayford anomalies prove that the condition of isostasy with the compensation distributed to a considerable depth is very near the truth.

AGREEMENT AS TO POSITIVE AND NEGATIVE AREAS DEDUCED FROM GRAVITY AND FROM DEFLECTION DATA.

In figure 18 are shown the 1912 Hayford anomalies for the 219 stations in the United States and the differences between the observed and the computed values of the deflection of the vertical at many astronomic stations used by Hayford.^a There are also shown a number of ovals inclosing areas in each of which, according to Hayford, the density of the material in the earth's crust is abnormal. They were drawn by him before any results of the gravity reductions were available.

In some of these areas gravity stations have been established, and in no case is there a conflict in the sign of the area as indicated and the sign of the gravity anomaly. There are many of the gravity stations not within these positive and negative areas as shown on the illustration which agree with the deflections of the vertical in their locality.

The two classes of data supplement each other and frequently give a rather definite idea as to the direction from the station of the area under which the cause of a deflection of the vertical is located. For instance, if an arrow in figure 18, which shows by its length the size of the unaccounted-for deflection, is close to a gravity station, the latter being in prolongation of the resultant deflection, the gravity anomaly by its sign will indicate whether the plumb line is attracted in the direction of the arrow or repelled from the opposite side. It may be said that the gravity and deflection data are in general in close accord.

^aSupplemental Investigation in 1909 of the Figure of the Earth and Isostasy.

Chapter IV.—RELATION BETWEEN THE GRAVITY ANOMALIES AND THE TOPOGRAPHY.

A severe test of the reasonableness of a method of reduction of gravity stations is whether the anomalies are different in size and sign, on an average, for different characters of topography.

There are given below five tables, for as many different characters of topography, which contain the anomalies by four methods of reduction. The first method may be called the Hayford, 1912. In this method isostasy is considered complete, and the compensation is assumed to be directly under the station and uniformly distributed to a depth of 113.7 km. The formula used in this method for computing the theoretical gravity at a station is what is called the United States Coast and Geodetic Survey 1912 formula, in which the gravity at the equator is given as 978.038 dynes. The reciprocal of the flattening is 1/298.2 (the Helmert value of 1901; see p. 113). The second method is similar to the first one, except that the depth of compensation is 60 km., and the formula used gives a value of gravity at the equator of 978.040 dynes. Each of these methods is based on the theory of isostasy. The values of the depth and the equatorial gravity used in the second method were derived from a solution of all the data in the United States, from which was obtained the United States Coast and Geodetic Survey 1916 formula for the United States. The derivation of this formula is given on page 123.

The third method is the Bouguer, in which topography is considered, but the isostatic compensation is not. It postulates a rigid crust of the earth. The fourth method is the free air, in which neither the topography nor the compensation is taken into account. It postulates a very plastic crust with the compensation at zero depth. The Helmert formula of 1901 was used in computing the theoretical gravity at the latitude of the stations for the Bouguer and the free-air methods.

At the end of the five tables there is given a table of the mean anomalies with and without regard to sign.

HAYFORD, BOUGUER, AND FREE-AIR ANOMALIES, ARRANGED IN GROUPS ACCORDING TO TOPOGRAPHY.

Twenty-seven coast stations, in the order of their distances from the 1000-fathom line.

Number and name of station	Distance from 1000-fathom line	Anomaly.			
		Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60.0 km	Bouguer (g ₀ - γ ₀)	In free air (g ₀ - γ ₀)
	<i>Kilometers</i>				
54. San Francisco, Cal.....	85	-0.023	-0.010	+0.019	+0.030
18. Beaufort, N. C.....	95	-0.021	-0.008	+0.023	+0.023
80. Astoria, Oreg.....	120	-0.013	-0.010	+0.003	+0.003
90. Virginia Beach, Va.....	130	-0.048	-0.039	-0.015	-0.015
92. Fernandina, Fla.....	145	+0.010	+0.015	+0.036	+0.035
1. Key West, Fla.....	150	+0.005	+0.015	+0.048	+0.048
125. Atlantic City, N. J.....	160	-0.023	-0.018	+0.003	+0.003
8. Point Isabel, Tex.....	160	+0.027	+0.030	+0.049	+0.050
126. Bridgehampton, N. Y.....	180	-0.022	-0.016	+0.005	+0.006
215. Crisfield, Md.....	185	-0.029	-0.023	-0.002	-0.002
149. Wilmington, N. C.....	190	-0.031	-0.024	-0.001	.000
164. Pensacola, Fla.....	190	-0.014	-0.010	+0.008	+0.008
127. Chatham, Mass.....	195	-0.014	-0.007	+0.018	+0.018
5. New Orleans, La.....	210	-0.013	-0.010	+0.008	+0.008
4. Apalachicola, Fla.....	225	.000	+0.004	+0.023	+0.023
27. New York, N. Y.....	225	+0.022	+0.025	+0.037	+0.041
26. Hoboken, N. J.....	230	+0.024	+0.027	+0.039	+0.040
66. Compton, Cal.....	230	-0.050	-0.049	-0.041	-0.042
2. West Palm Beach, Fla.....	243	+0.018	+0.017	+0.057	+0.057
161. Cedar Keys, Fla.....	260	-0.021	-0.016	+0.003	+0.003
3. Punta Gorda, Fla.....	280	+0.010	+0.017	+0.038	+0.038
29. Boston, Mass.....	300	+0.005	+0.008	+0.024	+0.026
30. Cambridge, Mass.....	300	+0.005	+0.009	+0.022	+0.023
17. Charleston, S. C.....	305	-0.021	-0.016	+0.003	+0.003
7. Galveston, Tex.....	330	-0.009	-0.008	+0.006	+0.006
159. Titusville, Fla.....	330	-0.001	+0.007	+0.030	+0.030
128. Rockland, Me.....	350	-0.015	-0.013	+0.003	+0.004
Mean with regard to sign.....		-0.009	-0.003	+0.017	+0.017
Mean without regard to sign.....		.018	.017	.021	.022

Forty-six stations near the coast, in the order of their distances from the open coast.

Number and name of station	Distance from the open coast	Anomaly			
		Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60 km	Bouguer ($g_0'' - \gamma_0$)	In free air ($g_0 - \gamma_0$)
	<i>Kilometers</i>				
157. Homestead, Fla.	20	-0.036	-0.026	+0.001	+0.001
31. Calais, Me.	50	-0.008	-0.007	+0.006	+0.010
25. Princeton, N. J.	60	-0.019	-0.016	-0.004	+0.002
93. Wilmer, Ala.	65	-0.044	-0.042	-0.027	-0.018
217. Dover, Del.	65	-0.010	-0.006	+0.010	+0.011
23. Baltimore, Md.	75	-0.011	-0.008	.000	+0.003
28. Worcester, Mass.	85	-0.020	-0.015	-0.014	+0.006
160. Leesburg, Fla.	85	-0.014	-0.008	+0.012	+0.015
24. Philadelphia, Pa.	90	+0.022	+0.025	+0.037	+0.039
124. Port Jervis, N. Y.	100	-0.033	-0.027	-0.035	-0.022
158. Sebring, Fla.	110	-0.017	-0.010	+0.011	+0.014
148. Greenville, N. C.	130	-0.018	-0.012	+0.007	+0.009
81. Sisson, Cal.	142	-0.010	+0.009	-0.103	+0.013
147. Emporia, Va.	145	+0.013	+0.016	+0.032	+0.036
150. Cheraw, S. C.	150	+0.002	+0.005	+0.017	+0.023
146. Richmond, Va.	150	+0.003	+0.005	+0.018	+0.021
213. Upper Marlboro, Md.	150	+0.013	+0.016	+0.027	+0.028
173. Greenville, Ala.	160	-0.011	-0.009	-0.001	+0.013
209. Laurel, Md.	160	+0.034	+0.036	+0.043	+0.049
21. Washington, D. C. (Coast and Geodetic Survey office)	170	+0.037	+0.038	+0.048	+0.049
22. Washington, D. C. (Smithsonian Institution)	170	+0.039	+0.040	+0.049	+0.050
103. Albany, Ga.	170	+0.002	+0.005	+0.015	+0.021
145. Laurel, Miss.	170	+0.014	+0.016	+0.025	+0.033
84. Washington, D. C. (Bureau of Standards)	175	+0.037	+0.039	+0.046	+0.057
216. Fredericksburg, Va.	180	+0.005	+0.007	+0.015	+0.017
144. Alexandria, La.	190	-0.006	-0.005	+0.008	+0.011
212. Rockville, Md.	190	+0.046	+0.048	+0.053	+0.067
214. Fairfax, Va.	200	+0.036	+0.037	+0.042	+0.055
91. Durham, N. C.	210	+0.036	+0.038	+0.045	+0.058
9. Laredo, Tex.	215	-0.020	-0.022	-0.015	-0.009
65. Yuma, Ariz.	220	+0.009	+0.006	+0.001	+0.007
97. Nacogdoches, Tex.	220	-0.012	-0.013	-0.005	+0.005
123. Albany, N. Y.	220	-0.043	-0.041	-0.048	-0.041
16. McCormick, S. C.	235	+0.015	+0.017	+0.017	+0.035
10. Austin, Tex. (capitol)	245	-0.008	-0.008	-0.021	-0.003
11. Austin, Tex. (university)	245	-0.010	-0.010	-0.023	-0.003
19. Charlottesville, Va.	250	-0.013	-0.011	-0.021	-0.003
151. Charlotte, N. C.	250	+0.025	+0.029	+0.023	+0.048
219. Hagerstown, Md.	250	-0.049	-0.046	-0.053	-0.035
162. Macon, Ga.	265	+0.019	+0.021	+0.023	+0.034
165. Opelika, Ala.	265	-0.026	-0.020	-0.028	-0.001
32. Ithaca, N. Y.	305	-0.023	-0.020	-0.033	-0.010
94. Aliceville, Ala.	305	-0.017	-0.017	-0.010	-0.001
62. Kerrville, Tex.	310	+0.031	+0.035	-0.003	+0.052
106. Fort Kent, Mo.	315	-0.013	-0.014	-0.021	-0.004
6. Rayville, La.	325	+0.016	+0.017	+0.029	+0.032
Mean with regard to sign.		-0.001	+0.002	+0.004	+0.017
Mean without regard to sign.		.021	.020	.025	.023

Eighty-eight stations in the interior and not in mountainous regions, arranged in the order of elevation.

Number and name of station	Elevation	Anomaly			
		Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60 km	Bouguer ($g_0'' - \gamma_0$)	In free air ($g_0 - \gamma_0$)
	<i>Meters</i>				
167. Arkansas City, Ark.	44	-0.012	-0.012	-0.004	+0.001
95. New Madrid, Mo.	79	+0.001	-0.002	+0.001	+0.010
168. Memphis, Tenn.	80	+0.013	+0.012	+0.015	+0.023
88. Wilson, N. Y.	87	-0.010	-0.013	-0.014	-0.004
13. Little Rock, Ark.	89	+0.030	+0.027	+0.030	+0.039
142. Texarkana, Ark.	99	+0.011	+0.009	+0.009	+0.020
87. Potsdam, N. Y.	130	+0.021	+0.021	+0.011	+0.025
141. Fort Smith, Ark.	135	-0.016	-0.018	-0.030	-0.015
132. Watertown, N. Y.	147	-0.025	-0.024	-0.032	-0.016
35. Terre Haute, Ind.	151	-0.009	-0.010	-0.016	.000
38. St. Louis, Mo.	154	-0.005	-0.007	-0.014	+0.004
169. Mammoth Spring, Ark.	156	+0.013	+0.013	+0.002	+0.019
120. Keithsburg, Ill.	167	-0.008	-0.008	-0.018	-0.003
170. Hopkinsville, Ky.	176	+0.006	+0.007	+0.001	+0.020
89. Alpena, Mich.	178	-0.020	-0.019	-0.032	-0.012

Eighty-eight stations in the interior and not in mountainous regions, arranged in the order of elevation—Continued.

Number and name of station	Elevation	Anomaly			
		Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60 km	Bouguer ($g''-\gamma_0$)	In free air ($g_0-\gamma_0$)
	<i>Meters</i>				
174. Birmingham, Ala.....	179	-0.033	-0.030	-0.034	-0.014
177. Traverse City, Mich.....	180	+ .001	.000	-.009	+ .011
179. Oconto, Wis.....	181	-.025	-.027	-.038	-.018
36. Chicago, Ill.....	182	-.007	-.009	-.012	+ .008
138. Springfield, Ill.....	183	-.016	-.017	-.023	+ .003
104. Charleston, W. Va.....	184	-.024	-.024	-.045	-.026
135. Parkersburg, W. Va.....	185	-.024	-.023	-.042	-.022
143. Hot Springs, Ark.....	190	+ .018	+ .018	+ .009	+ .030
134. Erie, Pa.....	198	-.027	-.027	-.040	-.018
166. Huntsville, Ala.....	200	-.023	-.021	-.034	-.012
181. Winona, Minn.....	201	+ .015	+ .015	-.008	+ .017
207. Wheeling, W. Va.....	205	-.029	-.026	-.047	-.024
14. Columbia, Tenn.....	207	+ .026	+ .028	+ .017	+ .040
33. Cleveland, Ohio.....	210	-.003	-.003	-.016	+ .005
203. Duluth, Minn.....	216	+ .050	+ .049	+ .025	+ .048
137. Indianapolis, Ind.....	217	+ .001	+ .002	-.012	+ .012
178. Seney, Mich.....	223	+ .001	+ .002	-.008	+ .016
73. Denison, Tex.....	230	+ .005	+ .004	-.012	+ .012
136. Columbus, Ohio.....	231	-.012	-.011	-.028	-.003
211. Pittsburg, Pa.....	235	-.023	-.022	-.041	-.015
121. Grand Rapids, Mich.....	236	+ .002	+ .002	-.008	+ .013
12. McAlester, Okla.....	240	-.027	-.028	-.015	-.018
59. Pembina, N. Dak.....	243	+ .019	+ .015	-.008	+ .018
34. Cincinnati, Ohio.....	245	-.019	-.019	-.034	-.009
74. Minneapolis, Minn.....	256	+ .059	+ .057	+ .034	+ .062
191. Crookston, N. Dak.....	260	+ .011	+ .008	-.016	+ .013
133. Southport, N. Y.....	266	-.030	-.024	-.047	-.018
37. Madison, Wis.....	270	-.005	-.005	-.021	+ .006
39. Kansas City, Mo.....	278	-.016	-.018	-.038	-.009
154. Winston-Salem, N. C.....	284	-.038	-.034	-.049	-.018
171. Danville, Ky.....	300	-.030	-.026	-.043	-.010
196. Faribault, Minn.....	301	+ .036	+ .035	+ .011	+ .044
140. Joplin, Mo.....	303	+ .016	+ .016	-.009	+ .025
184. Cambridge, Minn.....	303	-.027	-.028	-.051	-.017
180. Grand Rapids, Wis.....	306	-.042	-.042	-.063	-.029
122. Angola, Ind.....	318	+ .011	+ .012	-.001	+ .030
200. Cokato, Minn.....	319	+ .006	+ .005	-.019	+ .017
199. Dawson, Minn.....	323	+ .017	+ .015	-.014	+ .022
15. Atlanta, Ga.....	324	-.023	-.021	-.036	-.001
197. St. James, Minn.....	330	+ .006	+ .005	-.020	+ .016
119. Fort Dodge, Iowa.....	340	+ .015	+ .013	-.011	+ .025
182. Baldwin, Wis.....	342	-.050	-.051	-.074	-.036
208. Leon, Iowa.....	344	-.008	-.008	-.031	+ .007
204. Osage, Iowa.....	356	-.026	-.025	-.050	-.011
108. Fergus Falls, Minn.....	366	-.006	-.008	-.034	+ .003
185. Brainerd, Minn.....	367	+ .012	+ .012	-.018	+ .023
96. Mena, Ark.....	368	-.052	-.051	-.066	-.029
218. North Tamarack, Mich.....	370	+ .031	+ .031	+ .019	+ .059
183. Cumberland, Wis.....	380	-.049	-.048	-.074	-.033
139. Lebanon, Mo.....	385	+ .011	+ .012	-.012	+ .031
186. Aberdeen, S. Dak.....	396	+ .012	+ .009	-.029	+ .015
60. Mitchell, S. Dak.....	408	+ .001	-.003	-.040	+ .003
58. Ely, Minn.....	448	+ .023	+ .023	-.010	+ .039
189. Towner, N. Dak.....	451	+ .032	+ .030	-.014	+ .036
118. Pierre, S. Dak.....	454	+ .014	+ .009	-.039	+ .009
57. Iron River, Mich.....	458	+ .038	+ .041	+ .009	+ .060
40. Ellsworth, Kans.....	469	+ .014	+ .012	-.029	+ .016
107. Prentice, Wis.....	469	+ .024	+ .026	-.005	+ .042
205. Randolph, Nebr.....	515	+ .002	.000	-.012	+ .015
76. Bismarck, N. Dak.....	516	+ .002	.000	-.052	+ .005
190. Crosby, N. Dak.....	598	+ .017	+ .015	-.041	+ .026
192. Poplar, Mont.....	608	+ .019	+ .015	-.050	+ .018
61. Sweetwater, Tex.....	655	-.029	-.028	-.084	-.012
77. Hinsdale, Mont.....	661	+ .029	+ .024	-.053	+ .020
72. Shamrock, Tex.....	708	+ .032	+ .034	-.031	+ .047
193. Miles City, Mont.....	718	+ .030	+ .028	-.061	+ .018
206. Valentine, Nebr.....	785	+ .018	+ .020	-.058	+ .030
187. Faith, S. Dak.....	786	+ .015	+ .014	-.058	+ .029
188. Marmarth, N. Dak.....	822	+ .035	+ .036	-.051	+ .041
83. Paxton, Nebr.....	832	-.006	-.006	-.099	+ .004
100. Guymon, Okla.....	949	-.017	-.016	-.110	-.010
41. Wallace, Kans.....	1005	-.012	-.009	-.105	-.004
99. Farwell, Tex.....	1259	-.016	-.013	-.132	+ .003
Mean with regard to sign.....		-.001	-.001	-.028	+ .009
Mean without regard to sign.....		.019	.019	.033	.020

Thirty-six stations in mountainous regions and below the general level, arranged in the order of their distances below the general level.

Number and name of station	Average elevation within 100 miles of station minus elevation of station	Elevation of station	Anomaly			
			Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60 km	Bouguer ($\rho''-\gamma_0$)	In free air ($\rho_0-\gamma_0$)
	<i>Meters</i>	<i>Meters</i>				
70. Gallup, N. Mex.	30	1990	-0.013	-0.001	-0.211	+0.009
156. Bristol, Va.	32	514	-0.015	-0.007	-0.052	+0.005
105. State College, Pa.	33	358	-0.021	-0.017	-0.038	-0.003
202. Moorcroft, Wyo.	52	1295	+0.021	+0.024	-0.109	+0.034
67. Goldfield, Nev.	112	1716	-0.013	-0.001	-0.166	+0.022
153. Cleveland, Tenn.	123	263	-0.028	-0.020	-0.041	-0.013
210. Harrisburg, Pa.	125	104	-0.029	-0.027	-0.031	-0.019
175. Lexington, Va.	126	324	-0.024	-0.019	-0.047	-0.011
172. Clifton Forge, Va.	157	325	-0.034	-0.027	-0.065	-0.029
85. North Hero, Vt.	167	35	+0.001	-0.002	-0.004	.000
176. Prestonsburg, Ky.	180	193	-0.024	-0.023	-0.042	-0.020
131. Little Falls, N. Y.	198	137	-0.024	-0.021	-0.038	-0.023
155. Knoxville, Tenn.	200	290	-0.021	-0.019	-0.045	-0.014
201. Wasta, S. Dak.	201	706	+0.030	+0.026	-0.052	+0.025
63. El Paso, Tex.	205	1146	+0.007	+0.010	-0.111	+0.016
198. Edgemont, S. Dak.	208	1066	+0.054	+0.054	-0.067	+0.050
113. Heppner, Oreg.	264	568	-0.027	-0.030	-0.093	-0.026
130. Whitehall, N. Y.	290	38	-0.039	-0.037	-0.047	-0.043
112. Olympia, Wash.	306	19	+0.033	+0.029	+0.025	+0.029
110. Boulder, Mont.	307	1493	-0.015	-0.006	-0.181	-0.014
111. Skykomish, Wash.	322	280	-0.028	-0.019	-0.087	-0.067
117. Guernsey, Wyo.	324	1322	+0.036	+0.035	-0.113	+0.028
115. Winnemucca, Nev.	346	1311	-0.009	-0.006	-0.150	-0.005
109. Sheridan, Wyo.	378	1150	+0.032	+0.035	-0.116	+0.009
82. Rock Springs, Wyo.	379	1910	+0.013	+0.020	-0.191	+0.020
45. Gunnison, Colo.	380	2340	+0.020	+0.037	-0.229	+0.027
194. Huntley, Mont.	385	919	+0.011	+0.007	-0.105	-0.003
42. Colorado Springs, Colo.	420	1841	-0.007	+0.003	-0.188	-0.006
195. Lander, Wyo.	536	1635	+0.019	+0.024	-0.182	-0.001
49. Salt Lake City, Utah.	570	1322	+0.010	+0.011	-0.146	-0.023
44. Denver, Colo.	574	1638	-0.016	-0.016	-0.182	-0.023
79. Boise, Idaho.	575	821	+0.008	+0.002	-0.117	-0.026
78. Sandpoint, Idaho.	588	637	+0.002	-0.000	-0.105	-0.034
69. Grand Canyon, Ariz.	824	849	-0.010	-0.001	-0.173	-0.066
46. Grand Junction, Colo.	850	1396	+0.024	+0.024	-0.158	-0.019
47. Green River, Utah.	870	1243	-0.021	-0.026	-0.180	-0.056
Mean with regard to sign.			-0.003	.000	-0.107	-0.008
Mean without regard to sign.			.020	.018	.108	.024

Twenty stations in mountainous regions and above the general level, arranged in the order of their distances above the general level.

Number and name of station	Elevation of station minus average elevation within 100 miles	Elevation of station	Anomaly			
			Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60 km	Bouguer ($\rho''-\gamma_0$)	In free air ($\rho_0-\gamma_0$)
	<i>Meters</i>	<i>Meters</i>				
129. Lancaster, N. H.	1	261	-0.018	-0.011	-0.031	-0.003
71. Las Vegas, N. Mex.	18	1900	+0.003	+0.016	-0.189	+0.028
116. Ely, Nev.	19	1902	-0.021	-0.003	-0.207	+0.007
101. Helenwood, Tenn.	33	422	+0.040	+0.045	+0.015	+0.063
52. Lower Geyser Basin, Wyo.	63	2200	-0.001	+0.015	-0.193	+0.035
51. Norris Geyser Basin, Wyo.	139	2276	+0.021	+0.038	-0.177	+0.080
48. Pleasant Valley Junction, Utah.	147	2191	+0.004	+0.021	-0.187	+0.036
152. Asheville, N. C.	180	670	-0.005	+0.009	-0.045	+0.029
50. Grand Canyon, Wyo.	249	2396	-0.002	+0.017	-0.208	+0.044
98. Alpine, Tex.	265	1359	+0.021	+0.034	-0.088	+0.062
64. Nogales, Ariz.	288	1181	-0.050	-0.040	-0.132	-0.004
20. Deer Park, Md.	291	770	+0.010	+0.022	-0.019	+0.059
86. Lake Placid, N. Y.	306	571	+0.006	+0.016	-0.017	+0.046
103. Hughes, Tenn.	427	994	-0.029	-0.012	-0.074	+0.032
75. Lead, S. Dak.	468	1590	+0.052	+0.062	-0.072	+0.104
68. Yavapai, Ariz.	512	2179	+0.001	+0.012	-0.162	+0.043
114. Truckee, Cal.	512	1805	-0.028	.000	-0.162	+0.037
55. Mount Hamilton, Cal.	1202	1283	-0.003	+0.013	+0.003	+0.125
102. Cloudland, Tenn.	1324	1890	+0.004	+0.021	-0.042	+0.142
43. Pikes Peak, Colo.	2035	4293	+0.021	+0.045	-0.204	+0.216
Mean with regard to sign.			+0.001	+0.016	-0.110	+0.058
Mean without regard to sign.			.017	.022	.111	.059

Mean anomalies.

WITH REGARD TO SIGN.

	Number of stations	Mean anomaly.			
		Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60 km	Bouguer	In free air
Coast stations.....	27	-0.009	-0.003	+0.017	+0.017
Stations near the coast.....	46	- .001	+ .002	+ .004	+ .017
Stations in the interior, not in mountainous regions.....	88	- .001	- .001	- .028	+ .009
Stations in mountainous regions, below the general level.....	36	- .003	.000	- .107	- .008
Stations in mountainous regions, above the general level.....	20	+ .001	+ .016	- .110	+ .058
All stations (except the two Seattle stations).....	217	- .002	+ .001	- .036	+ .013

WITHOUT REGARD TO SIGN.

Coast stations.....	27	0.018	0.012	0.021	0.022
Stations near the coast.....	46	.021	.020	.025	.023
Stations in the interior, not in mountainous regions.....	88	.019	.019	.033	.020
Stations in mountainous regions, below the general level.....	36	.020	.018	.108	.024
Stations in mountainous regions, above the general level.....	20	.017	.022	.111	.059
All stations (except the two Seattle stations).....	217	.019	.019	.049	.025

Anomalies for all stations treated as a single group.

	Anomaly			
	Hayford, 1912; depth, 113.7 km	Hayford, 1916; depth, 60 km	Bouguer	In free air
Mean with regard to sign, 219 stations.....	-0.003	0.000	-0.037	+0.012
Mean without regard to sign, 219 stations.....	.020	.020	.050	.026
Mean with regard to sign, 217 stations (Seattle stations omitted).....	- .002	+ .001	- .036	+ .013
Mean without regard to sign, 217 stations (Seattle stations omitted).....	.019	.019	.049	.025

The mean anomalies with regard to sign for the Bouguer reduction show a remarkable range in values from +0.017 dyne for the coast stations to -0.110 dyne for stations in mountainous regions which are above the general level. The other classes of topography have mean Bouguer values which fall between these extremes. The value which is nearest zero is for the stations near but not on the coast; that is, on the coastal plains. The effect of ignoring the compensation here should have little effect as the topography is in general very low. We may conclude that there are decided relations between the Bouguer anomalies and the character of the topography. Therefore it is certain that the earth's crust is not rigid with the oceans and continents held in place as a result of its rigidity. The Bouguer method is certainly not based upon correct principles.

The free-air anomalies have means with regard to sign for the five topographic groups which range from -0.008 for mountain stations below the general level to +0.058 for those mountain stations which are above the general level. The coast stations and those near but not on the coasts have mean anomalies, with sign considered, of +0.017. The stations in the interior not in mountain regions have a mean of +0.009. If the mean of the 1912 and 1916 values for the gravity at the equator, which is 0.009 dyne greater than the Helmert 1901 value, had been used, the mean of the anomalies by the free-air method for the stations in the interior and not in mountainous regions would have been zero. This is as one might expect, for the effects of the distant topography and compensation are not large (see tables on pp. 20 to 48) and the effect of the near topography on a plain is almost exactly balanced by the isostatic compensation. It is a fact which should be kept in mind when studying the effect of topography and isostatic compensation that the attractive effect of a mass of uniform density, of great horizontal extent, and of a uniform thickness is the same as for a mass of a much greater thickness, with a correspondingly smaller density and the same great horizontal extent. As an

example, a disk of material 100 feet thick of density 2.67 and 1000 miles in horizontal radius will have practically the same attraction as a mass 100 000 feet thick with a density of 0.00267 and as before 1000 miles in horizontal dimensions from the center of the disk. Therefore we have the attractive effect of the topography of a plain of great dimensions exactly or nearly balanced by the effect of the compensation. (See p. 72.)

The mean of the 1912 Hayford anomalies with regard to sign is only -0.002 (omitting the Seattle stations) and the mean value for each of the five topographic groups is small except one. The mean of the coast station anomalies is -0.009 . This mean anomaly may be explained in part by the fact that nearly all the material along the coasts belongs to the Cenozoic or recent formation, and authorities give its density as ranging from 2.40 to 2.50. (See table on p. 215 of "The Strength of the Earth's Crust" by Joseph Barrell in Volume XXII of *Journal of Geology*.) This material is no doubt of considerable thickness at many parts of the coasts. It is shown on pages 70 to 83 under the heading "Relation between the gravity anomalies and the geologic formation" that the presence of light material in the earth's crust near a station would tend to make the computed value of gravity too great and the difference between the observed and computed values would tend to be negative. If we should eliminate from consideration the coast stations or assume that the value -0.009 is explained by the presence of the Cenozoic material, then the mean with regard to sign of the anomalies for the various topographic groups is never more than 0.003 dyne from the mean for all stations, and three of the groups have means which are only 0.001 from the mean of all. The total range in the means with regard to sign for the various groups, ignoring coast stations, is only 0.004 dyne. This is very different from the range in the means for the Bouguer and the free-air anomalies. It shows that this method is very much closer to the truth.

The means for the Hayford 1912 anomalies for the various groups without regard to sign vary only slightly. The lowest is 0.017 for mountain stations above the general level, and the largest is 0.021 for stations near but not on the coast. The mean for all is 0.019. The mean of the Bouguer anomalies without regard to sign for the several groups varies from 0.021 for coast stations to 0.111 for stations in mountainous regions above the general level, while the free-air anomalies vary from 0.022 at coast stations to 0.059 at stations in mountainous regions above the general level.

We must conclude that the average size of the anomalies without regard to sign indicates that there is no relation between the Hayford 1912 anomalies and the topography.

The Hayford 1916 anomalies give substantially the same evidence in favor of isostasy that is given by the 1912 anomalies, but it is difficult to see which method of reduction is nearer the truth.

The mean value for the 1916 anomalies with regard to sign for 217 stations is $+0.001$. The mean anomaly for the coast stations is -0.003 , which is different from the mean by 0.004. For the 1912 anomalies the mean coast anomaly differs 0.007 from the mean of all, which is -0.002 . This may be considered as being in favor of a depth of 60 km. as against the depth of 113.7 km. But, as stated above, and also on pages 76 and 77, the material near the coast belongs in general to the Cenozoic geologic formation which is less dense than normal (2.67). The presence of this less dense material makes the computed value of gravity too great and the anomalies negative. The effect of reducing the depth of compensation to 60 km. is to give the compensation of the oceans less effect at the coast stations, the computed gravity is less, and the negative anomalies are reduced in size on an average. It is questionable whether the reduced size of the mean anomaly with regard to sign for the 1916 reduction is evidence in favor of the reduced depth of compensation.

The means with regard to sign for the 1916 anomalies in the groups near the coast, in the interior not in the mountainous regions, and in mountainous regions below the general level, are practically the same as for the 1912 anomalies. Hence there is little evidence from these in favor of either reduction.

There is a decided difference between the mean with regard to sign for the 1912 and 1916 anomalies at stations in mountainous regions above the general level. The former is only $+0.001$, which shows no systematic error, while the latter is $+0.016$, which, on the other hand, shows a great systematic error.

The change in depth from 113.7 km. to 60 km. does not make a material difference in the effect of the compensation for the stations in mountainous regions below the general level if there is local compensation of the mountain masses. (See p. 108.) The table of individual values for the anomalies on page 66 shows that for this class of topography the anomalies are nearly the same for the 1912 and the 1916 reductions.

The table on page 66 for stations above the general level in mountainous regions shows that there is little or no similarity between the anomalies by the 1912 and 1916 methods. For the first method there are 9 stations of the 20 with negative anomalies, while for the latter there are only 4. There are only 3 of the 1912 anomalies above 0.030, while there are 6 of the 1916 anomalies.

If there is local compensation, then the effect of reducing the depth is to make the effect (negative) of the compensation greater and the computed value of gravity at a mountainous station less. The sign of the anomaly would in consequence tend to be positive. This is what we find to be the case. If the compensation is regional, then the effect of changing the depth of compensation is smaller than if the compensation were local.

It is believed that from the above evidence the conclusion may be drawn that the depth of 113.7 km. is nearer the truth than 60 km. in mountainous regions, and that local distribution of the compensation is more probable than the regional if the latter distribution extends to great distances from the topographic features. This agrees with the evidence given under the heading "Regional versus local distribution of compensation." (See pp. 85 to 92.) The data and discussion on pages 97 to 131 in connection with the anomalies for various depths should be considered in connection with the data given above.

It is believed that the further conclusions may be justified, that there is a relation between the coast topography and the gravity anomalies by the 1912 reduction, this relation probably being due to the lighter material in the earth's crust below sea level, and that there is also a relation between the topography and the gravity anomalies at stations in mountainous regions above the general level for the 1916 method, this relation being explained by the erroneous depth of compensation for this method (60 km.).

Chapter V.—RELATION BETWEEN THE GRAVITY ANOMALIES AND THE GEOLOGIC FORMATION.

Surface densities are known to differ somewhat from the mean surface density and these differences will sometimes occur over large areas. They should cause, therefore, some variation of the value of the intensity of gravity from the normal. As the surface densities vary somewhat for the different geologic formations, a study was made to learn whether there is any relation between the Hayford gravity anomalies and the surface geology at the stations. On page 215 of the *Journal of Geology* (Vol. XXII, 1914) Barrell gives the following estimated mean specific gravities of geologic formations:

Pre-Cambrian.....	2.75-2.80
Paleozoic and Mesozoic.....	2.50-2.60
Cenozoic.....	2.40-2.50

The author presents the data in the tables following, which may be used as the basis for investigation by others who are interested in this subject. The tables give data for the 219 stations in the United States, 42 stations in Canada, and 73 stations in India. For all of these stations the 1912 Hayford anomalies have been computed and are given.

The stations in the United States and in Canada were plotted on the geologic map of North America which bears the following title: "Geologic map of North America, compiled by the United States Geological Survey in cooperation with the Geological Survey of Canada and Instituto Geologico de Mexico, under the supervision of Bailey Willis and George W. Stose, Scale 1:5 000 000, 1911." The decision as to the surface geologic formation on which the stations are located was based entirely on this map. It is probable that the classification would differ occasionally if other sources of information were used. The writer believes, however, that only minor changes would be made in the tables given below and the conclusions drawn from them would not be materially changed.

The Indian stations were plotted on a geologic map taken from the pocket at the back of "A manual of the geology of India," by Medlicott and Blanford, second edition, revised by Oldham, superintendent Geological Survey of India, 1893.

The tables give the stations and the Hayford 1912 anomalies for each of the formations, (1) pre-Cambrian, (2) Paleozoic, (3) Mesozoic, (4) Cenozoic, (5) Effusive and Intrusive, and (6) unclassified.

In the tables for the United States the 1912 and 1916 Hayford anomalies are given. The former are based upon the United States Coast and Geodetic Survey formula of 1912, viz,

$$\gamma_0 = 978.038 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi)$$

which gives the value of gravity for any latitude at sea level. The compensation was assumed to be uniformly distributed and complete at a depth of 113.7 km. The 1916 values are based upon the United States Coast and Geodetic Survey formula of 1916 (see p. — of this volume) viz,

$$\gamma_0 = 978.040 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi)$$

and upon a depth of isostatic compensation of 60 km.

The relations between the gravity anomalies and the geologic formations in Canada and India are considered later (pp. 80 to 82). The anomalies given for these countries are comparable with those shown in the following table for the 1912 formula and depth of compensation. It will be shown later in what measure the relations for the stations in those countries confirm or negative those in the United States.

RELATION BETWEEN THE GRAVITY ANOMALIES AND THE GEOLOGIC FORMATION FOR STATIONS IN THE UNITED STATES.

Stations in the United States and Hayford anomalies for specified formations.

Formation and station number	Hayford anomaly		Formation and station number	Hayford anomaly		Formation and station number	Hayford anomaly	
	1912	1916		1912	1916		1912	1916
Pre-Cambrian formation:			Paleozoic formation—Con.			Cenozoic formation—Con.		
16.....	+0.015	+0.017	179.....	-0.025	-0.027	93.....	-0.044	-0.042
24.....	+0.022	+0.025	181.....	+0.015	+0.015	95.....	+0.001	+0.002
43.....	+0.021	+0.045	182.....	-0.050	-0.051	97.....	-0.012	-0.013
45.....	+0.020	+0.037	183.....	-0.049	-0.048	99.....	-0.016	-0.013
57.....	+0.038	+0.041	184.....	-0.027	-0.028	100.....	-0.017	-0.016
58.....	+0.023	+0.023	196.....	+0.036	+0.035	109.....	+0.032	+0.035
75.....	+0.052	+0.062	204.....	-0.026	-0.025	112.....	+0.033	+0.029
102.....	+0.004	+0.021	207.....	-0.029	-0.026	115.....	-0.009	-0.006
107.....	+0.024	+0.026	208.....	-0.008	-0.008	117.....	+0.036	+0.035
153.....	-0.006	+0.009	210.....	-0.029	-0.027	125.....	-0.023	-0.018
165.....	-0.026	-0.020	211.....	-0.023	-0.022	126.....	-0.022	-0.016
185.....	+0.012	+0.012	219.....	-0.049	-0.046	127.....	-0.014	-0.007
191.....	+0.011	+0.008	Mesozoic formation:			142.....	+0.011	+0.009
203.....	+0.050	+0.049	10.....	-0.006	-0.008	144.....	-0.006	-0.005
Paleozoic formation:			11.....	-0.010	-0.010	145.....	+0.014	+0.016
12.....	-0.027	-0.028	22.....	-0.011	-0.008	148.....	-0.018	-0.012
14.....	+0.026	+0.028	25.....	-0.010	-0.016	149.....	-0.031	-0.024
20.....	+0.010	+0.022	40.....	+0.014	+0.012	157.....	-0.036	-0.026
29.....	+0.005	+0.008	42.....	-0.007	+0.003	158.....	-0.017	-0.010
30.....	+0.005	+0.009	46.....	+0.024	+0.024	159.....	-0.001	+0.007
32.....	-0.023	-0.020	47.....	-0.021	-0.026	160.....	-0.014	-0.006
33.....	-0.003	-0.003	54.....	-0.023	-0.010	161.....	-0.021	-0.016
34.....	-0.019	-0.019	55.....	-0.008	+0.013	162.....	+0.002	+0.005
35.....	-0.006	-0.010	60.....	+0.001	-0.003	164.....	-0.014	-0.010
36.....	-0.007	-0.009	62.....	+0.031	+0.035	167.....	-0.012	-0.012
37.....	-0.005	-0.005	70.....	-0.013	-0.001	168.....	+0.013	+0.012
38.....	-0.005	-0.007	71.....	+0.003	+0.016	190.....	+0.017	+0.015
39.....	-0.016	-0.018	73.....	+0.006	+0.004	208.....	+0.018	+0.020
59.....	+0.019	+0.015	77.....	+0.029	+0.024	213.....	+0.013	+0.016
61.....	-0.029	-0.028	91.....	+0.036	+0.038	215.....	-0.029	-0.023
72.....	+0.032	+0.034	94.....	-0.017	-0.017	217.....	-0.010	-0.006
74.....	+0.059	+0.057	106.....	-0.006	-0.008	Intrusive formation:		
78.....	+0.002	+0.000	118.....	+0.014	+0.009	28.....	-0.020	-0.015
85.....	+0.001	-0.002	150.....	+0.002	+0.005	31.....	-0.008	-0.007
88.....	-0.010	-0.013	162.....	+0.019	+0.021	86.....	+0.006	+0.016
89.....	-0.020	-0.019	186.....	+0.012	+0.009	103.....	-0.029	-0.012
96.....	-0.052	-0.051	187.....	+0.015	+0.014	111.....	-0.028	-0.019
101.....	+0.040	+0.045	188.....	+0.036	+0.036	151.....	+0.025	+0.026
104.....	-0.024	-0.024	189.....	+0.032	+0.030	154.....	-0.038	-0.034
105.....	-0.021	-0.017	192.....	+0.019	+0.015	Effusive formation:		
106.....	-0.013	-0.014	193.....	+0.030	+0.028	50.....	-0.002	+0.017
119.....	+0.015	+0.013	194.....	+0.011	+0.007	51.....	+0.021	+0.038
120.....	-0.008	-0.008	195.....	+0.019	+0.024	52.....	-0.001	+0.015
121.....	+0.002	+0.002	197.....	+0.006	+0.005	81.....	-0.010	+0.006
122.....	+0.011	+0.012	198.....	+0.054	+0.054	98.....	+0.021	+0.024
123.....	-0.043	-0.041	200.....	+0.006	+0.005	110.....	-0.015	-0.006
124.....	-0.033	-0.027	201.....	+0.030	+0.026	112.....	-0.027	-0.030
128.....	-0.015	-0.013	202.....	+0.021	+0.024	114.....	-0.028	-0.000
129.....	-0.018	-0.011	216.....	+0.006	+0.007	Unclassified:		
130.....	-0.039	-0.037	Cenozoic formation:			13.....	+0.030	+0.027
131.....	-0.024	-0.021	1.....	+0.006	+0.015	15.....	-0.023	-0.021
132.....	-0.025	-0.024	2.....	+0.018	+0.027	19.....	-0.013	-0.011
133.....	-0.030	-0.024	3.....	+0.010	+0.017	21.....	+0.037	+0.038
134.....	-0.027	-0.027	4.....	-0.000	+0.004	22.....	+0.039	+0.040
135.....	-0.024	-0.023	5.....	-0.013	-0.010	26.....	+0.024	+0.027
136.....	-0.012	-0.011	6.....	+0.016	+0.017	27.....	+0.022	+0.025
137.....	+0.001	+0.002	7.....	-0.009	-0.008	41.....	-0.012	-0.009
138.....	-0.016	-0.017	8.....	+0.027	+0.030	48.....	+0.004	+0.021
139.....	+0.011	+0.012	9.....	-0.020	-0.022	49.....	+0.010	+0.011
140.....	+0.016	+0.016	17.....	-0.021	-0.016	67.....	-0.013	-0.001
141.....	-0.016	-0.018	18.....	-0.021	-0.008	68.....	+0.001	+0.012
143.....	+0.018	+0.018	44.....	-0.016	-0.016	69.....	-0.010	-0.001
153.....	-0.023	-0.020	53.....	-0.008	-0.100	84.....	+0.037	+0.039
155.....	-0.021	-0.019	56.....	+0.007	+0.010	87.....	+0.021	+0.021
156.....	-0.015	-0.007	63.....	-0.050	-0.040	116.....	-0.021	-0.008
166.....	-0.023	-0.021	64.....	+0.009	+0.006	146.....	+0.003	+0.005
169.....	+0.013	+0.013	65.....	-0.050	-0.049	147.....	+0.013	+0.016
170.....	+0.006	+0.007	66.....	+0.002	+0.000	173.....	-0.011	-0.009
171.....	-0.030	-0.026	76.....	+0.008	+0.002	180.....	-0.042	-0.042
172.....	-0.034	-0.027	79.....	-0.013	-0.010	199.....	+0.017	+0.015
174.....	-0.033	-0.030	80.....	+0.013	+0.020	205.....	+0.002	-0.000
175.....	-0.024	-0.019	82.....	-0.006	-0.005	209.....	+0.034	+0.036
176.....	-0.024	-0.022	83.....	-0.048	-0.039	212.....	+0.046	+0.048
177.....	+0.001	+0.000	90.....	+0.010	+0.015	214.....	+0.036	+0.037
178.....	+0.001	+0.002	92.....			218.....	+0.031	+0.031

* These stations are near pre-Cambrian formations.

Stations in the United States and Hayford anomalies for specified formations—Continued.

SUMMARY.

Geologic formation	Number of stations					Mean anomaly			
	With plus anomalies		With minus anomalies		All	With regard to sign		Without regard to sign	
	1912	1916	1912	1916		1912	1916	1912	1916
Pre-Cambrian.....	12	13	2	1	14	+0.019	+0.025	0.023	0.028
Paleozoic.....	23	20	49	50	72	-.011	-.010	.021	.020
Mesozoic.....	25	26	11	10	36	+.009	+.011	.017	.017
Cenozoic ^a	22	22	32	32	55	-.007	-.004	.019	.018
Cenozoic ^b	22	22	31	31	54	-.006	-.003	.018	.016
Intrusive.....	2	2	5	5	7	-.013	-.006	.022	.019
Effusive.....	2	5	6	2	8	-.005	+.010	.015	.019
Unclassified.....	18	17	8	8	26	+.010	+.014	.021	.021
All stations ^a	104	105	113	108	218	-.002	-.000	.020	.019
All stations ^b	104	105	112	107	217	-.002	+.001	.019	.019

^a Counting the two Seattle stations as one.^b With Seattle stations omitted.

ANOMALIES ON PRE-CAMBRIAN FORMATIONS.

In the above summary it is seen that there are 14 stations located on pre-Cambrian formations and that 12 have positive and only 2 negative 1912 anomalies. For the 1916 anomalies 13 are positive and only 1 negative. This seems to be very strong evidence that we may expect positive anomalies at much the greater number of future stations in the United States which may be located on the pre-Cambrian formation. It is noteworthy that nearly all of the pre-Cambrian stations in the United States are located on very small areas of that formation. This may give some clew as to the cause of the large positive anomaly.

If the density of the upper strata of the earth's crust for large distances (horizontal) from the stations is above normal, then the effect of this greater density, which will tend to increase the gravity, will be offset by the opposite effect of the compensating deficiency of density in the deeper crust. This is due to the fact that the effect of a certain amount of material in the form of a disk of infinite horizontal extent is the same on a unit mass of matter whether the unit mass is immediately above the surface of the attracting matter or at an indefinite distance above it. Therefore, if we should have a stratum or mass of pre-Cambrian material of density 2.90 at the earth's surface directly under the station, and of great or infinite extent horizontally, it would have the same attractive effect on the unit mass as if this matter were distributed through a great vertical distance but had the same horizontal extent. Therefore, if the dense material at the surface were compensated for by a deficiency of density in the lower crust, the positive effect of the former would be exactly counterbalanced by the negative effect of the compensation. Hence, we should not expect a decided positive anomaly at a pre-Cambrian gravity station should the formation be of uniform thickness and of great horizontal dimensions. This statement is based upon the assumption, which may be substantially true, that the area in question is in a state of perfect isostatic equilibrium at the depth of compensation.

If, however, the area of denser material is limited in horizontal extent, then the effect of the added material, being inversely proportional to the square of its distance from the attracted unit mass, will be greater than the negative effect of the compensation. Therefore, if there is a compensating lack of density in the lower crust, the resultant effect will be positive and we should have a positive gravity anomaly. The size of the anomaly will depend upon the thickness of the stratum of pre-Cambrian rock, its density, its horizontal extent, and the vertical location of the compensation.

In Special Publication No. 10 (pp. 110 and 111) there are given some numerical examples showing the effect of strata of various thicknesses and densities.

It should be borne in mind that in making the gravity reductions no numerical values are given for the densities in the earth's crust below sea level. (See p. 8.) It is assumed that the

densities in the crust under the coastal plane at sea level for the various strata are normal, and that these densities are modified by the isostatic compensation under the topography of the interior of the continents and under the oceans. It is only the deviations from the normal densities in the crust below sea level which are considered in these investigations.

The effect of masses in different locations with reference to the station is indicated in the following table, which, with some additions, is reprinted from page 109 of Special Publication No. 10:

Table of attractions for various masses.

[Each tabular value is the vertical attraction in dynes produced at a station by a mass equivalent to a stratum 100 feet thick, of density 2.67, and of the horizontal extent indicated in the left-hand argument, if that mass is uniformly distributed from the level of the station down to the depth indicated in the top argument and from the station in all directions horizontally to the distance indicated in the left-hand argument.]

Radius of mass	Depth				
	1000 feet.	5000 feet.	10 000 feet.	15 000 feet.	113.7 kilo-meters.
1.28 km. (the outer radius of zone E)	0.0030	0.0018	0.0011	0.0008	0.0000
5 km.	.0033	.0029	.0025	.0021	.0001
10 km.	.0034	.0032	.0029	.0027	.0003
166.7 km. (the outer radius of zone O)	.0037	.0034	.0034	.0034	.0024
1190 km. (or 10° 44', the outer radius of zone 10)	.0040	.0037	.0037	.0037	.0035

It is seen from the preceding table that a pre-Cambrian formation 10 000 feet thick, with a density of 2.94 (just 10 per cent greater than the assumed normal surface density of 2.67) and 10 km. in horizontal extent in all directions from a station on its surface will give an increase in gravity of 0.029 dyne. The effect of the isostatic compensation (uniformly distributed to the depth of compensation), the negative equivalent of 1000 feet of material of normal density (2.67), is only 0.003 dyne. The resultant effect is +0.026 dyne, approximately the average size of the 1912 pre-Cambrian anomaly.

If we should have a pre-Cambrian formation 10 000 feet thick of density 2.94, as above, but of 166.7 km. horizontal extent in all directions from the station, the effect of the topography on gravity would be increased by 0.034 dyne, while the effect of the compensation of this excess of mass would be -0.024 dyne, and the resultant effect would be only +0.010 dyne. Now, if the foundation under consideration were extended horizontally 1190 km. from the station, the positive effect would be +0.037 dyne and the effect of its compensation -0.035 dyne, and the resultant effect at the station only +0.002 dyne.

On page 80, under the discussion of the Canadian stations, it is shown that the anomalies at the stations in pre-Cambrian formations are not positive as in the United States. They differ little from the mean of all stations. The pre-Cambrian formations in Canada are of considerable horizontal extent, and therefore the effect of the increased surface densities is offset by the isostatic compensation. This agrees with the above reasoning.

If there were many gravity stations on and near a limited area of pre-Cambrian formation, it might be possible to estimate from the results the approximate limits of the space within which the densities were above normal. But it must be borne in mind that the problem of determining exactly the space or spaces within which there are abnormal densities which might cause the anomalies is not susceptible of mathematical solution. This is because there are too many unknowns which would enter into any equations used and arbitrary assumptions would have to be made. Of course, the problem can be treated mathematically and with greater numbers of stations in any given area the truth can be more closely approximated.

It seems to be evident that the anomalies are not due simply to an assumed erroneous density of the mass above sea level, for at a number of pre-Cambrian stations the elevation above sea level is less than 1500 feet, and the maximum effect of a change in the density of 10 per cent in that mass would be only 0.005 dyne. The cause of the anomaly must therefore be located to a large extent below sea level in nearly all cases.

It is no doubt true that the deep-seated rocks have densities comparable with those of the pre-Cambrian rocks seen at the surface, but the cause of the anomaly at pre-Cambrian stations seems to be due largely to the dense rock protruding through the materials of the upper crust which are of less density.

The author does not mean to state that the whole of any anomaly is due to the geological formation, for there is probably in many cases a local lack of perfect isostasy which may produce deviations from the normal gravity.

It is a noteworthy fact that the pre-Cambrian stations in the United States show an excess of gravity in general, and that they are on areas which have been subjected to erosive action for geologic ages. We may conclude that as erosion has taken place there has been a rising of the areas due probably to isostatic adjustment.

The 1916 anomalies, based upon a depth of compensation of only 60 km., are very little different from the 1912 anomalies, which are based upon a depth of 113.7 km. The former are, on an average, 0.006 dyne greater than the latter, and this is what might be expected upon the assumption of local perfect compensation. The fact that the compensation is closer to the station would make its effect greater, consequently the combined effect of the greater density of material above sea level and the compensating deficiency of material in the lower crust would be smaller than for the 1912 anomalies.

The effect of a change in the depth of compensation is discussed on pages 97 to 131.

ANOMALIES ON PALEOZOIC FORMATIONS.

In the United States there are 72 stations in the Paleozoic formation, for which 49 of the 1912 anomalies are negative and 23 positive. The mean with regard to sign is -0.011 dyne, and the mean without regard to sign is 0.021 dyne.

The addition of 94 stations in the United States since the investigation in 1912 (Special Publication No. 12) has increased the tendency of the Paleozoic anomalies to be negative. A large area of the United States is covered by rock of this formation, and the 72 Paleozoic stations are nearly one-third of all the stations.

The density of the Paleozoic formations is given by Barrell as 2.50 to 2.60. The average density, 2.55, is 0.12, or about 5 per cent, lower than the density used in making the computations. The situation here is opposite to that connected with the pre-Cambrian formation, for the stations there tended to have positive anomalies. It might be assumed that the crust under the Paleozoic formation is not in a state of perfect isostasy, and that the anomalies are the result of the departure from that state. This view is probably erroneous, because the anomalies on very large areas of Paleozoic formation have negative values and would therefore indicate decided regional deviation from the perfect condition. Most of the data contained in this report, including the anomaly maps, indicate that we have in the United States local rather than regional deviations from perfect isostasy.

The tendency of the anomalies to be negative could be caused by the lower density of the material in this formation, as compared with the value used in the computations. If near a station in a Paleozoic area the density of the upper crust were below normal, say, 5 per cent, to a depth of 15 000 feet and to a horizontal distance of 10 km. from the station, the effect of this deficient density would be a change in the attraction of 0.020 dyne. The effect of the compensating increase in density in the lower crust would be $+0.002$. The combined effect of considering the local densities makes a difference of 0.018 in the anomaly at the station in question.

The effect on gravity at a station due to using an erroneous value of the density of the topography, that is the material which is above sea level, would be small as a general rule for the average elevation of the Paleozoic stations in the United States is somewhat less than 1000 feet. The effect of changing by 5 per cent the density of the topography to a depth of 1000 feet and 10 km. in all directions from the stations would be only 0.0017 dyne. The effect of

the compensation of the excess of mass would be less than 0.0002 dyne. It is evident that the principal cause of the negative Paleozoic anomalies is lower than sea level in the earth's crust.

It is probably true that the lighter density of Paleozoic material is the principal cause of the tendency for the anomalies at stations on this formation to have negative signs. This is no doubt supplemented by local departures from perfect isostasy near stations with large anomalies.

It is possible that the positive anomalies and the small negative anomalies are in areas where the Paleozoic strata are thin or which have material denser than normal underlying the Paleozoic matter.

The 1916 anomalies for Paleozoic areas seldom differ from the 1912 anomalies more than two units in the last place and the mean anomalies with and without regard to sign are practically the same. This is as might be expected, for the Paleozoic stations are in general on low topography and, as shown on page 72 in the discussion of the pre-Cambrian stations, a disk of very great horizontal extent has the same attractive effect regardless of the distance of the attracted mass from the surface of the disk. In fact, the effect of the topography and its compensation are so nearly equal at stations in Paleozoic areas that the anomalies by the free-air reduction, in which no account is taken of the topography and compensation, are nearly the same as the Hayford anomalies. An erroneous depth of compensation used in the computation can not explain the anomalies in the Paleozoic formation.

That there is in general a close approximation to perfect isostasy is shown by the Bouguer anomalies in the interior of the continent not in mountainous regions, for they are nearly all negative and are of considerable size, while the algebraic mean of the Hayford anomalies is nearly zero.

The Paleozoic negative anomalies in general are probably due in most part to departures from normal densities in the strata in the upper crust, but below sea level, comparatively near the station, and to a less degree to local departures from perfect isostasy.

ANOMALIES ON MESOZOIC FORMATIONS.

Of the 36 stations in the Mesozoic formation, 25 have positive and 11 negative 1912 anomalies. The means with and without regard to sign are respectively +0.009 and 0.017 dyne.

Barrell gives the density of Mesozoic rock as ranging from 2.50 to 2.60. This is lower than the density (2.67) used in making the topographic reductions. There seems to be no evident relation between the surface densities of the Mesozoic rocks and the anomalies. If there were the anomalies would be negative rather than positive.

That there is some relation between the formation and the anomalies seems to be well established, for the positive anomalies largely exceed the negative ones in number, and the mean anomaly with regard to sign is just one-half the size of the mean of all (219) anomalies without regard to sign. But the cause of the positive sign of the Mesozoic anomalies is below the upper strata. That it is regional to a certain extent is shown by the persistency of the sign in any extensive Mesozoic formation, such as in the Dakotas and in eastern Montana. But that it varies from place to place is indicated by the different values of the anomaly. For instance, at Edgemont, S. Dak. (station No. 198) the anomaly is +0.054 dyne and at Moorcroft, Wyo. (station No. 202) only 90 miles distant, it is +0.021 dyne.

There, of course, may be departures in the Mesozoic areas from the state of perfect isostasy, but it is impossible with the present data to determine with any degree of certainty what portion of an anomaly is due to such departures and what is caused by departures from normal densities in the crust above the depth of compensation or even below that depth. The depth of compensation as computed from geodetic data should not be considered as very definite. The probable error of the determination is comparatively large. The change in the deflection and the gravity anomalies is comparatively slow with a change of depth and the value of the depth is therefore somewhat indeterminate. (See pp. 97 to 112.)

ANOMALIES ON CENOZOIC FORMATIONS.

The anomalies at Cenozoic stations have a tendency to be negative, as is shown by an inspection of the anomalies at 55 Cenozoic stations in the United States. Only 22 of them are positive, while 32 are negative.

Barrell gives the Cenozoic densities as ranging from 2.40 to 2.50 (see table on p. 70), which is less than the density used in making the topographic reductions. That a portion of the anomalies is due to the small density of the surface material and of the crust close to the surface seems to be evident. The size of the anomalies may be an indication of the space occupied by the lighter material. Where the anomaly is large and negative the light strata would probably be of great thickness and of small horizontal dimensions. The erroneous density could be the cause of the negative anomalies, provided there were no local departure from perfect isostasy.

If the Cenozoic formation of small density is small in horizontal dimensions, and if there is perfect local isostasy, the effect of the light material in the upper crust and near the surface would be much greater than the opposite effect of the compensating increase in density in the lower crust.

For instance, if the density of the upper crust to a depth of 10 000 feet is 2.40 (10 per cent less than the assumed surface density), and if the material extends in a horizontal direction 10 km. from the station, the effect would be -0.029 dyne. The effect of the compensating increase in density in the remainder of the crust to the depth of the compensation would be only $+0.003$ dyne and the combined effect would be -0.026 dyne. If the lighter material extends 20 or 30 km. from the station, the combined effect would be somewhat less, while if it extended 166.7 km. in all directions from the station, the combined effect would be only -0.010 dyne.

The cause of the large Cenozoic anomalies must be local, for there are decided differences in the size of the anomalies at pairs of stations which are comparatively close together. For instance, at Virginia Beach (station No. 90) the anomaly is -0.048 dyne, while at Crisfield (station No. 215) the anomaly is only -0.029 dyne. The distance between the stations is about 80 miles.

It appears from the evidence above that we may gain from the negative anomalies of the Cenozoic formations some idea of the depth of the Cenozoic material at a station, and where there are many stations in any given locality of Cenozoic formation we may get an approximation to the horizontal limits of the affected spaces. For instance, it is reasonable to conclude that if the Virginia Beach anomaly is caused by a thick stratum of material of light density, and that if this stratum extends to Crisfield, it is considerably thinner at the latter station. The reasoning employed in the discussion of the pre-Cambrian anomalies on pages 72 to 74 would indicate that the large Cenozoic anomalies must be due largely to local causes, if it is assumed that an area under investigation is in a state of perfect isostatic equilibrium.

The data in the table on page 63 indicate that there is strong evidence that the coast stations tend to have negative anomalies. In the table given on page 79 there are shown the anomalies at the Cenozoic stations back from the coast. Of the 19 stations there are 8 with positive and 11 with negative 1912 anomalies, but the mean anomaly with regard to sign is -0.009 dyne. If, however, we eliminate the Seattle anomaly, which is -0.093 , and the anomaly of station 93 (Wilmer, Ala.), which is -0.044 dyne, there would be 8 positive and 9 negative anomalies and the mean with regard to sign would be only -0.001 dyne.

This is practically normal on an average. It may indicate that the Cenozoic material in the interior of the country is not of great thickness, or that, if thick, it is of considerable horizontal extent, or that the materials under the Cenozoic stratum have densities which are greater than the normal. Of course, the anomaly may in part be caused by a lack of perfect compensation. The Bouguer anomalies at the 17 stations under consideration indicate that there is considerable isostatic compensation under these stations.

There is evidently a definite relation between the coasts and the gravity anomaly, but it may be due to the presence of Cenozoic materials which extend along practically all of the coasts. The cause of the difference in the size of the anomalies at different stations may be

due to the varying thickness of the material and the varying horizontal dimensions of thick and thin strata.

That the Cenozoic areas are undercompensated, as the negative anomalies might indicate, does not seem to be true, for the reason that these areas are areas of deposition in recent times and the areas have probably been sinking during the time when materials were accumulating on them. This deposition of material would lead one to suppose that the crust under such areas is heavier than normal. Undercompensation therefore appears to be improbable. The writer is aware that there may be even in areas of heavy deposition sections which are undercompensated, but this would be due to conditions existing before deposition began.

The 1916 anomalies at Cenozoic stations show greater differences from the 1912 anomalies than they do for the other formations considered above. In most cases, where there are decided differences, the stations are on or near the coasts near where there is deep water. The computed effect, which is positive at a land station, of the compensation under the water is greater when it is farther from the surface, for the effect of lengthening the distance to the effective center of the attracting mass is more than offset by the increase in the sine of the angle of depression to the effective center. The effect of a mass in the earth's crust on the attracted unit mass is directly proportional to the sine of the angle of depression to the effective center of the attracting mass and inversely proportional to the square of the distance.

The coast stations would therefore have a smaller computed gravity with the depth of 60 km. than with a depth of 113.7 km. Consequently the negative anomalies would be reduced in size and the positive anomalies increased. For the coast stations the new depth (60 km.) gives a mean anomaly with regard to sign of -0.003 dyne, while with a depth of 113.7 km. the mean is -0.009 dyne. The new mean is nearer zero, but it is uncertain whether this is an indication that the smaller depth is nearer the truth. The discussion above shows that the negative anomalies based on the old depth may be accounted for in general by lighter material in the upper crust.

ANOMALIES ON INTRUSIVE FORMATIONS.

The number of stations in intrusive areas is only 7, of which 2 are positive and 5 negative. While there are two and one-half times as many negative as positive anomalies, we would not be justified in deciding that there is a definite relation between the intrusive formation and the gravity anomalies. Many additional stations would have to be established on this formation before any decision can be arrived at in the matter. The mean of the 1916 anomalies is slightly smaller than that of the 1912 anomalies and this may be an indication that the new depth, 60 km., is nearer the truth than the older depth of 113.7 km.

ANOMALIES ON EFFUSIVE FORMATIONS.

On this formation there are eight stations and of the 1912 anomalies 2 are positive and 6 negative. The mean with regard to sign is -0.005 dyne and without regard to sign it is 0.015 dyne. The largest anomaly is only 0.028 dyne. Of the 1916 anomalies 5 are positive, 2 negative, and 1 zero. The means with and without regard to sign are, respectively, $+0.010$ and 0.019 dyne.

There seems to be no relation between this formation and the anomalies, but the indications are very slightly in favor of the greater depth of compensation for the effusive areas. It would be of interest and value to have additional stations in areas covered by this formation.

ANOMALIES ON UNCLASSIFIED FORMATIONS.

These stations, as the designation implies, could not be associated with any particular formations, and it is not possible to draw any conclusions from a study of their relations.

Of the 26 unclassified stations 18 have positive and only 8 negative 1912 anomalies. This is what might be expected for the mean anomaly with regard to sign of all the 219 stations is made practically zero (only -0.002 dyne) by the use of the 1912 formula. A greater number of stations are in the Paleozoic, Cenozoic, Intrusive, and Effusive formations, which tend to be negative, than in the pre-Cambrian and Mesozoic formations, which tend to be positive, there-

fore to have the mean of all stations with regard to sign nearly zero there would be a tendency for the unclassified stations to be positive.

The 1916 anomalies, with depth of 60 km., are practically the same as the 1912 anomalies with the depth of 113.7 km.

An effort was made to learn whether under any one formation the plus anomalies occurred more frequently in proportion in one subdivision than in others. No such relationship between the sign of the anomaly and the subdivision of a principal geological formation could be found. For instance, in the Quaternary division of the Cenozoic there are 11 stations with positive and 19 with negative anomalies, or 37 per cent positive. In the whole Cenozoic formation there are 22 positive and 32 negative anomalies, the positive anomalies being 41 per cent of all. Like results were obtained from other tests. It appears then that the sign of the anomaly is in some way connected with a large geologic division as a whole and not with one of its subdivisions.

RELATION BETWEEN THE GRAVITY ANOMALIES AND THE GEOLOGIC FORMATION AT STATIONS IN THE UNITED STATES NOT WITHIN 20 MILES OF ANOTHER FORMATION.

In making the study of the relation between the gravity anomalies and the geological formation those stations which were not within 20 miles of other formations were separated and the data tabulated. These stations and their anomalies are shown in the following tables. The results are practically the same as when all stations on a formation are considered. For instance, for the Cenozoic stations 65 per cent are negative, while for all stations in that formation 59 per cent are negative. The mean with regard to sign is -0.010 dyne for the Cenozoic stations in the table below, while it is -0.007 for all stations in this formation. (See table on p. 72.) A similar condition exists for the other formations. The Effusive and Intrusive formations have so few stations which are not close to other formations that data for them are not given.

The table given below also contains data for 19 Cenozoic stations not on the coast and not within 20 miles of any other formation. If the two Seattle stations are counted as one, the mean with regard to sign is -0.009 , while without the Seattle value the mean is -0.004 . As the effect of the coast is not present, these mean values show a decided relation between the anomalies and the Cenozoic formation.

Hayford anomalies for stations in the United States on specified formations and not within 20 miles of other formations.

Formation and station number	Hayford anomaly		Formation and station number	Hayford anomaly		Formation and station number	Hayford anomaly	
	1912	1916		1912	1916		1912	1916
Pre-Cambrian formations:			Paleozoic formation—Con.			Paleozoic formation—Con.		
57.....	+0.038	+0.041	105.....	-0.021	-0.017	176.....	-0.024	-0.022
58.....	+ .023	+ .023	106.....	- .013	- .014	177.....	+ .001	+ .000
107.....	+ .024	+ .026	120.....	- .008	- .008	178.....	+ .001	+ .002
185.....	+ .012	+ .012	121.....	+ .002	+ .002	179.....	- .025	- .027
191.....	+ .011	+ .008	122.....	+ .011	+ .012	181.....	+ .015	+ .015
Paleozoic formation:			123.....	- .043	- .041	182.....	- .050	- .051
12.....	- .027	- .028	133.....	- .030	- .024	184.....	- .027	- .028
14.....	+ .026	+ .028	134.....	- .027	- .027	196.....	+ .036	+ .035
20.....	+ .010	+ .022	135.....	- .024	- .023	204.....	- .026	- .025
32.....	- .023	- .020	136.....	- .012	- .011			
33.....	- .003	- .003	137.....	+ .001	+ .002	207.....	- .029	- .026
34.....	- .019	- .019	138.....	- .016	- .017	208.....	- .008	- .008
35.....	- .009	- .010	139.....	+ .011	+ .012	211.....	- .023	- .022
36.....	- .007	- .009	140.....	+ .016	+ .016			
37.....	- .005	- .005	141.....	- .016	- .018	Mesozoic formation:		
38.....	- .005	- .007	143.....	+ .018	+ .018	40.....	+ .014	+ .012
39.....	- .016	- .018	153.....	- .023	- .020	46.....	+ .024	+ .024
59.....	+ .019	+ .015	155.....	- .021	- .019	47.....	- .021	- .025
61.....	- .029	- .028	156.....	- .015	- .007	62.....	+ .031	+ .035
72.....	+ .032	+ .034	166.....	- .023	- .021	70.....	- .013	- .001
74.....	+ .059	+ .067						
88.....	- .010	- .013	169.....	+ .013	+ .013	73.....	+ .005	+ .004
89.....	- .020	- .019	170.....	+ .006	+ .007	76.....	+ .002	+ .000
96.....	- .052	- .051	171.....	- .030	- .026	77.....	+ .029	+ .024
101.....	+ .040	+ .045	172.....	- .034	- .027	94.....	- .017	- .017
104.....	- .024	- .024	174.....	- .033	- .030	108.....	- .006	- .008

Hayford anomalies for stations in the United States on specified formations and not within 20 miles of other formations—Continued.

Formation and station number	Hayford anomaly		Formation and station number	Hayford anomaly		Formation and station number	Hayford anomaly	
	1912	1916		1912	1916		1912	1916
Mesozoic formation—Con.			Cenozoic formation—Con.			Cenozoic formation, away from coast—Continued.		
118.....	+0.014	+0.009	97.....	-0.012	-0.013	93.....	-0.044	-0.042
186.....	+0.012	+0.009	99.....	-0.016	-0.013	95.....	+0.001	-0.002
187.....	+0.015	+0.014	112.....	+0.033	+0.029	97.....	-0.012	-0.013
189.....	+0.032	+0.030	125.....	-0.023	-0.018	99.....	-0.016	-0.013
193.....	+0.030	+0.028	126.....	-0.022	-0.016	112.....	+0.033	+0.029
202.....	+0.021	+0.024	127.....	-0.014	-0.007	142.....	+0.011	+0.009
Cenozoic formation:			142.....	+0.011	+0.009	144.....	-0.006	-0.005
1.....	+0.005	+0.015	144.....	-0.006	-0.005	145.....	+0.014	+0.016
2.....	+0.018	+0.027	145.....	+0.014	+0.016	158.....	-0.017	-0.010
3.....	+0.010	+0.017	157.....	-0.036	-0.026	160.....	-0.014	-0.008
4.....	-0.000	+0.004	158.....	-0.017	-0.010	163.....	+0.002	+0.005
5.....	-0.013	-0.010	159.....	-0.001	+0.007	167.....	-0.012	-0.012
6.....	+0.016	+0.017	160.....	-0.014	-0.008	168.....	+0.013	+0.012
7.....	-0.009	-0.008	161.....	-0.021	-0.016	190.....	+0.017	+0.015
8.....	+0.027	+0.030	163.....	+0.002	+0.005	215.....	-0.029	-0.023
9.....	-0.020	-0.022	164.....	-0.014	-0.010	Effusive and intrusive formations:		
17.....	-0.021	-0.016	167.....	-0.012	-0.012	50.....	-0.002	+0.017
18.....	-0.021	-0.008	168.....	+0.013	+0.012	51.....	+0.021	+0.038
53.....	-0.093	-0.100	190.....	+0.017	+0.015	52.....	-0.001	+0.015
56.....	-0.050	-0.049	215.....	-0.029	-0.023	111.....	-0.028	-0.019
66.....	-0.050	-0.049	217.....	-0.010	-0.006	113.....	-0.027	-0.030
80.....	-0.013	-0.010	Cenozoic formation, away from coast:					
83.....	-0.006	-0.005	6.....	+0.016	+0.017			
90.....	-0.048	-0.039	9.....	-0.020	-0.022			
92.....	+0.010	+0.015	53.....	-0.093	-0.100			
93.....	-0.044	-0.043	56.....	-0.093	-0.100			
95.....	+0.001	-0.002	83.....	-0.006	-0.005			

SUMMARY.

Geologic formation	Number of stations					Mean anomaly			
	With plus anomalies		With minus anomalies		All	With regard to sign.		Without regard to sign	
	1912	1916	1912	1916		1912	1916	1912	1916
Pre-Cambrian.....	5	5	0	0	5	+0.022	+0.022	0.022	0.022
Paleozoic.....	18	17	39	39	57	-0.009	-0.008	-0.020	-0.020
Mesozoic.....	12	11	4	4	16	+0.011	+0.010	-0.018	-0.017
Cenozoic.....	13	14	26	26	40	-0.010	-0.007	-0.019	-0.018
Cenozoic ^a	13	14	25	25	39	-0.008	-0.005	-0.017	-0.016
Cenozoic, away from coast ^b	8	7	11	12	19	-0.009	-0.008	-0.020	-0.019
Cenozoic, away from coast ^a	8	7	10	11	18	-0.004	-0.003	-0.016	-0.014
Effusive and intrusive.....	1	3	4	2	5	-0.007	+0.004	-0.016	-0.024

^a With Seattle stations omitted.

^b With the two Seattle stations counted as one.

RELATION BETWEEN THE GRAVITY ANOMALIES AND THE GEOLOGIC FORMATION FOR STATIONS IN CANADA.

There are 42 stations in Canada for which the principal facts are given in the table on page 54. The stations with their anomalies (Hayford, 1912) arranged according to the geologic formations are given in the following table:

Canadian stations and Hayford anomalies for specified formations.

Formation and station number	Hayford anomaly 1912	Formation and station number	Hayford anomaly 1912	Formation and station number	Hayford anomaly 1912	Formation and station number	Hayford anomaly 1912
Pre-Cambrian formations:		Paleozoic formation:		Paleozoic formation—Continued.		Unclassified:	
2.....	-0.010	1.....	-0.018	28.....	-0.026	23.....	-0.006
4.....	-0.028	3.....	-0.012	29.....	+0.008	24.....	-0.029
5.....	+0.001	6.....	-0.005	31.....	-0.009	26.....	-0.023
9.....	-0.030	7.....	+0.011	37.....	-0.011	36.....	+0.007
10.....	-0.002	8.....	+0.006			39.....	-0.009
		12.....	-0.021	Mesozoic formation:		40.....	-0.008
11.....	-0.022	16.....	-0.034	32.....	+0.007		
13.....	+0.004	17.....	-0.012	33.....	-0.005		
14.....	-0.045	18.....	+0.012	34.....	-0.006		
15.....	+0.006	19.....					
25.....	+0.011	20.....	+0.006	Cenozoic formation:			
30.....	+0.001	21.....	-0.006	35.....	-0.004		
38.....	-0.043	22.....	-0.016	42.....	-0.016		
41.....	+0.002	27.....	-0.009				
			-0.011				

SUMMARY.

Geological formation	Number of stations			Mean anomaly	
	All	With plus anomalies	With minus anomalies	With regard to sign	Without regard to sign
Pre-Cambrian.....	13	6	7	-0.012	0.016
Paleozoic.....	18	5	13	-0.008	.013
Mesozoic.....	3	1	2	-0.001	.006
Cenozoic.....	2	0	2	-0.010	.010
Unclassified.....	6	1	5	-0.011	.014
All stations.....	42	13	29	-0.009	.013

It is a fact worthy of careful consideration that the mean without regard to sign for the Canadian stations is only 0.013 dyne while for the stations in the United States the mean is 0.019 dyne. There are only three stations (7 per cent of all) in Canada with anomalies greater than 0.030 dyne, while in the United States there are 40 stations (18 per cent of all) with anomalies greater than that amount.

The mean with regard to sign for the Canadian anomalies is -0.009 dyne, while in the United States it is -0.002 dyne. The anomalies are computed with the 1912 formula with the depth of 113.7 km., so they are comparable with the 1912 anomalies in the United States. The writer can see no cause for the mean with regard to sign being so far from that of the United States. Nor can he see any reason why the mean without regard to sign for Canadian stations is so much smaller than for the stations in the United States. The latter is an indication that the area covered by the Canadian stations is more nearly in a state of perfect isostasy locally.

The mean with regard to sign for the stations in the pre-Cambrian formation is -0.012, which is only 0.003 from the mean of all, and for the Paleozoic and Cenozoic formations the means differ only 0.001 dyne from the mean of all. The mean without regard to sign for the three Mesozoic stations is -0.001 dyne, which is 0.008 from the mean of all, but this has little significance as there are so few stations.

The conclusion must be drawn that there is no apparent relation between the geologic formation and the gravity anomalies at stations in Canada.

RELATION BETWEEN THE GRAVITY ANOMALIES AND THE GEOLOGIC FORMATION FOR STATIONS IN INDIA.

In the table below the stations in India are arranged in groups according to the geologic formation. In order to decide on what formations the stations are located, they were plotted on a geologic map in the 1890 report of the Geological Survey of India. (See p. 70).

Indian stations and Hayford anomalies for specified formations.

Formation and station number	Hayford anomaly, 1912	Formation and station number	Hayford anomaly, 1912	Formation and station number	Hayford anomaly, 1912
Pre-Cambrian formations:		Cenozoic formation—Continued.		Effusive formation:	
42.....	+0.007	16.....	-0.003	5.....	+0.019
43.....	+ .023	22.....	- .002	8.....	+ .023
82.....	+ .008	26.....	+ .024	14.....	+ .018
84.....	+ .001	29.....	- .005	17.....	+ .065
		30.....	- .003	31.....	+ .012
91.....	+ .023			45.....	+ .083
94.....	- .056	32.....	- .078	50.....	+ .039
95.....	+ .046	35.....	+ .003	55.....	- .022
108.....	- .039	38.....	+ .030	73.....	- .027
		40.....	- .028	97.....	+ .008
		44.....	- .015	98.....	+ .029
Paleozoic formation:				106.....	- .018
13.....	+ .006	51.....	- .027		
20.....	- .004	52.....	+ .031	Unclassified:	
48.....	- .000	58.....	- .061	4.....	- .011
		60.....	- .065	9.....	+ .031
59.....	- .011	66.....	+ .033	12.....	+ .014
88.....	- .010			18.....	- .002
103.....	+ .021	67.....	- .013	19.....	+ .017
Mesozoic formation:		70.....	- .033	24.....	- .013
107.....	+ .022	71.....	+ .011	33.....	- .015
		77.....	+ .007	37.....	+ .013
		78.....	- .050	39.....	+ .012
Cenozoic formation:				41.....	- .006
1.....	+ .009	83.....	- .063	55.....	- .009
2.....	- .014	89.....	+ .019	72.....	- .003
3.....	+ .001	92.....	- .052	75.....	+ .047
6.....	- .036	96.....	+ .001	87.....	+ .001
15.....	- .022	100.....	- .066	99.....	+ .016
		101.....	- .047		

SUMMARY.

Geological formation	Number of stations			Mean anomaly	
	All	With plus anomalies	With minus anomalies	With regard to sign	Without regard to sign
Pre-Cambrian.....	8	6	2	+0.002	0.025
Paleozoic.....	6	2	3	- .000	.009
Mesozoic.....	1	1	0	+ .022	.022
Cenozoic.....	31	11	20	- .017	.028
Effusive.....	12	9	3	+ .014	.025
Unclassified.....	15	8	7	+ .006	.014
All stations.....	73	37	35	- .004	.023

The anomalies are based upon the United States Coast and Geodetic Survey formula of 1912, and hence are comparable with the 1912 anomalies in Canada and in the United States. The mean with regard to sign is -0.004 , and this differs only 0.002 from the mean in the United States, which is -0.002 dyne.

If the latest value of gravity for the base station, Dehra Dun, 979.065 dynes, had been used instead of 979.063 dynes, (see p. 55), the observed values in India would each be greater by 0.002 dyne. Then the mean with regard to sign would be -0.002 , the same as for the United States.

There are 8 stations in pre-Cambrian formations in India, of which 6 have positive anomalies and 2 negative anomalies. The two stations, Nos. 94 and 108, with negative anomalies, which are quite large, and one station, No. 82, with a rather small positive anomaly, are in the extreme southern part of the Indian Peninsula on a very extensive area of pre-Cambrian formation. The wide extent of this area would probably prevent the existence of large positive anomalies (see p. 72) in spite of the density, greater than normal, of the surface and subsurface rocks, but there must be in addition some unusual local deficiency in the underlying matter in order to

account for these large negative anomalies. Stations 94 and 108 are only about 8 miles apart and should really be considered as only one station, as both must be affected by the same anomalous condition. The mean anomaly at these two stations is -0.048 . If these two stations were considered as one, then there would be 6 pre-Cambrian stations with positive anomalies and only 1 with negative anomaly and the mean with regard to sign for this group would be $+0.009$, which is of the same sign and about one-third the size of the corresponding value for United States pre-Cambrian stations. With the exception of the three stations, 82, 94, and 108, noted above, all the pre-Cambrian stations are situated on less widely extended areas and have positive anomalies, but there is no striking relation between the extent of the area and the magnitude of the anomaly except perhaps at station 43, Jubbulpore, which is on a very limited area of the formation. The map does not indicate the extent of the formation around station 95, Sandakphu.

There seems to be no relation between the anomaly and the Paleozoic formation, as the mean anomaly is nearly normal. This fact should not be given much consideration, as there are comparatively few stations in this formation.

The Mesozoic formation has only one station, and that can not be considered as representing any relation whatever.

The Cenozoic formation has 42 per cent of all the stations and has the only negative mean anomaly with regard to sign. This mean anomaly is -0.017 . It agrees in sign, but is much larger than the Cenozoic mean anomaly with regard to sign in the United States, which is -0.007 dyne. All of the Indian Cenozoic stations are back from the coast except one, and it must be concluded that there is a very definite relation between the anomalies and the Cenozoic formation. On page 76 the question was discussed as to whether the Cenozoic formation or the proximity to the open coast was the cause of the negative anomalies at coast stations. The 31 Cenozoic anomalies in India seem to prove that this formation is the main cause of the negative anomalies.

Many of the Cenozoic stations in India are in areas to which great quantities of material have been carried from the Himalaya Mountains. It is probable that the larger Cenozoic anomalies are above portions of the crust where the recent material is thick and of limited horizontal extent. (See discussion under "pre-Cambrian anomalies," pp. 72 to 74.)

It has been held by some geodesists in India^a that there is probably a rift in the earth's crust where the large negative anomalies exist. The evidence at hand makes it possible to account for the anomalies by the Cenozoic formation in the affected area.

Of course, it is probable that in India, as in other countries, there are local, and in some areas regional, departures from a state of perfect isostasy, but as evidence in the form of gravity stations accumulates the theory of isostasy is given added strength.

The effect of the change of depth from 113.7 km. to 60 km. is discussed at some length on pages 97 to 112. It should be noticed that the general effect of the change in the depth is slight, though in a few cases it is comparatively large. The anomalies, not being materially changed by a decided change in depth, are dependent upon some other condition or conditions in the earth's crust than an erroneous depth.

The summaries on pages 72 and 81, which give evidence for stations in the United States and India, respectively, point strongly to rather definite relations between the sign of the anomaly and the surface geology at the station. This relation may be due to variation from the normal density for strata in the upper crust, these abnormal densities being compensated for by a counterbalancing change in density occurring in the lower crust, possibly to the depth of compensation.

RELATION BETWEEN THE GRAVITY ANOMALIES AND THE GEOLOGIC FORMATION SHOWN GRAPHICALLY.

In figure 17 there are shown areas which have certain geologic formations at the surface of the earth. The outlines of the areas were copied from the geologic map of North America mentioned on page 70. The scale of this illustration is the same as for those which show the

^a Survey of India, Professional Paper No. 12, On the Origin of the Himalaya Mountains, by Col. S. G. Burrard, p. 5.

gravity anomaly contours (figs. 11 to 14). The Cenozoic and Paleozoic areas are shown in yellow, which is also used on the anomaly maps to show the negative areas. The pre-Cambrian and Mesozoic areas are shown in green, the color used to indicate positive areas on the anomaly illustrations.

The largest continuous area is for the Paleozoic formation, and extends from eastern New York westward to Minnesota, southwestward to Texas, and southward to Alabama. There is practically no portion of this area with any material other than that of the Paleozoic. There is a striking similarity between this Paleozoic area and the very extensive negative area which extends from New England westward to Iowa and Missouri, as shown in figure 11, which shows the Hayford 1912 anomalies. A break in this negative area occurs in Michigan, Ohio, and Indiana, where there are four stations with positive anomalies; but their size is small, the maximum anomaly being only $+0.012$ dyne. Within this large Paleozoic area there are 52 stations with negative anomalies and only 23 with positive anomalies.

Along the Atlantic coast from New York City southward and along all of the Gulf coast the geologic formation is Cenozoic, except for a small break on the coast of South Carolina. Figure 17 gives the limits of the coastal areas belonging to this formation (shown in yellow). A comparison with figure 11 shows that there is some similarity between the negative areas and the Cenozoic areas near the coast. They agree more closely very near the coast.

There is an extensive area in Minnesota, South Dakota, and North Dakota within which the geology is largely pre-Cambrian and Mesozoic. There is a second pre-Cambrian and Mesozoic area in Montana and Wyoming. Between these two areas there is an area in which the geology is largely Cenozoic. The gravity anomaly map (fig. 11) shows that there are no negative anomalies within the limits of the above three areas. There are only two stations in the intervening Cenozoic area, however. It is worthy of note that there is a narrow extension of the first-mentioned pre-Cambrian and Mesozoic area southward into Nebraska and Kansas, and that a positive area in figure 11 coincides approximately with this extension.

A narrow strip of nearly all Cenozoic formation extends southward from South Dakota to Texas and New Mexico. A band of negative area in figure 11 partly coincides with this Cenozoic region. If more stations were established within the two areas, they would possibly coincide more nearly.

In western and central Texas there is an area mostly of Mesozoic formation. Figure 11 shows only three stations within the area, and two are positive. The other station, at Austin, is negative, but is very close to the border of the area under consideration. The contours are drawn in such a way as to make negative nearly one-half the area.

A long strip of pre-Cambrian or Mesozoic formation (including a few small areas of other formations) extends from the Hudson River southwestward along the Appalachian Mountains to Alabama, thence northward in a very narrow band to western Kentucky. There is some similarity between this area and the areas of positive anomaly which extend along the Appalachian system from New York to Georgia and Alabama.

In northern Michigan and Wisconsin and across the international boundary there is an area of pre-Cambrian formation in which all of the stations of the United States have positive anomalies.

That portion of the United States which has not been considered above has no extensive area in which there is only one geologic formation or combinations of pre-Cambrian and Mesozoic or of Paleozoic and Cenozoic. It is interesting to note that in the remainder of the United States, not colored in figure 17, the gravity contours show that there are no steep contours except in the vicinity of Seattle. The western part of the United States is largely negative, but the characteristics of the contours would no doubt be changed greatly by the addition of new stations.

We must conclude that the data contained in figures 11 and 17 substantiate the evidence given in the table on pages 71 and 72 that the pre-Cambrian and Mesozoic areas have in general positive anomalies and that the Paleozoic and Cenozoic areas have a strong tendency to negative anomalies.

RELATION BETWEEN THE GRAVITY ANOMALIES AND AREAS OF EROSION AND DEPOSITION.

It has been shown that there is a rather definite relation between the gravity anomalies and certain geologic formations and that there is also a relation between the anomalies and the topography for coast stations. (See pp. 70 to 83 and also pp. 63 to 69.) It has been indicated that this relation at coast stations is due to the fact that along most of the coast the materials, at least at the surface, belong to the Cenozoic geologic formation. (See p. 76.)

It is probably true that along the whole coast of the United States deposition of the material has been taking place in recent geologic time. The natural assumption would be that this deposited material is an extra load on the earth's crust and that in consequence observed gravity should be in excess of the computed gravity. This, however, is not the case. An inspection of the gravity anomaly map, figure 11, shows that along the coasts observed gravity is, in general, less than the computed gravity.

The logical conclusion from all available data seems to be that isostasy along the coasts is nearly perfect on the whole and that the computed gravity is too great because the materials in the upper crust are less than normal. According to Barrell the densities of Cenozoic matter vary from 2.40 to 2.50, while on an average the density for the whole land surface of the earth is about 2.67, the value used in the computations in this volume. It seems probable that as the materials are deposited along the coasts isostatic adjustment takes place and the pressure at the depth of compensation is in general normal. In the interior of the country the areas covered by the Cenozoic formation, which are likewise areas of recent deposition, are largely negative, as shown in figure 11. This is a condition similar to that found along the coasts.

The areas of recent erosion are greater than those of recent deposition. They are areas within which theoretically the gravity anomalies should be negative, but there appears to be no such relation. In fact, the oldest formations which no doubt have been subjected to the greatest erosion are in general areas of positive anomalies. This is shown by a comparison of figures 11 and 17, one of which shows the gravity anomalies and areas of negative and positive anomalies and the other limits of large areas of certain geologic formations. The pre-Cambrian formation which has been longest exposed to erosion is, in the United States, a formation in which the gravity anomalies have a very strong tendency to be positive.

It is probable that the positive anomalies at stations in the pre-Cambrian formation are due largely to the density greater than 2.67 in the material above sea level and also to a density greater than normal in the strata in the upper crust below sea level. (See pp. 72 and 81.) No assumption need be made in regard to what is the normal density of the materials in a stratum at a certain depth below sea level. It is only the deviation from the normal with which we are concerned.

The mountain regions have a number of stations above the general level. They are all included in areas which have been and are now subject to erosion. There seems to be no relation between the anomalies and the topography in these cases.

In India there is a broad belt of recent geologic material running approximately east and west at the foot of the Himalaya Mountains. The stations on this recent formation, which no doubt is largely due to the deposition of materials eroded from the mountains, have in general negative anomalies. It is impossible that the addition of materials could make the pressure less than normal on the surface at the depth of compensation. We may therefore conclude that isostatic adjustment probably follows the deposition of materials and that the negative anomaly is probably due to the lighter materials in the upper crust. (See p. 82.)

There seems to be no effect due to the melting of the ice cap on the size and sign of the gravity anomaly. This is evidenced by a study of figure 11. If isostasy were perfect at the beginning of the ice age and if the isostatic adjustment kept pace with the accumulation of ice, there must have been an adjustment of opposite sign, upon the melting of the ice, for on an average the area that was covered by the sheet of ice is very close to a state of equilibrium now.

Chapter VI.—REGIONAL VERSUS LOCAL DISTRIBUTION OF COMPENSATION.

On pages 98 to 102 of Special Publication No. 10 there is a discussion of this subject based upon data for 41 stations in the United States and 4 stations not in this country. Similar data are now available for 124 stations in the United States.

The question to be considered is whether a topographic feature is compensated for by a deficiency of mass directly under it, or whether the topographic feature is compensated for by a deficiency of mass distributed through a more extensive portion of the earth's crust than that directly beneath the feature.

The theory of local compensation postulates that the deficiency of mass under any topographic feature is uniformly distributed in a column extending directly from the topographic feature vertically to a certain depth. In this discussion the depth is taken as 113.7 km. This depth is the one used in making the reduction for topography and isostatic compensation.

The theory of regional compensation postulates, on the other hand, that an individual topographic feature is compensated for by a deficiency of mass equal in amount to the topography, but of opposite sign, and that this deficiency is uniformly distributed from the surface to the depth of compensation, but has a horizontal extent greater than that of the feature itself.

The method of computing the data need not be given here, as the reader can learn of this by consulting pages 98 and 99 of Special Publication No. 10.

The table following gives the data for 124 stations in the United States. In column 1 are given the number and name of the stations. The effect of topography and compensation computed on the theory of complete local isostasy is given for each station in the second column. In columns 3, 5, and 7 are given the effect of local compensation out to the outer limits of zones K, M, and O, respectively, while in columns 4, 6, and 8 are given the effect of compensation computed upon the theory that the compensation is uniformly distributed horizontally to the outer limits of zones K, M, and O, respectively. In column 9 are given the Hayford anomalies based on complete local compensation. These are what are called the 1912 anomalies. (See p. 53.) They are computed by the 1912 Coast and Geodetic Survey formula and upon the assumption that the depth of compensation is 113.7 km. In the last three columns are given the anomalies for the three methods of regional distribution of compensation with a depth of compensation of 113.7 km.

Comparison between local and regional isostatic compensation.

Number and name of station	Effect of topography and compensation	Effect of compensation within outer limit of—						Hayford anomaly, 1912	Anomaly with regional compensation within outer limit of—		
		Zone K (18.8 km.)		Zone M (58.8 km.)		Zone O (166.7 km.)			Zone K	Zone M	Zone O
		Local	Regional	Local	Regional	Local	Regional				
1. Key West, Fla.	+0.032	0.000	0.000	+0.001	+0.003	+0.010	+0.021	+0.008	+0.008	+0.006	—0.003
2. West Palm Beach, Fla.	+ .031	.000	+ .001	+ .003	+ .005	+ .007	+ .009	+ .018	+ .017	+ .016	+ .016
3. Punta Gorda, Fla.	+ .030	.000	.000	.000	.000	.000	.000	+ .010	+ .010	+ .010	+ .010
4. Apalachicola, Fla.	+ .015	.000	.000	.000	.000	+ .001	+ .001	.000	.000	.000	.000
5. New Orleans, La.	+ .013	.000	.000	.000	.000	.000	.000	— .013	— .013	— .013	— .013
6. Rayville, La.	+ .008	.000	— .001	.000	— .001	.000	— .003	+ .016	+ .017	+ .017	+ .019
7. Galveston, Tex.	+ .007	.000	.000	.000	.000	.000	.000	— .009	— .009	— .009	— .009
8. Point Isabel, Tex.	+ .015	.000	.000	.000	.000	+ .003	+ .006	+ .027	+ .027	+ .027	+ .024
9. Laredo, Tex.	+ .003	.000	— .002	— .004	— .007	— .009	— .012	— .020	— .018	— .017	— .017
10. Austin, Tex. (State capital) ..	— .002	— .003	— .003	— .009	— .010	— .018	— .019	— .008	— .008	— .007	— .007

Comparison between local and regional isostatic compensation—Continued.

Number and name of station	Effect of topography and compensation	Effect of compensation within outer limit of—						Hayford anomaly, 1912	Anomaly with regional compensation within outer limit of—		
		Zone K (18.8 km.)		Zone M (58.8 km.)		Zone O (166.7 km.)			Zone K	Zone M	Zone O
		Local	Regional	Local	Regional	Local	Regional				
11. Austin, Tex. (university).....	-0.001	-0.003	-0.003	-0.009	-0.010	-0.018	-0.019	-0.010	-0.010	-0.009	-0.009
12. McAlester, Okla.....	+ .001	- .003	- .004	- .010	- .010	- .017	- .017	- .027	- .026	- .027	- .027
13. Little Rock, Ark.....	+ .001	.000	- .002	- .002	- .005	- .008	- .014	+ .030	+ .032	+ .033	+ .036
14. Columbia, Tenn.....	+ .006	- .004	- .004	- .009	- .009	- .017	- .017	+ .026	+ .026	+ .026	+ .026
15. Atlanta, Ga.....	+ .014	- .004	- .005	- .011	- .013	- .021	- .022	- .023	- .022	- .021	- .022
16. McCormick, S. C.....	+ .012	- .002	- .002	- .006	- .007	- .012	- .015	+ .015	+ .015	+ .016	+ .018
17. Charleston, S. C.....	+ .016	.000	.000	.000	.000	.000	+ .001	- .021	- .021	- .021	- .022
18. Beaufort, N. C.....	+ .036	.000	.000	.000	.000	+ .005	+ .017	- .021	- .021	- .021	- .033
19. Charlottesville, Va.....	+ .002	- .002	- .003	- .010	- .011	- .020	- .024	- .013	- .012	- .012	- .009
20. Deer Park, Md.....	+ .041	- .013	- .015	- .029	- .026	- .044	- .035	+ .010	+ .012	+ .007	+ .001
21. Washington, D. C. (Coast Geodetic Survey Office).....	+ .004	.000	- .001	- .001	- .003	- .005	- .009	+ .037	+ .038	+ .039	+ .041
22. Washington, D. C. (Smithsonian Institution).....	+ .003	.000	- .001	- .001	- .003	- .005	- .009	+ .039	+ .040	+ .041	+ .043
23. Baltimore, Md.....	+ .006	.000	- .001	- .001	- .003	- .005	- .009	+ .011	- .010	- .009	- .007
24. Philadelphia, Pa.....	+ .009	.000	- .001	- .001	- .002	- .004	- .007	+ .022	+ .023	+ .023	+ .025
25. Princeton, N. J.....	+ .013	.000	- .001	- .001	- .003	- .005	- .008	- .019	- .018	- .017	- .016
26. Hoboken, N. J.....	+ .008	.000	.000	- .001	- .002	- .005	- .009	+ .024	+ .024	+ .025	+ .028
27. New York, N. Y.....	+ .011	.000	.000	- .001	- .002	- .006	- .009	+ .022	+ .022	+ .023	+ .025
28. Worcester, Mass.....	+ .018	- .002	- .003	- .007	- .008	- .012	- .011	- .020	- .019	- .019	- .021
29. Boston, Mass.....	+ .013	.000	.000	.000	.001	- .002	- .005	+ .005	+ .005	+ .006	+ .008
30. Cambridge, Mass.....	+ .010	.000	.000	- .002	- .001	- .005	- .005	+ .005	+ .005	+ .004	+ .005
31. Calais, Me.....	+ .010	.000	.000	- .001	- .002	- .003	- .005	- .008	- .008	- .007	- .006
32. Ithaca, N. Y.....	+ .005	- .003	- .005	- .011	- .013	- .023	- .026	- .023	- .021	- .021	- .020
33. Cleveland, Ohio.....	.000	- .004	- .004	- .010	- .010	- .019	- .019	- .003	- .003	- .003	- .003
34. Cincinnati, Ohio.....	+ .002	- .004	- .004	- .010	- .009	- .020	- .019	- .019	- .019	- .020	- .020
35. Terre Haute, Ind.....	+ .001	- .002	- .002	- .006	- .007	- .013	- .016	- .009	- .009	- .008	- .006
36. Chicago, Ill.....	+ .007	- .002	- .003	- .005	- .007	- .010	- .014	- .007	- .006	- .005	- .003
37. Madison, Wis.....	+ .003	- .004	- .005	- .012	- .013	- .021	- .020	- .005	- .004	- .004	- .006
38. St. Louis, Mo.....	+ .001	- .001	- .002	- .005	- .007	- .012	- .014	- .005	- .004	- .004	- .003
39. Kansas City, Mo.....	- .001	- .004	- .005	- .012	- .013	- .022	- .023	- .016	- .015	- .015	- .015
40. Ellsworth, Kans.....	- .004	- .007	- .008	- .020	- .021	- .038	- .041	+ .014	+ .015	+ .015	+ .017
41. Wallace, Kans.....	.000	- .018	- .018	- .048	- .048	- .084	- .085	- .012	- .012	- .012	- .011
42. Colorado Springs, Colo.....	- .007	- .036	- .036	- .094	- .093	- .165	- .164	- .007	- .007	- .008	- .008
43. Pikes Peak, Colo.....	+ .187	- .052	- .014	- .113	- .100	- .189	- .172	+ .021	+ .013	+ .008	+ .004
44. Denver, Colo.....	- .015	- .026	- .028	- .076	- .085	- .152	- .169	- .016	- .014	- .007	+ .001
45. Gunnison, Colo.....	- .001	- .041	- .044	- .120	- .128	- .212	- .210	+ .020	+ .023	+ .028	+ .018
46. Grand Junction, Colo.....	- .051	- .026	- .028	- .082	- .089	- .156	- .170	+ .024	+ .026	+ .031	+ .038
47. Green River, Utah.....	- .043	- .021	- .024	- .067	- .074	- .130	- .150	- .021	- .018	- .014	- .001
48. Pleasant Valley Junction, Utah.....	+ .024	- .040	- .041	- .103	- .100	- .171	- .159	+ .004	+ .005	+ .001	- .008
49. Salt Lake City, Utah.....	- .041	- .026	- .028	- .075	- .078	- .137	- .143	+ .010	+ .012	+ .013	+ .016
50. Grand Canyon, Wyo.....	+ .038	- .041	- .042	- .108	- .109	- .180	- .165	- .002	- .001	- .001	- .017
51. Norris Geyser Basin, Wyo.....	+ .031	- .040	- .042	- .104	- .105	- .176	- .163	+ .021	+ .023	+ .022	+ .008
52. Lower Geyser Basin, Wyo.....	+ .028	- .039	- .041	- .103	- .104	- .177	- .169	- .001	+ .001	.000	- .009
53. Seattle, Wash. (university).....	- .020	.000	.000	- .002	- .004	- .020	- .038	- .063	- .093	- .091	- .075
54. San Francisco, Cal.....	+ .045	.000	.000	- .002	- .003	+ .009	+ .033	- .023	- .023	- .022	- .047
55. Mount Hamilton, Cal.....	+ .120	- .012	- .012	- .017	- .009	- .018	- .003	- .003	- .003	- .011	- .018
56. Seattle, Wash. (high school).....	- .018	.000	.000	- .002	- .004	- .020	- .038	- .063	- .093	- .091	- .075
57. Iron River, Mich.....	+ .014	- .007	- .008	- .020	- .020	- .031	- .024	+ .038	+ .039	+ .038	+ .031
58. Ely, Minn.....	+ .008	- .007	- .008	- .019	- .021	- .033	- .029	+ .023	+ .024	+ .025	+ .019
59. Pembina, N. Dak.....	- .009	- .004	- .004	- .011	- .012	- .023	- .025	+ .019	+ .019	+ .020	+ .021
60. Mitchell, S. Dak.....	- .006	- .007	- .007	- .018	- .019	- .035	- .037	+ .001	+ .001	+ .002	+ .003
61. Sweetwater, Tex.....	+ .009	- .011	- .012	- .028	- .029	- .049	- .049	- .029	- .028	- .028	- .029
62. Kerrville, Tex.....	+ .013	- .009	- .010	- .024	- .025	- .038	- .032	+ .031	+ .032	+ .032	+ .025
63. El Paso, Tex.....	+ .001	- .020	- .021	- .054	- .055	- .098	- .104	+ .007	+ .008	+ .008	+ .013
64. Nogales, Ariz.....	+ .038	- .020	- .020	- .046	- .041	- .076	- .069	- .050	- .050	- .055	- .057
65. Yuma, Ariz.....	- .010	- .001	- .001	- .004	- .006	- .012	- .018	+ .009	+ .009	+ .011	+ .015
66. Compton, Cal.....	.000	.000	- .001	- .003	- .004	- .014	- .024	- .050	- .049	- .049	- .040
67. Goldfield, Nev.....	+ .027	- .030	- .030	- .074	- .078	- .134	- .141	- .013	- .013	- .009	- .006
68. Yavapai, Ariz.....	+ .034	- .030	- .030	- .080	- .080	- .137	- .129	+ .001	+ .001	+ .001	- .007
69. Grand Canyon, Ariz.....	- .096	- .028	- .029	- .079	- .080	- .136	- .127	- .010	- .009	- .009	- .019
70. Gallup, N. Mex.....	+ .014	- .036	- .036	- .095	- .095	- .163	- .156	- .013	- .013	- .013	- .020
71. Las Vegas, N. Mex.....	+ .017	- .036	- .035	- .094	- .094	- .160	- .150	+ .003	+ .002	+ .003	- .007
72. Shamrock, Tex.....	+ .007	- .013	- .012	- .031	- .031	- .055	- .056	+ .032	+ .031	+ .032	+ .033
73. Denison, Tex.....	- .001	- .004	- .004	- .010	- .009	- .018	- .017	+ .005	+ .005	+ .004	+ .004
74. Minneapolis, Minn.....	- .005	- .004	- .005	- .012	- .013	- .022	- .024	+ .059	+ .060	+ .060	+ .061
75. Lead, S. Dak.....	+ .044	- .026	- .027	- .064	- .061	- .102	- .099	+ .052	+ .053	+ .049	+ .039
76. Bismarck, N. Dak.....	- .005	- .008	- .009	- .024	- .026	- .044	- .047	+ .002	+ .003	+ .004	+ .005
77. Hinsdale, Mont.....	- .017	- .010	- .012	- .030	- .034	- .058	- .067	+ .029	+ .031	+ .033	+ .038
78. Sandpoint, Idaho.....	- .044	- .014	- .014	- .045	- .049	- .086	- .095	+ .002	+ .002	+ .006	+ .011
79. Boise, Idaho.....	- .042	- .016	- .018	- .047	- .051	- .094	- .108	+ .008	+ .010	+ .012	+ .022
80. Astoria, Oreg.....	+ .008	.000	.000	- .002	- .005	.000	+ .008	- .013	- .013	- .010	- .021

Comparison between local and regional isostatic compensation—Continued.

Number and name of station	Effect of topography and compensation	Effect of compensation within outer limit of—						Hayford anomaly, 1912	Anomaly with regional compensation within outer limit of—		
		Zone K (18.8 km.)		Zone M (58.8 km.)		Zone O (166.7 km.)			Zone K	Zone M	Zone O
		Local	Regional	Local	Regional	Local	Regional				
81. Sisson, Cal.	+0.015	-0.022	-0.026	-0.058	-0.059	-0.096	-0.088	-0.010	-0.006	-0.009	-0.018
82. Rock Springs, Wyo.	-0.01	-0.036	-0.034	-0.093	-0.093	-0.169	-0.177	+0.013	+0.011	+0.013	+0.021
83. Paxton, Nebr.	+0.002	-0.014	-0.016	-0.041	-0.043	-0.073	-0.077	-0.006	-0.004	-0.004	-0.002
84. Washington, D. C. (Bureau of Standards)	+0.012	.000	-0.001	-0.001	-0.003	-0.005	-0.009	+0.037	+0.038	+0.039	+0.041
85. North Hero, Vt.	-0.009	.000	-0.001	-0.003	-0.007	-0.012	-0.016	+0.001	+0.002	+0.005	+0.005
86. Lake Placid, N. Y.	+0.032	-0.011	-0.012	-0.024	-0.021	-0.033	-0.020	+0.006	+0.007	+0.003	-0.007
87. Potsdam, N. Y.	-0.004	-0.002	-0.003	-0.008	-0.010	-0.017	-0.017	+0.021	+0.022	+0.023	+0.021
88. Wilson, N. Y.	-0.002	.000	-0.002	-0.003	-0.004	-0.011	-0.017	-0.010	-0.008	-0.009	-0.004
89. Alpena, Mich.	.000	-0.004	-0.003	-0.010	-0.008	-0.016	-0.016	-0.020	-0.021	-0.022	-0.020
90. Virginia Beach, Va.	+0.025	.000	.000	.000	.000	.000	+0.002	-0.048	-0.048	-0.048	-0.050
91. Durham, N. C.	+0.014	.000	-0.002	-0.004	-0.006	-0.008	-0.010	+0.036	+0.038	+0.038	+0.038
92. Fernandina, Fla.	+0.017	.000	.000	.000	.000	.000	+0.001	+0.010	+0.010	+0.010	+0.009
93. Wilmer, Ala.	+0.018	.000	-0.001	-0.001	-0.002	-0.001	-0.002	-0.044	-0.043	-0.043	-0.043
94. Aliceville, Ala.	+0.008	.000	-0.001	-0.001	-0.003	-0.005	-0.007	-0.017	-0.016	-0.015	-0.015
95. New Madrid, Mo.	+0.001	.000	-0.002	-0.001	-0.004	-0.007	-0.011	+0.001	+0.003	+0.004	+0.005
96. Mena, Ark.	+0.015	-0.004	-0.006	-0.012	-0.013	-0.020	-0.017	-0.052	-0.050	-0.051	-0.055
97. Nacodoches, Tex.	+0.008	.000	-0.002	-0.001	-0.004	-0.005	-0.006	-0.012	-0.010	-0.009	-0.011
98. Alpine, Tex.	+0.033	-0.022	-0.025	-0.061	-0.063	-0.098	-0.085	+0.021	+0.024	+0.023	+0.008
99. Farwell, Tex.	+0.011	-0.020	-0.021	-0.055	-0.056	-0.096	-0.094	-0.016	-0.015	-0.015	-0.018
100. Guymon, Okla.	-0.001	-0.014	-0.016	-0.042	-0.046	-0.077	-0.081	-0.017	-0.015	-0.013	-0.013
101. Helenwood, Tenn.	+0.015	-0.007	-0.008	-0.020	-0.020	-0.033	-0.030	+0.040	+0.041	+0.040	+0.037
102. Cloudland, Tenn.	+0.130	-0.019	-0.017	-0.039	-0.033	-0.058	-0.043	+0.004	+0.002	-0.002	-0.011
103. Hughes, Tenn.	+0.073	-0.018	-0.018	-0.038	-0.034	-0.057	-0.044	-0.029	-0.029	-0.033	-0.042
104. Charleston, W. Va.	-0.010	-0.004	-0.005	-0.012	-0.015	-0.027	-0.035	-0.024	-0.023	-0.021	-0.016
105. State College, Pa.	+0.010	-0.005	-0.007	-0.016	-0.018	-0.030	-0.030	-0.021	-0.019	-0.019	-0.021
106. Fort Kent, Me.	+0.001	-0.002	-0.003	-0.006	-0.009	-0.016	-0.017	-0.013	-0.012	-0.010	-0.012
107. Prentiss, Wis.	+0.010	-0.007	-0.008	-0.019	-0.019	-0.032	-0.028	+0.024	+0.025	+0.024	+0.020
108. Fergus Falls, Minn.	+0.001	-0.005	-0.006	-0.014	-0.015	-0.026	-0.029	-0.006	-0.005	-0.005	-0.003
109. Sheridan, Wyo.	-0.031	-0.020	-0.021	-0.063	-0.077	-0.120	-0.118	+0.032	+0.033	+0.041	+0.030
110. Boulder, Mont.	-0.007	-0.031	-0.032	-0.077	-0.074	-0.137	-0.139	-0.015	-0.014	-0.018	-0.013
111. Skykomish, Wash.	-0.047	-0.014	-0.018	-0.038	-0.038	-0.058	-0.047	-0.028	-0.024	-0.028	-0.039
112. Olympia, Wash.	-0.012	.000	.000	-0.002	-0.003	-0.014	-0.025	+0.033	+0.033	+0.034	+0.044
113. Heppner, Oreg.	-0.007	-0.010	-0.010	-0.027	-0.029	-0.050	-0.067	-0.027	-0.027	-0.025	-0.016
114. Truckee, Cal.	+0.057	-0.035	-0.035	-0.085	-0.081	-0.129	-0.100	-0.028	-0.028	-0.032	-0.057
115. Winnemucca, Nev.	-0.004	-0.022	-0.023	-0.062	-0.065	-0.116	-0.128	-0.009	-0.008	-0.006	+0.003
116. Ely, Nev.	+0.020	-0.038	-0.039	-0.094	-0.093	-0.159	-0.150	-0.021	-0.020	-0.022	-0.030
117. Guernsey, Wyo.	-0.016	-0.022	-0.024	-0.062	-0.067	-0.117	-0.127	+0.036	+0.038	+0.041	+0.046
118. Pierre, S. Dak.	-0.013	-0.007	-0.008	-0.021	-0.023	-0.042	-0.048	+0.014	+0.015	+0.016	+0.020
119. Fort Dodge, Iowa	+0.002	-0.004	-0.006	-0.014	-0.015	-0.026	-0.027	+0.015	+0.017	+0.016	+0.016
120. Keithsburg, Ill.	-0.003	-0.004	-0.003	-0.009	-0.008	-0.016	-0.016	-0.008	-0.009	-0.009	-0.008
121. Grand Rapids, Mich.	+0.003	-0.004	-0.004	-0.010	-0.009	-0.018	-0.017	+0.002	+0.002	+0.001	+0.001
122. Angola, Ind.	+0.011	-0.004	-0.005	-0.011	-0.012	-0.019	-0.018	+0.011	+0.012	+0.012	+0.010
123. Albany, N. Y.	-0.006	-0.001	-0.002	-0.008	-0.011	-0.020	-0.025	-0.043	-0.042	-0.040	-0.038
1 4. Port Jervis, N. Y.	+0.033	-0.003	-0.004	-0.011	-0.013	-0.020	-0.019	-0.033	-0.032	-0.031	-0.034
Mean with regard to sign								-0.002	-0.001	-0.001	-0.002
Mean without regard to sign								.020	.019	.020	.020
Mean with regard to sign *								.000	+0.001	+0.001	-0.001
Mean without regard to sign *								.018	.018	.018	.019

* Omitting Seattle stations.

If we ignore the two Seattle stations, which seems to be justifiable on account of their excessively large anomalies (see p. 53), we have means with regard to sign, which are zero or 0.001 dyne, for the four methods of horizontal distribution of the compensation. Also three of the methods have means without regard to sign of 0.018 dyne and one of them a mean of 0.019 dyne. These anomalies show that for the country taken as a whole, no one of the methods has an advantage over the others.

It can be readily understood that for a station on a plateau of considerable horizontal extent the effect of compensation should be the same by the several methods, for the amount of compensation under any portion of the area near the station would be the same for each. If the country has varied topography, then the effect of compensation will be different for the different methods of distribution. For instance, in a valley with mountains on either side the

effect of the compensation will be different if some of the compensation of the mountain masses is extended horizontally under the valley.

The decision as to whether we have local or regional compensation must depend upon whether any one method has a general application to a set of stations which exist under the same or similar conditions. For instance, if mountain stations have smaller anomalies on an average, and if the mean of all these stations with regard to sign should be close to zero when reduced by a given method, then we should be justified in concluding that this method is based upon more nearly correct assumptions than a method which gives larger anomalies and a larger mean with regard to sign.

In order to make the regional method of reduction logical, the compensation of each topographic feature should be computed separately to the limits of the zone having the topographic feature at its center. The method of computation actually adopted may give very erroneous results. For instance, let us assume that the compensation is distributed regionally within zone O, with the station at its center. It may happen that the station is in a broad valley or on a plain with mountains surrounding it at a distance of about 167 kms. None of the compensation under the mountains would be taken into account in making the reductions, and the computed value of gravity would be too great. On the other hand, if the station were in the mountains, with valleys or plains just beyond the limits of zone O, then none of the compensation of the mountains would be distributed to the valleys or plains, and the computed value of gravity at the station would be too small. Therefore, in making the reductions by the regional method the compensation for each topographic feature should be distributed separately before making the computations to obtain its effect. This, of course, would be possible, but it would be such a laborious process that it would not be practicable.

RELATION OF LOCAL-COMPENSATION ANOMALIES AND REGIONAL-COMPENSATION ANOMALIES TO THE TOPOGRAPHY.

The tables given in the following pages contain the anomalies computed by the local and the three regional methods, with the stations arranged according to the same topographic groupings as are shown on pages 63 to 67.

Local and regional anomalies at 18 coast stations arranged in the order of their distances from the 1000-fathom line.

Number and name of station.	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within limit of—			Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within limit of—		
		Zone K	Zone M	Zone O			Zone K	Zone M	Zone O
54. San Francisco, Cal.....	-0.023	-0.023	-0.022	-0.047	25. Hoboken, N. J.....	+0.024	+0.024	+0.025	+0.028
18. Beaufort, N. C.....	-0.021	-0.021	-0.021	-0.033	66. Compton, Cal.....	-0.050	-0.049	-0.048	-0.037
80. Astoria, Oreg.....	-0.013	-0.013	-0.010	-0.021	2. West Palm Beach, Fla.....	+0.018	+0.017	+0.016	+0.016
90. Virginia Beach, Va.....	-0.048	-0.048	-0.048	-0.050	3. Punta Gorda, Fla.....	+0.010	+0.010	+0.010	+0.010
92. Fernandina, Fla.....	+0.010	+0.010	+0.010	+0.009	29. Boston, Mass.....	+0.005	+0.005	+0.006	+0.008
1. Key West, Fla.....	+0.008	+0.008	+0.006	-0.003	30. Cambridge, Mass.....	+0.005	+0.005	+0.006	+0.007
8. Point Isabel, Tex.....	+0.027	+0.027	+0.027	+0.024	17. Charleston, S. C.....	-0.021	-0.021	-0.021	-0.022
5. New Orleans, La.....	-0.013	-0.013	-0.013	-0.013	7. Galveston, Tex.....	-0.009	-0.009	-0.009	-0.009
4. Apalachicola, Fla.....	-0.000	-0.000	-0.000	-0.000					
27. New York, N. Y.....	+0.022	+0.022	+0.023	+0.025	Mean with regard to sign.....	-0.004	-0.004	-0.004	-0.006
					Mean without regard to sign.....	.018	.018	.018	.020

For coast stations the mean anomalies with and without regard to sign are the same for local and for regional compensation through zones K and M. In no case does a regional anomaly with compensation out through zones K and M differ more than 0.003 dyne from a local compensation anomaly. This is as one might expect, for the topography is low and the water within zone M is comparatively shallow, so the distribution of compensation regionally can have little influence on the value of the effect of the compensation.

The anomalies for regional compensation to the outer limit of zone O have decidedly larger negative values than those for local compensation at San Francisco (No. 54), at Beaufort (No. 18),

and at Astoria (No. 80), while at Key West (No. 1) the anomaly changes from $+0.008$ to -0.003 . These decided differences are to be expected for a portion of the compensation under the water, which is of positive sign, is distributed through the zone, and as the vertical component of its attraction is greater for the regional distribution than for the local it increases the computed value of gravity at the station and hence makes the anomaly $g-g_c$ have a smaller positive or a larger negative value.

The anomaly at Compton (No. 66) is changed in the opposite direction. This is due to the distribution of the compensation for the high land, which decreases the computed value of the intensity of gravity at the station.

The mean anomaly with regard to sign for regional compensation to the outer limit of zone O is -0.006 , while the mean for local compensation is -0.004 . The means without regard to sign for these anomalies are, respectively, 0.020 and 0.018 . The differences are small but they do not favor distribution of compensation regionally to the outer limit of zone O.

The reason why the mean with regard to sign is negative for the Hayford anomalies at coast stations is discussed under the heading "Relation between the gravity anomalies and the geologic formation." (See p. 70.)

The following table gives the local and regional anomalies at stations near the coast, the stations being arranged in the order of their distance from the open coast. These distances are given in the table on page 64.

Local and regional anomalies at 25 stations near the coast, arranged in the order of their distances from the open coast.

Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—			Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—		
		Zone K	Zone M	Zone O			Zone K	Zone M	Zone O
31. Calais, Me.....	-0.008	-0.008	-0.007	-0.006	123. Albany, N. Y.....	-0.043	-0.042	-0.040	-0.038
25. Princeton, N. J.....	-0.019	-0.018	-0.017	-0.016	16. McCormick, S. C.....	+0.015	+0.015	+0.016	+0.018
93. Wilmer, Ala.....	-0.044	-0.043	-0.043	-0.043	10. Austin, Tex. (Capitol).....	-0.008	-0.008	-0.007	-0.007
23. Baltimore, Md.....	-0.011	-0.010	-0.009	-0.007	11. Austin, Tex. (University).....	-0.010	-0.010	-0.008	-0.009
28. Worcester, Mass.....	-0.020	-0.019	-0.019	-0.021	19. Charlottesville, Va.....	-0.013	-0.012	-0.012	-0.009
24. Philadelphia, Pa.....	+0.022	+0.023	+0.023	+0.025	32. Ithaca, N. Y.....	-0.023	-0.021	-0.021	-0.020
124. Port Jervis, N. Y.....	-0.033	-0.032	-0.031	-0.034	94. Aliceville, Ala.....	-0.017	-0.016	-0.015	-0.015
81. Sisson, Cal.....	-0.010	-0.006	-0.009	-0.018	62. Kerrville, Tex.....	+0.031	+0.032	+0.032	+0.025
21. Washington, D. C. (Coast & Geodetic Survey Office).....	+0.037	+0.038	+0.039	+0.041	106. Fort Kent, Me.....	-0.013	-0.012	-0.010	-0.012
22. Washington, D. C. (Smithsonian Institution).....	+0.039	+0.040	+0.041	+0.043	6. Rayville, La.....	+0.016	+0.017	+0.017	+0.019
84. Washington, D. C. (Bureau of Standards).....	+0.037	+0.038	+0.039	+0.041	Mean with regard to sign.....	-0.002	-0.001	-0.001	-0.001
91. Durham, N. C.....	+0.036	+0.038	+0.038	+0.038	Mean without regard to sign.....	.022	.021	.021	.022
9. Laredo, Tex.....	-0.020	-0.020	-0.019	-0.020					
65. Yuma, Ariz.....	+0.009	+0.009	+0.011	+0.015					
97. Nacogdoches, Tex.....	-0.011	-0.009	-0.008	-0.010					

There are only three stations at which there are decided differences between the local and regional anomalies in the above table. These are Sisson (No. 81), where the change is 0.008 , Yuma (No. 65), where it is 0.006 , and Kerrville (No. 62), where the change is also 0.006 .

As practically all of the 25 stations under consideration are in topography with little relief, one would expect the anomalies to be little changed by the different methods of making the reductions. The mean anomalies with and without regard to sign have a total range of only 0.001 . These stations, therefore, give no information as to whether one of the methods has any advantage over any other one.

The following table gives the local and regional anomalies at 39 stations in the interior which are not in mountainous regions. The stations are arranged in the order of their elevation above sea level. These elevations are given in the table on page 64.

Local and regional anomalies at 39 stations in the interior, and not in mountainous regions, arranged in the order of elevation.

Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—			Number and name of station.	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—		
		Zone K	Zone M	Zone O			Zone K	Zone M	Zone O
95. New Madrid, Mo.	+0.001	+0.003	+0.004	+0.005	122. Angola, Ind.	+0.011	+0.012	+0.012	+0.010
88. Wilson, N. Y.	— .010	— .008	— .009	— .004	15. Atlanta, Ga.	— .023	— .022	— .021	— .022
13. Little Rock, Ark.	+ .030	+ .032	+ .033	+ .036	119. Fort Dodge, Iowa.	+ .015	+ .017	+ .016	+ .016
87. Potsdam, N. Y.	+ .021	+ .022	+ .023	+ .021	108. Fergus Falls, Minn.	— .006	— .005	— .005	— .003
35. Terre Haute, Ind.	— .009	— .009	— .008	— .006	90. Mena, Ark.	— .052	— .050	— .051	— .055
38. St. Louis, Mo.	— .005	— .004	— .003	— .003	60. Mitchell, S. Dak.	+ .001	+ .002	+ .004	+ .005
120. Keithsburg, Ill.	— .008	— .007	— .007	— .006	58. Ely, Minn.	+ .023	+ .025	+ .026	+ .021
89. Alpena, Mich.	— .020	— .021	— .022	— .020	118. Pierre, S. Dak.	+ .014	+ .015	+ .016	+ .020
36. Chicago, Ill.	— .007	— .008	— .008	— .006	57. Iron River, Mich.	+ .038	+ .039	+ .038	+ .031
104. Charleston, W. Va.	— .024	— .023	— .021	— .016	40. Ellsworth, Kans.	+ .014	+ .015	+ .015	+ .017
14. Columbia, Tenn.	+ .026	+ .026	+ .026	+ .026	107. Prentiss, Wis.	+ .024	+ .025	+ .024	+ .020
33. Cleveland, Ohio.	— .003	— .003	— .003	— .003	76. Bismarck, N. Dak.	+ .002	+ .003	+ .004	+ .005
73. Menison, Tex.	+ .005	+ .005	+ .004	+ .004	61. Sweetwater, Tex.	— .029	— .028	— .028	— .029
121. Grand Rapids, Mich.	+ .002	+ .003	+ .003	+ .003	77. Hinsdale, Mont.	+ .029	+ .031	+ .033	+ .038
12. McAlester, Okla.	— .027	— .026	— .027	— .027	72. Shamrock, Tex.	+ .032	+ .031	+ .032	+ .033
59. Pembina, N. Dak.	+ .019	+ .019	+ .020	+ .021	83. Paxton, Nebr.	— .006	— .004	— .004	— .002
34. Cincinnati, Ohio.	— .019	— .019	— .020	— .020	100. Guymon, Okla.	— .017	— .015	— .013	— .013
74. Minneapolis, Minn.	+ .059	+ .060	+ .060	+ .061	41. Wallace, Kans.	— .012	— .012	— .012	— .011
37. Madison, Wis.	— .005	— .004	— .004	— .006	99. Farwell, Tex.	— .016	— .015	— .015	— .018
39. Kansas City, Mo.	— .016	— .015	— .015	— .015	Mean with regard to sign.	+ .001	+ .002	+ .002	+ .003
					Mean without regard to sign.	.017	.018	.018	.017

The differences between the anomalies for the local and for the regional compensation to the outer limits of zones K and M are very small, there being only two as great as 0.004 and only five others as great as 0.003.

The differences between the anomalies for local compensation and for regional compensation to the outer limit of zone O are only slightly larger, the maximum difference being 0.009.

As with the stations back from the coast, the differences between the local and regional anomalies may be expected to be small, for the topography in the vicinity of these stations is fairly level.

The means without regard to sign for the different methods are practically the same, while the means with regard to sign differ only slightly. It must be considered that there is no evidence here in favor of either method, although the slight differences in the means with regard to sign favor the local distribution.

There are 22 stations in the United States in mountainous regions and below the general level, the anomalies for which by the local and regional methods of distribution of compensation are given in the following table. The elevations of the stations and the distances of the stations below the general elevation are given in the table on page 66.

Local and regional anomalies at 22 stations in mountainous regions and below the general level, arranged in the order of their distances below the general level.

Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—			Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—		
		Zone K	Zone M	Zone O			Zone K	Zone M	Zone O
70. Gallup, N. Mex.	—0.013	—0.013	—0.013	—0.020	49. Salt Lake City, Utah.	+0.010	+0.012	+0.013	+0.016
105. State College, Pa.	— .021	— .019	— .019	— .021	44. Denver, Colo.	— .016	— .014	— .007	+ .001
67. Goldfield, Nev.	— .013	— .013	— .012	— .009	79. Boise, Idaho.	+ .008	+ .010	+ .012	+ .022
85. North Hero, Vt.	+ .001	+ .002	+ .005	+ .005	78. Sandpoint, Idaho.	+ .002	+ .002	+ .006	+ .011
63. El Paso, Tex.	+ .007	+ .008	+ .008	+ .013	69. Grand Canyon, Ariz.	— .010	— .009	— .009	— .019
113. Beppner, Oreg.	— .027	— .027	— .025	— .016	46. Grand Junction, Colo.	+ .024	+ .026	+ .031	+ .038
112. Olympia, Wash.	+ .033	+ .033	+ .034	+ .044	47. Green River, Utah.	— .021	— .018	— .014	— .001
110. Boulder, Mont.	— .015	— .014	— .018	— .013	Mean with regard to sign.	.000	+ .001	+ .003	+ .006
111. Skykomish, Wash.	— .028	— .024	— .028	— .039	Mean without regard to sign.	.017	.017	.018	.019
117. Guernsey, Wyo.	+ .036	+ .038	+ .041	+ .046					
115. Winnemucca, Nev.	— .009	— .008	— .006	+ .003					
109. Sheridan, Wyo.	+ .032	+ .033	+ .041	+ .030					
82. Rock Springs, Wyo.	+ .013	+ .011	+ .013	+ .021					
45. Gunnison, Colo.	+ .020	+ .023	+ .028	+ .018					
42. Colorado Springs, Colo.	— .007	— .007	— .008	— .008					

The anomalies for the regional compensation to the outer limits of zones K and M are only slightly different from the anomalies for local compensation and the means with regard to sign show only a slight advantage for the local compensation method. The means without regard to sign for the three sets of anomalies are practically the same. But for regional compensation to the outer limit of zone O, there are four anomalies which are larger than the maximum anomaly for local compensation, 0.036. While the average anomaly without regard to sign is nearly the same for the two methods, the mean with regard to sign is zero for local compensation and +0.006 for regional compensation to the outer limit of zone O. This, it is believed, is comparatively strong evidence in favor of local distribution of compensation. This is especially true as the mean with regard to sign for 122 stations, regional compensation considered to the outer limit of zone O (see bottom of table on p. 87), is -0.001. The mean in the above table is, therefore, 0.007 different from the mean of all.

As the compensation of the higher land is brought closer to the station it is natural that the computed gravity at the stations should be less than for the local distribution of the compensation.

The last table of this series gives the local and regional anomalies at 18 stations in mountainous regions which are above the general level. The elevations of the stations above sea level and the distances above the general level are given in the table on page 66.

Local and regional anomalies at 18 stations in mountainous regions and above the general level, arranged in the order of their distances above the general level.

Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—			Number and name of station	Hayford anomaly, 1912 (local compensation)	Anomaly with regional compensation within outer limit of—		
		Zone K	Zone M	Zone O			Zone K	Zone M	Zone O
71. Las Vegas, N. Mex.....	+0.003	+0.002	+0.003	-0.007	86. Lake Placid, N. Y.....	+0.006	+0.007	+0.003	-0.007
116. Ely, Nev.....	-.021	-.020	-.022	-.030	103. Hughes, Tenn.....	-.029	-.029	-.033	-.042
101. Helenwood, Tenn.....	+ .040	+ .041	+ .040	+ .037	75. Lead, S. Dak.....	+ .052	+ .053	+ .049	+ .039
52. Lower Geyser Basin, Wyo.	-.001	+ .001	.000	-.009	08. Yavapai, Ariz.....	+ .001	+ .001	+ .001	-.007
51. Norris Geyser Basin, Wyo.	+ .021	+ .023	+ .022	+ .008	114. Truckee, Cal.....	-.028	-.028	-.032	-.057
48. Pleasant Valley Junction, Utah.....	+ .004	+ .005	+ .001	-.008	55. Mount Hamilton, Cal.....	-.003	-.003	-.011	-.018
50. Grand Canyon, Wyo.....	-.002	-.001	-.001	-.017	102. Cloudland, Tenn.....	+ .004	+ .002	-.002	-.011
98. Alpine, Tex.....	+ .021	+ .024	+ .023	+ .008	43. Pikes Peak, Colo.....	+ .021	+ .013	+ .008	+ .004
64. Nogales, Ariz.....	-.050	-.050	-.055	-.057	Mean with regard to sign.....	+ .003	+ .003	.000	-.010
20. Deer Park, Md.....	+ .010	+ .012	+ .007	+ .001	Mean without regard to sign.....	.018	.018	.017	.020

This table gives strong evidence that the local compensation and the regional compensation to the outer limits of zones K and M are much nearer the truth than regional compensation to the outer limit of zone O. There is some slight evidence in favor of regional compensation to the outer limit of zone M.

The mean anomaly without regard to sign for regional compensation to the outer limit of zone O is only 0.002 larger than for the local method, but the mean with regard to sign is -0.010 while for the local method it is only +0.003, and the former is 0.009 different from the mean for 122 stations, -0.001 (see p. 87).

The progressive decrease algebraically in the regional anomalies as the radius of distribution of the compensation is increased is what one would naturally expect, for as the compensation is placed farther and farther from the station it has less effect, and so the computed gravity is increased and the anomalies are decreased algebraically.

CONCLUSION.

The evidence and analysis given on pages 85 to 91 lead to the definite conclusion that the local distribution of compensation is much nearer the truth than the regional distribution of the compensation to a distance of 166.7 km. from the stations. This conclusion is based upon the great difference of 0.016 dyne between the mean zone-O anomaly for stations in moun-

tainous regions below the general level and the mean zone-O anomaly at stations in mountainous regions above the general level. The difference between the mean anomalies for the local method for these two groups of stations is only 0.003.

There is no evidence which favors the local as against the regional distribution out through zones K and M. Whether there is some intermediate zone between 58.8 and 166.7 km. which would give as good results as the local distribution could be determined only by further computations.

The discussions under other headings in this report show that the cause of the anomalies is local to a great extent. We are forced to believe that the anomalies can not be materially reduced by any method of regional distribution of the compensation of general application. This fact is clearly shown in the preceding tables, for only occasionally is a large local-compensation anomaly greatly reduced by a regional method of distributing the compensation. More often the regional distribution increases the anomaly.

As stated on page 88, the method employed for the regional distribution is somewhat illogical in that the compensation for each topographic feature is not distributed separately, but the author believes the above conclusions would not be changed if the ideal method were employed.

Chapter VII. EFFECT OF THE ELEVATION OF THE STATION UPON THE INTENSITY OF GRAVITY.

In computing the correction to the intensity of gravity due to the elevation of a station above sea level the well known formula

$$c = -0.0003086 H$$

was used, c being the correction for height in dynes and H the elevation in meters.

The constant factor of this formula was not questioned during the investigation until it was found that the gravity anomalies were quite different at pairs of stations near each other horizontally, but with a considerable difference in elevation. In the United States there are 3 such pairs of stations and from the report of the International Geodetic Association 9 sets in Europe were selected and the Hayford anomalies were computed for each station involved. Later it was found that there are 2 pairs in India.

There are shown in the following table the data for each of the sets. In two cases there are three stations in a set.

The density is given for information only. Its value is taken from reports of the International Geodetic Association. The corrections for topography and isostatic compensation are all based on the same density, 2.67.

Sets of adjacent stations having great differences of elevation.

Sets of stations	Latitude	Longitude	H	Density	$g - g_0$	Hayford anomaly, 1912
	° ' "	° ' "	Meters.			
1 {Stillferjoch, Austria.....	46 31.8	10 27.4	2760	2.4	-0.010	-0.018
1 {Franzenhöhe, Austria.....	46 32.0	10 29.0	2188	2.4	- .014	- .022
2 {Schneekoppe, Germany.....	50 44.2	15 44.6	1605	2.73	+ .029	+ .021
2 {Alter Bruch, Germany.....	50 45.7	15 44.6	917	2.65	+ .019	+ .011
3 {Brocken, Germany.....	51 48.0	10 37	1140	2.6	+ .053	+ .045
3 {Scharfenstein, Germany.....	51 50.0	10 36.0	623	2.6	+ .052	+ .044
4 {Naye, Switzerland.....	46 26.0	6 58.7	1987	2.7	+ .026	+ .018
4 {Villeneuve, Switzerland.....	46 24.1	6 55.7	376	2.6	+ .019	+ .011
5 {Chamont, Switzerland.....	47 01.4	6 57.1	1018	2.7	+ .044	+ .036
5 {Neuenburg, Switzerland.....	47 00.1	6 57.3	487	2.7	+ .032	+ .024
6 {Gornergrat, Switzerland.....	45 59.0	7 46.8	3016	2.73	+ .053	+ .045
6 {Riffelberg, Switzerland.....	45 59.6	7 45.3	2566	2.74	+ .055	+ .047
6 {Zermatt, Switzerland.....	46 01.5	7 45.0	1603	2.76	+ .044	+ .036
7 {Belalp, Switzerland.....	46 22.9	7 59.6	2132	2.65	+ .010	+ .002
7 {Brig, Switzerland.....	46 19.7	8 00.4	683	2.72	- .004	- .012
8 {Eggishorn, Switzerland.....	46 25.2	8 06.8	2187	2.65	+ .013	+ .006
8 {Flesch, Switzerland.....	46 24.2	8 08.1	1049	2.65	+ .000	- .008
9 {Sanetsch, Switzerland.....	46 19.3	7 17.2	2041	2.70	+ .020	+ .012
9 {Gsteig, Switzerland.....	46 23.2	7 16.2	1185	2.63	+ .021	+ .013
10 {Pikes Peak, Colo.....	38 50.3	105 02.0	4293	2.62	+ .029	+ .021
10 {Colorado Springs, Colo.....	38 50.7	104 49.0	1841	2.4	+ .001	- .007
11 {Yavapai, Ariz.....	36 03.9	112 07.1	2179		+ .009	+ .001
11 {Grand Canyon, Ariz.....	36 05.3	112 06.8	849		- .002	- .010
12 {Cloudland, Tenn.....	36 06.2	82 07.9	1890		+ .012	+ .004
12 {Hughes, Tenn.....	36 08.5	82 07.2	994		- .021	- .029
13 {Mussoorie (Camels Back), India.....	30 27.6	78 04.5	2110	(2.8)	+ .055	+ .047
13 {Rajpur, India.....	30 24.2	78 05.8	1012	2.5	+ .027	+ .019
13 {Dahra Dun, India.....	30 19.5	78 03.2	682	2.45	+ .006	- .002
14 {Yercaud, India.....	11 46.9	78 12.5	1369	2.7	- .031	- .039
14 {Salem, India.....	11 40.1	78 09.2	289	2.6	- .048	- .056

The following table shows the difference in elevation of the stations forming a set and the differences in the anomalies for each set. There are two cases where there are three stations in a set. In one case (set No. 6) the mean of the two high stations was used in getting the differences in elevation and anomaly and in the other case (set No. 13) the mean of the two low stations was used:

Differences of elevations and anomalies for sets of near stations.

Set No.	Difference of elevation high—low	Difference of anomalies high—low	Set No.	Difference of elevation high—low	Difference of anomalies high—low
	<i>Meters.</i>	<i>Dynes.</i>		<i>Meters.</i>	<i>Dynes.</i>
1.....	572	+0.004	9.....	856	-0.001
2.....	688	+ .010	10.....	2452	+ .028
3.....	517	+ .001	11.....	1330	+ .011
4.....	1611	+ .007	12.....	896	+ .033
5.....	531	+ .012	13.....	1263	+ .039
6.....	1188	+ .010	14.....	1080	+ .017
7.....	1449	+ .014			
8.....	1138	+ .013	Total.....	15571	+ .198

It is seen that in only one case is the difference in anomaly negative, and this difference is only 0.001 dyne. On an average a difference in elevation of 100 meters causes a difference in the anomalies of 0.0013 dyne; and a difference of anomaly of 0.0010 dyne is caused by a difference in elevation of 79 meters.

If a change of 0.0000130 in the constant term of the height formula were made, the resulting formula, $c = -0.0002956 H$, would make the total difference in the anomalies with regard to sign equal to zero.

The derivation of the constant term of the formula from the observed value of gravity at 124 stations in the United States made its value 0.0003066, with a probable error of ± 0.0000017 . That the height formula is in error by such an amount as the 0.0000130 indicated by the above data is improbable for two reasons: First, because if the changed height formula were used in computing the correction for elevation for the United States stations, there would be a strong relation between the elevation of the stations and the gravity anomaly. The higher the station the less algebraically would be its anomaly, while with the unchanged formula there is no apparent relation between the anomalies and the elevation. Second, a very careful and thorough investigation was made by W. D. Lambert, of the Survey, which failed to disclose any flaws in the derivation of the constant factor of the formula.

An investigation of the subject along other lines was made, and it was found that there are several causes to which may be due some of the difference in the anomalies at high and low stations which are horizontally close together.

First. In general the higher station of a pair is on a mountain peak which has comparatively steep slopes. The corrections for topography were computed by the zone method, the average elevation in the zone being used in the computations. This has the effect of lessening the effect of the closer part of the topography in the zone, as the leveling method involved in assuming a uniform average level for the whole zone lowers the nearby topography and increases its distance from the station. A test was made of the effect of using narrower zones from the station out to a distance of 2.29 km. The tables for these zones are shown on pages 11 to 18. When the effect of the topography near the high station was computed with the narrower zones for station Pikes Peak, a difference of 0.0033 dyne was found. At station Yavapai, Ariz., the difference was found to be 0.0031. The sign of this difference is such as to bring the two anomalies for a pair of stations nearer together.

Second. It may be assumed that in general the higher station of a pair is on topography of greater density than the lower one. The former is usually on a mountain peak which is composed of well-compacted matter, while the lower station is in a valley or in the foothills, where the material is not so well compacted and has much more porosity than the higher mountain mass. It is sometimes true that the two stations of a pair are on different geologic formations. The higher station in general is on the older formation with a greater density.

If it is assumed that the high station is on topography which has a density 0.10 greater than the assumed normal (2.67) and that the lower station is on material 0.10 less than normal, and that these densities obtain for all the topography above sea level, then the topography for the area near the high station would have a greater effect than that which has been used in this investigation, and, conversely, the topography at the lower station would have a less effect than normal.

This is shown in a clear manner by making the changes in density at Pikes Peak and Colorado Springs. The change in the effect of the topography within a radius of 3.5 km. due to increasing its density 0.10 is +0.0085 dyne, while the change from decreasing the density at Colorado Springs by 0.10 is -0.0057. The sum of the two changes in topographic effect is +0.014. The difference between the anomalies at these two stations is 0.028 dyne. The changes in density in the topography near each of the stations reduced by one-half the difference between the anomalies. The changes at the two stations Cloudland and Hughes would be +0.0054 and -0.0035, respectively, and the difference of the anomalies at the two stations would be reduced from 0.033 to 0.024.

In practically all cases the difference in the existing anomalies at two close stations, as shown in the table on page 93, would be reduced by increasing the density of the topography at the high station and decreasing the density of the topography at the low one. The only exception to this general rule is pair No. 9 in the above table. Here the lower station has the larger anomaly, but the difference between the two anomalies is only 0.001 dyne.

It is scarcely possible to make a correction for erroneous density of topography used in the regular reductions, for even if the density of the surface rocks were known one would not be justified in assuming that the density of the surface obtained to any given depth below the surface.

Third. Another correction could be applied to the combined effect of topography and compensation at a station which would make the difference smaller between the anomalies at a pair of stations close together horizontally but with different elevations. In making the tables for computing the effect of topography and compensation it was assumed that the compensation began at the surface and extended to a depth of 113.7 km. This was done to facilitate the computation, although it does not seem to be a reasonable assumption. It is more probable that the compensation begins at sea level or at some lower depth. If it is assumed that the compensation begins at sea level, then the effect of compensation for the topography near the station above sea level is less than when computed by the usual method.

If the average elevation of the topography in a near zone is 1900 meters (6200 feet), then the change in the effect of the compensation will be one-sixtieth of the effect of the topography in that zone. The approximate general rule is that the effect of compensation of topography near the station will be reduced by an amount equal to the product of the elevation of a zone by the correction for topography for the zone divided by the depth of compensation.

Let us apply this at Pikes Peak. The elevations for zones C, D, E, and F are, respectively, 4300, 4100, 3900, and 3700 meters. The corrections for topography for those zones are, respectively, +0.0165, +0.0325, +0.0545, and +0.0639 dyne. The change in the compensation for the four zones is 0.008, and this is the amount the effect of compensation at Pikes Peak is reduced. There would be a further reduction in the compensation if the test were made for a few zones beyond zone F. The effect of the change at a single station becomes zero in general at about zones J or K. For the outer zones the effect is small for any one station and for a pair of stations the effect on the relative anomaly is negligible.

At Colorado Springs, the lower station of the pair, the average elevation of the topography out to the limits of zone F is about 1800 meters, and the change in the effect of compensation by having it distributed from sea level for zones A to F is 0.002 dyne. The total effect on the difference in the anomalies of changing the position of the upper surface of the compensation at Pikes Peak and Colorado Springs would be about 0.010 dyne. The reduction of the differences at other pairs of stations in this country and abroad would be less than this, in most cases much less.

If the depth of compensation were materially reduced, say, to 60 km., then the effect of starting the distribution of the compensation at the sea level rather than at the surface would be about double what it would be for the depth 113.7 km.

The table on pages 103-105 shows that if the depth of compensation were 127.9 km. the difference in the anomalies at Pikes Peak and Colorado Springs would be reduced to 0.026 dyne, and it would be further reduced to 0.021 dyne if the depth were 184.6 km. If the depth were 42.6 km., the difference in the anomalies at those stations would be increased to 0.051 dyne. For 85.3 km. it would be 0.033 dyne. A change in the depth makes practically no change in the difference between the anomalies at the pair of stations Cloudland and Hughes. The discussion on page 111 indicates that a depth greater than 130 km. is very improbable.

If the compensation has a regional distribution rather than a local distribution, then the anomaly will be reduced at Pikes Peak, it will remain about the same at Colorado Springs, and the difference in the anomalies at the two stations will be considerably reduced. If the distribution of compensation is regional to the outer limit of zone O (167 km.), the difference in the anomalies will be reduced from 0.028 to 0.012 dyne. It would be 0.016 dyne for regional distribution to the outer limit of zone M (59 km.). The regional distribution of the compensation does not materially reduce the difference in anomalies for the pair of stations Cloudland and Hughes and for the pair Yavapai and Grand Canyon. The effect of regional distribution at the pairs of stations not in the United States has not been computed. On page 91 it is shown that the regional distribution of the compensation to a distance of 167 km. is not so probable as the regional distribution to a much shorter distance or as the local distribution of the compensation.

We may conclude that the systematic difference in the anomalies at a pair of stations close together, with one high and one low station, is not due to error in the height formula nor to error in the assumed depth of compensation, but that it is due in part to errors in the assumed densities of the topography under the stations, to deviations from the normal densities in the material below sea level and in the upper crust, to the use of wide zones in computing the effect of the topography, to the probably erroneous assumption that the compensation begins at the surface of the topography, and to the assumption of local distribution of the compensation. That the cause is located in the upper crust rather than in the lower crust is evident from the fact that any deviation from the normal conditions in the lower crust would affect each of the two stations of a pair equally, or very nearly so. It is probable that the effect of any one of these causes varies considerably for the different pairs. It would be impossible to arrive at the true effect of each one of the causes for any pair except the effect of the use of the wide zones. The difference in the anomalies is probably due to the combined effect of all of the causes.

Chapter VIII.—EFFECT ON THE INTENSITY OF GRAVITY OF CHANGES IN THE DEPTH OF COMPENSATION.

On pages 103 to 105 of Special Publication No. 10, "The effect of topography and isostatic compensation on the intensity of gravity," is a discussion of some preliminary tests of the effect of a change in the assumed depth of compensation on the gravity anomalies. The conclusion reached was that the available gravity stations probably would not determine a depth that could compete in accuracy with the depths determined from deflections of the plumb line. The further accumulation of material and the further study of the question have brought about a partial revision of this conclusion.

To study the effect of a change in the depth of compensation it is necessary to have the effects of topography and isostatic compensation for different depths. To make these computations with complete theoretic accuracy would require a great amount of labor, even if there were available complete sets of tables similar to those on pages 30 to 47 of Special Publication No. 10, but computed for depths other than 113.7 km. This labor was greatly lessened by the adoption of the approximations below. The results of the computations are given on pages 100–102.

The effect of topography is not altered by a change of depth, but the compensation, and therefore the resultant, changes with the changing depth. The method of computation consists in multiplying either the compensation or the resultant of the topography and compensation by a factor depending on the depth and on the zone involved.

In the tables on pages 30 to 43 of Special Publication No. 10, the correction for elevation of the station above or below the compartment is, strictly speaking, the correction to the combined effect of topography and compensation, but most of the correction is due to the change in the effect of the topography and the part due to the change in the effect of the compensation is relatively small. The change with changing depth in the part due to compensation will generally be smaller still. Neglecting this—that is, considering the compartment to be on the same level as the station—the formula for the compensation C is

$$C = 2\pi k\delta\{c_2 - c_1 - \sqrt{c_2^2 + t^2} + \sqrt{c_1^2 + t^2}\}$$

in which k is the gravitation constant, c_1 and c_2 are the inner and outerradii of the zone, and t is the depth of compensation. δ is the density of compensation and for land compartments is given by the formula, $\delta = 2.67 \frac{h}{t}$, where h is the mean elevation of the compartment, the density of the topography being assumed as 2.67. If C_o denote the compensation for depth 113.7 and C_d the compensation for any other depth, it is evident that $\frac{C_d}{C_o}$ or $\frac{C_d - C_o}{C_o}$ is independent of h , the elevation of the compartment, and also of the assumed density of the topography, and depends only on the two depths involved. The quantity $\frac{C_d - C_o}{C_o}$ was computed for an arbitrary elevation of compartment but applies equally well to any elevation and was so used. It is the factor which multiplied by C_o will give the correction to be added algebraically to C_o to give C_d , the compensation at the new depth. The values of $\frac{C_d - C_o}{C_o}$ for various depths of compensation are shown in the following tables for zones A to O. In interpolating values of $\frac{C_d - C_o}{C_o}$ for depths near 113.7 km., it should be remembered that $\frac{C_d - C_o}{C_o}$ is zero for this depth.

Factors, $\frac{C_d - C_o}{C_o}$, used in computing compensation for the given depths.

Zone	Factors for depth of compensation of—					
	42.6 km.	56.9 km.	85.3 km.	127.9 km.	156.25 km.	184.6 km.
A.....	+1.67	+1.00	+0.33	—0.11	—0.27	—0.38
B.....	+1.67	+1.00	+ .33	— .11	— .27	— .38
C.....	+1.66	+1.00	+ .33	— .11	— .27	— .38
D.....	+1.65	+1.00	+ .33	— .11	— .27	— .38
E.....	+1.63	+ .98	+ .33	— .11	— .27	— .38
F.....	+1.60	+ .97	+ .33	— .11	— .27	— .38
G.....	+1.55	+ .95	+ .32	— .11	— .26	— .38
H.....	+1.49	+ .92	+ .32	— .11	— .26	— .37
I.....	+1.39	+ .87	+ .31	— .10	— .26	— .37
J.....	+1.24	+ .80	+ .29	— .10	— .25	— .36
K.....	+1.03	+ .70	+ .27	— .10	— .24	— .35
L.....	+ .73	+ .55	+ .23	— .09	— .22	— .32
M.....	+ .22	+ .24	+ .14	— .06	— .17	— .26
N.....	— .23	— .10	— .00	— .02	— .07	— .14
O.....	— .45	— .31	— .11	+ .03	+ .06	+ .05

The factors in this table were also applied to ocean compartments, although the compensation which begins at the bottom of the ocean is never on the same level as the station. The error, however, is not large. For ocean compartments the density is 0.615 times that of a land compartment when the height of the land is equal to the depth of the ocean compartment. The sign of the density is reversed.

For the outer zones, numbers 1 to 18, a correction factor is applied to the resultant effect, R , of the topography and compensation. This resultant is proportional to the elevation of the compartment, or

$$R = ph^*$$

in which h is the elevation of the compartment and p is a factor of proportionality given in the tables in Special Publication No. 10, and there computed by the method of quadratures.† If a subscript zero denote the values of R and p for depth 113.7 km., and the same letters with subscript d the corresponding quantities for another depth, then

$$\frac{R_d - R_o}{R_o} = \frac{p_d - p_o}{p_o}$$

or the correction factor, $\frac{R_d - R_o}{R_o}$, is independent of the height of the compartment, though for convenience in computing a standard height was assumed. The values of this factor for various depths are given in the following table. The factors are to be multiplied by the resultant of the topography and compensation for depth 113.7 km. in the same way as the factors in the preceding table are to be multiplied by the compensation and give the correction to be added algebraically to the resultant for the depth 113.7 km. to obtain the resultant for the particular depth in question.

* The corrections for departures from proportionality and for elevation of station which occur in zones 14–18 are neglected as unimportant.

† The resultant might have been found mathematically by integration, but this was not discovered until Special Publication No. 10 was in press. The formula of integration and the tables for its use (based on zones different from those used by the Coast and Geodetic Survey) are given by G. Cassinis in publication entitled "Sull' Applicazione del Metodo Isostatico alle Riduzione delle Misure di Gravità," Rome, 1911. In computing the density of compensation of his outer zones I to XX, Cassinis neglects the convergence of the verticals bounding the compensation, and his density of compensation should be multiplied by approximately 1.019. Although this error is less than 2 per cent of the compensation, since topography and compensation are large and nearly equal for distant zones, it completely falsifies the resultant for these zones. This error is repeated in the publication by Reina and Cassinis, "Determinazione di Gravità Relativa compiute nel 1912 a Roma, Arcetri, Livorno, Genova, Vienna e Potsdam," Rome, 1913. This error was corrected before use was made in this publication of the computed reductions for topography and isostatic compensation given in the publication just mentioned. (See p. 57.)

In Gerland's "Beiträge zur Geophysik" Band XII, pp. 588–638, there is an extended discussion of formulas by Erich Hübner entitled, "Beitrag zur Theorie der isostatischen Reduktion der Schwerebeschleunigungen." On p. 638 he notes an error of 2 per cent in the tables of Special Publication No. 10, due to neglecting the convergence of the verticals. This error is, however, 2 per cent of the small resultant for any compartment, not 2 per cent of the compensation, and may, therefore, be neglected.

Factors, $\frac{R_d - R_o}{R_o}$, used in computing resultant of topography and compensation for given depths.

Zone	Factors for depth of compensation of—					
	42.6 km.	56.9 km.	85.3 km.	127.9 km.	156.25 km.	184.6 km.
18.....	-.53	-.41	-.17	+0.06	+0.14	+0.19
17.....	-.56	-.42	-.18	+ .07	+ .18	+ .24
16.....	-.57	-.43	-.19	+ .08	+ .21	+ .30
15.....	-.58	-.45	-.21	+ .09	+ .24	+ .36
14.....	-.59	-.46	-.22	+ .10	+ .27	+ .41
13.....	-.61	-.47	-.23	+ .11	+ .30	+ .48
12.....	-.62	-.49	-.24	+ .12	+ .34	+ .54
11.....	-.62	-.49	-.24	+ .12	+ .35	+ .57
10.....	-.62	-.50	-.24	+ .13	+ .36	+ .59
9.....	-.62	-.50	-.24	+ .13	+ .37	+ .62
8.....	-.63	-.50	-.25	+ .13	+ .38	+ .63
7.....	-.63	-.50	-.25	+ .13	+ .38	+ .63
6.....	-.63	-.50	-.25	+ .13	+ .38	+ .63
5.....	-.63	-.50	-.25	+ .13	+ .38	+ .63
4.....	-.63	-.50	-.25	+ .13	+ .38	+ .63
3.....	-.63	-.50	-.25	+ .13	+ .38	+ .63
2.....	-.63	-.50	-.25	+ .13	+ .38	+ .63
1.....	-.63	-.50	-.25	+ .13	+ .38	+ .63

An example of the use of these tables is given below. The quantities in the second and third columns are taken from page 42 and are multiplied by the factors in the tables on page 98 and above and the products are placed in the appropriate column. The total of these products for a given depth is the correction to be applied to the effect of topography and isostatic compensation for depth 113.7 km. in order to obtain the effect for the depth in question.

In the same way the computations for other stations in the United States have been made, and the results to three decimals of dynes are shown on pages 100-102.

Corrections for change of depth, station 195, Lander, Wyo.

[These corrections are in units of the fourth decimal place in dynes and are to be added algebraically to the effects of topography and compensation for the depth 113.7 km. to obtain the effects at other depths.]

Zone	Compensation only 113.7 km.	Resultant, topography and compensation 113.7 km.	Correction for depth—					
			42.6 km.	56.9 km.	85.3 km.	127.9 km.	156.25 km.	184.6 km.
A.....	0		0	0	0	0	0	0
B.....	0		0	0	0	0	0	0
C.....	- 4		- 7	- 4	- 1	0	+ 1	+ 2
D.....	- 6		- 10	- 6	- 2	+ 1	+ 2	+ 3
E.....	- 8		- 13	- 8	- 3	+ 1	+ 2	+ 3
F.....	- 20		- 32	- 19	- 7	+ 2	+ 5	+ 8
G.....	- 24		- 37	- 23	- 8	+ 3	+ 6	+ 9
H.....	- 32		- 48	- 29	- 10	+ 4	+ 8	+ 12
I.....	- 43		- 60	- 37	- 13	+ 4	+ 11	+ 16
J.....	- 66		- 82	- 53	- 19	+ 7	+ 16	+ 24
K.....	-109		-112	- 76	- 29	+ 11	+ 26	+ 38
L.....	-158		-115	- 87	- 36	+ 14	+ 35	+ 51
M.....	-425		- 94	-102	- 60	+ 26	+ 72	+110
N.....	-373		+ 86	+ 37	0	+ 7	+ 26	+ 52
O.....	-341		+153	+106	+ 37	- 10	- 20	- 17
18.....		- 68	+ 36	+ 28	+ 12	- 4	- 10	- 13
17.....		- 68	+ 38	+ 29	+ 12	- 5	- 12	- 16
16.....		- 71	+ 40	+ 31	+ 14	- 6	- 15	- 21
15.....		- 66	+ 38	+ 30	+ 14	- 6	- 16	- 24
14.....		- 61	+ 36	+ 28	+ 13	- 6	- 16	- 25
13.....		- 88	+ 54	+ 41	+ 20	- 10	- 26	- 42
12.....		- 51	+ 32	+ 25	+ 12	- 6	- 17	- 28
11.....		- 37	+ 23	+ 18	+ 9	- 4	- 13	- 21
10.....		- 17	+ 11	+ 8	+ 4	- 2	- 6	- 10
9.....		0	0	0	0	0	0	0
8.....		+ 8	- 5	- 4	- 2	+ 1	+ 3	+ 5
7.....		+ 7	- 4	- 4	- 2	+ 1	+ 3	+ 4
6.....		+ 9	- 6	- 4	- 2	+ 1	+ 3	+ 6
5.....		+ 9	- 6	- 4	- 2	+ 1	+ 3	+ 6
4.....		+ 8	- 5	- 4	- 2	+ 1	+ 3	+ 5
3.....		+ 5	- 3	- 2	- 1	+ 1	+ 2	+ 3
2.....		+ 3	- 2	- 2	- 1	0	+ 1	+ 2
1.....		+ 1	- 1	0	0	0	0	+ 1
Total.....			- 95	- 87	- 53	+ 27	+ 77	+142
Total topography and compensation, 113.7 km.....			-275	-275	-275	-275	-275	-275
Total topography and compensation at given depth.....			-370	-362	-328	-248	-198	-133

The following table gives the effect of topography and compensation for each of the 219 stations in the United States for various depths.

Corrections for topography and isostatic compensation for given depths of compensation.

Number and name of station	Depth, 42.6 km.	Depth, 56.9 km.	Depth, 85.3 km.	Depth, 113.7 km.	Depth, 127.9 km.	Depth, 156.25 km.	Depth, 184.6 km.
1. Key West, Fla.	+0.017	+0.022	+0.029	+0.035	+0.038	+0.043	+0.047
2. West Palm Beach, Fla.	+0.016	+0.019	+0.025	+0.031	+0.033	+0.038	+0.043
3. Punta Gorda, Fla.	+0.008	+0.010	+0.016	+0.020	+0.023	+0.027	+0.031
4. Apalachicola, Fla.	+0.006	+0.008	+0.012	+0.015	+0.017	+0.020	+0.023
5. New Orleans, La.	+0.005	+0.007	+0.010	+0.013	+0.015	+0.017	+0.020
6. Bayville, La.	+0.005	+0.005	+0.006	+0.008	+0.008	+0.010	+0.011
7. Galveston, Tex.	+0.003	+0.004	+0.006	+0.007	+0.008	+0.010	+0.011
8. Point Isabel, Tex.	+0.007	+0.009	+0.013	+0.015	+0.017	+0.019	+0.021
9. Laredo, Tex.	+0.004	+0.005	+0.003	+0.003	+0.003	+0.004	+0.006
10. Austin, Tex. (capitol)	-0.005	-0.005	-0.004	-0.003	-0.002	-0.004	.000
11. Austin, Tex. (university)	-0.003	-0.003	-0.002	-0.001	-0.001	+0.001	+0.002
12. McAlester, Okla.	.000	.000	.000	+0.001	+0.001	+0.002	+0.003
13. Little Rock, Ark.	+0.003	+0.002	+0.001	+0.001	+0.001	+0.002	+0.003
14. Columbia, Tenn.	+0.003	+0.003	+0.004	+0.006	+0.007	+0.009	+0.011
15. Atlanta, Ga.	+0.008	+0.009	+0.012	+0.014	+0.015	+0.018	+0.021
16. McCormick, S. C.	+0.008	+0.008	+0.009	+0.012	+0.014	+0.016	+0.019
17. Charleston, S. C.	+0.006	+0.008	+0.012	+0.016	+0.018	+0.021	+0.024
18. Beaufort, N. C.	+0.015	+0.020	+0.028	+0.036	+0.040	+0.046	+0.051
19. Charlottesville, Va.	-0.002	-0.002	.000	+0.002	+0.004	+0.007	+0.010
20. Deer Park, Md.	+0.021	+0.026	+0.035	+0.041	+0.044	+0.049	+0.054
21. Washington, D. C. (Coast and Geodetic Survey Office)	.000	+0.001	+0.002	+0.004	+0.005	+0.007	+0.010
22. Washington, D. C. (Smithsonian Institution)	-0.001	.000	+0.001	+0.003	+0.005	+0.007	+0.010
23. Baltimore, Md.	+0.001	+0.001	+0.003	+0.006	+0.007	+0.009	+0.012
24. Philadelphia, Pa.	+0.003	+0.004	+0.006	+0.009	+0.011	+0.014	+0.017
25. Princeton, N. J.	+0.007	+0.008	+0.010	+0.013	+0.015	+0.017	+0.021
26. Hoboken, N. J.	+0.001	+0.002	+0.005	+0.008	+0.010	+0.012	+0.016
27. New York, N. Y.	+0.004	+0.005	+0.007	+0.011	+0.012	+0.015	+0.019
28. Worcester, Mass.	+0.007	+0.010	+0.013	+0.018	+0.020	+0.024	+0.028
29. Boston, Mass.	+0.005	+0.007	+0.010	+0.013	+0.015	+0.018	+0.022
30. Cambridge, Mass.	+0.002	+0.003	+0.007	+0.010	+0.012	+0.015	+0.019
31. Calais, Me.	+0.005	+0.006	+0.008	+0.010	+0.012	+0.013	+0.016
32. Ithaca, N. Y.	-0.001	.000	+0.002	+0.005	+0.006	+0.009	+0.012
33. Cleveland, Ohio.	-0.002	-0.002	.000	+0.002	+0.001	+0.002	+0.003
34. Cincinnati, Ohio.	+0.001	.000	+0.001	+0.002	+0.003	+0.005	+0.007
35. Terre Haute, Ind.	.000	.000	.000	+0.001	+0.001	+0.002	+0.003
36. Chicago, Ill.	+0.007	+0.007	+0.006	+0.007	+0.008	+0.009	+0.011
37. Madison, Wis.	+0.001	+0.001	+0.002	+0.003	+0.004	+0.005	+0.007
38. St. Louis, Mo.	+0.002	+0.001	+0.001	+0.001	+0.001	+0.002	+0.002
39. Kansas City, Mo.	.000	-0.001	-0.002	-0.001	-0.001	-0.001	.000
40. Ellsworth, Kans.	-0.003	-0.004	-0.004	-0.004	-0.004	-0.004	-0.003
41. Wallace, Kans.	-0.007	-0.006	-0.003	.000	+0.001	+0.003	+0.006
42. Colorado Springs, Colo.	-0.024	-0.020	-0.014	-0.007	-0.004	+0.002	+0.010
43. Pikes Peak, Colo.	+0.147	+0.159	+0.175	+0.187	+0.192	+0.201	+0.211
44. Denver, Colo.	-0.015	-0.017	-0.018	-0.015	-0.013	-0.009	-0.004
45. Gunnison, Colo.	-0.024	-0.021	-0.012	-0.001	+0.004	+0.013	+0.024
46. Grand Junction, Colo.	-0.050	-0.053	-0.054	-0.051	-0.049	-0.046	-0.040
47. Green River, Utah.	-0.036	-0.040	-0.043	-0.043	-0.043	-0.041	-0.038
48. Pleasant Valley Junction, Utah.	-0.002	+0.004	+0.014	+0.024	+0.028	+0.035	+0.042
49. Salt Lake City, Utah.	-0.044	-0.044	-0.044	-0.041	-0.040	-0.037	-0.032
50. Grand Canyon, Wyo.	+0.009	+0.015	+0.027	+0.038	+0.043	+0.051	+0.060
51. Norris Geyser Basin, Wyo.	+0.005	+0.011	+0.021	+0.031	+0.036	+0.044	+0.052
52. Lower Geyser Basin, Wyo.	+0.004	+0.009	+0.018	+0.028	+0.033	+0.040	+0.049
53. Seattle, Wash. (university)	-0.012	-0.015	-0.019	-0.020	-0.021	-0.021	-0.020
54. San Francisco, Cal.	+0.024	+0.029	+0.038	+0.045	+0.048	+0.053	+0.058
55. Mount Hamilton, Cal.	+0.092	+0.100	+0.112	+0.120	+0.124	+0.130	+0.135
56. Seattle, Wash. (high school)	-0.009	-0.013	-0.017	-0.018	-0.018	-0.018	-0.018
57. Iron River, Mich.	+0.006	+0.008	+0.011	+0.014	+0.016	+0.018	+0.020
58. Ely, Minn.	+0.004	+0.005	+0.007	+0.008	+0.009	+0.010	+0.012
59. Pembina, N. Dak.	-0.006	-0.007	-0.008	-0.009	-0.009	-0.009	-0.009
60. Mitchell, S. Dak.	-0.004	-0.004	-0.005	-0.006	-0.006	-0.006	-0.006
61. Sweetwater, Tex.	+0.003	+0.005	+0.007	+0.009	+0.010	+0.013	+0.015
62. Kerrville, Tex.	+0.003	+0.006	+0.010	+0.013	+0.015	+0.018	+0.021
63. El Paso, Tex.	-0.005	-0.004	-0.002	+0.001	+0.002	+0.005	+0.009
64. Nogales, Ariz.	+0.020	+0.025	+0.032	+0.038	+0.040	+0.044	+0.049
65. Yuma, Ariz.	-0.008	-0.009	-0.010	-0.010	-0.010	-0.009	-0.008
66. Compton, Cal.	-0.005	-0.004	-0.002	.000	+0.002	+0.005	+0.009
67. Goldfield, Nev.	+0.006	+0.012	+0.019	+0.027	+0.031	+0.038	+0.046
68. Yavapai, Ariz.	+0.016	+0.020	+0.027	+0.034	+0.037	+0.042	+0.050
69. Grand Canyon, Ariz.	-0.110	-0.108	-0.102	-0.096	-0.093	-0.088	-0.080
70. Gallup, N. Mex.	-0.006	-0.001	+0.006	+0.014	+0.018	+0.024	+0.032
71. Las Vegas, N. Mex.	-0.004	+0.001	+0.009	+0.017	+0.021	+0.027	+0.035
72. Shamrock, Tex.	+0.003	+0.003	+0.005	+0.007	+0.008	+0.010	+0.012
73. Denison, Tex.	-0.002	-0.002	-0.001	-0.001	.000	+0.001	+0.002
74. Minneapolis, Minn.	-0.004	-0.005	-0.005	-0.005	-0.005	-0.005	-0.004
75. Lead, S. Dak.	+0.025	+0.031	+0.038	+0.044	+0.047	+0.051	+0.055

Corrections for topography and isostatic compensation for given depths of compensation—Continued.

Number and name of station	Depth, 42.6 km.	Depth, 56.9 km.	Depth, 85.3 km.	Depth, 113.7 km.	Depth, 127.9 km.	Depth, 156.25 km.	Depth, 184.6 km.
76. Bismarck, N. Dak.	-0.005	-0.005	-0.006	-0.005	-0.005	-0.005	-0.004
77. Hinsdale, Mont.	-0.012	-0.014	-0.015	-0.017	-0.017	-0.018	-0.017
78. Sandpoint, Idaho.	-0.042	-0.044	-0.045	-0.044	-0.042	-0.042	-0.040
79. Boise, Idaho.	-0.035	-0.038	-0.041	-0.042	-0.042	-0.042	-0.040
80. Astoria, Oreg.	+0.001	+0.002	+0.005	+0.008	+0.008	+0.011	+0.013
81. Sisson, Cal.	-0.015	-0.008	+0.004	+0.015	+0.020	+0.029	+0.038
82. Rock Springs, Wyo.	-0.014	-0.011	-0.007	-0.001	+0.001	+0.006	+0.013
83. Paxton, Neb.	-0.000	-0.001	-0.000	+0.002	+0.002	+0.004	+0.006
84. Washington, D. C. (Bureau of Standards)	+0.008	+0.008	+0.010	+0.012	+0.013	+0.015	+0.018
85. North Hero, Vt.	-0.007	-0.008	-0.009	-0.009	-0.008	-0.007	-0.006
86. Lake Placid, N. Y.	+0.014	+0.019	+0.026	+0.032	+0.034	+0.039	+0.043
87. Potsdam, N. Y.	-0.007	-0.006	-0.005	-0.004	-0.003	-0.001	+0.001
88. Wilson, N. Y.	-0.000	-0.001	-0.002	-0.002	-0.001	-0.001	-0.000
89. Alpena, Mich.	-0.004	-0.003	-0.002	-0.000	-0.000	+0.002	+0.003
90. Virginia Beach, Va.	+0.010	+0.013	+0.019	+0.025	+0.028	+0.032	+0.037
91. Durham, N. C.	+0.009	+0.009	+0.011	+0.014	+0.016	+0.019	+0.022
92. Fernandina, Fla.	+0.007	+0.009	+0.013	+0.017	+0.019	+0.023	+0.026
93. Wilmer, Ala.	+0.011	+0.013	+0.016	+0.018	+0.019	+0.022	+0.025
94. Aliceville, Ala.	+0.006	+0.006	+0.007	+0.008	+0.009	+0.010	+0.012
95. New Madrid, Mo.	+0.003	+0.002	+0.001	+0.001	+0.001	+0.001	+0.002
96. Mens, Ark.	+0.011	+0.012	+0.013	+0.015	+0.015	+0.017	+0.018
97. Nacogdoches, Tex.	+0.007	+0.007	+0.007	+0.008	+0.008	+0.009	+0.010
98. Alpine, Tex.	+0.013	+0.017	+0.025	+0.033	+0.036	+0.042	+0.048
99. Farwell, Tex.	+0.003	+0.005	+0.008	+0.011	+0.013	+0.016	+0.021
100. Guymon, Okla.	-0.003	-0.004	-0.003	-0.001	-0.000	+0.002	+0.005
101. Helenwood, Tenn.	+0.005	+0.007	+0.011	+0.015	+0.017	+0.020	+0.024
102. Cloudland, Tenn.	+0.102	+0.109	+0.121	+0.130	+0.134	+0.141	+0.147
103. Hughes, Tenn.	+0.026	+0.033	+0.044	+0.053	+0.056	+0.063	+0.069
104. Charleston, W. Va.	-0.011	-0.012	-0.011	-0.010	-0.009	-0.007	-0.004
105. State College, Pa.	+0.002	+0.003	+0.006	+0.010	+0.012	+0.015	+0.019
106. Fort Kent, Me.	-0.000	-0.000	-0.000	+0.001	+0.002	+0.003	+0.005
107. Prentice, Wis.	+0.003	+0.005	+0.008	+0.010	+0.011	+0.013	+0.015
108. Fergus Falls, Minn.	+0.002	+0.001	+0.001	+0.001	+0.001	+0.001	+0.002
109. Sheridan, Wyo.	-0.035	-0.036	-0.034	-0.031	-0.029	-0.025	-0.021
110. Boulder, Mont.	-0.022	-0.019	-0.013	-0.007	-0.005	-0.000	+0.006
111. Skykomish, Wash.	-0.063	-0.059	-0.053	-0.047	-0.045	-0.041	-0.037
112. Olympia, Wash.	-0.008	-0.010	-0.012	-0.012	-0.011	-0.011	-0.009
113. Heppner, Oreg.	-0.005	-0.006	-0.007	-0.007	-0.006	-0.005	-0.004
114. Truckee, Cal.	+0.014	+0.025	+0.043	+0.057	+0.064	+0.074	+0.085
115. Winnemucca, Nev.	-0.006	-0.009	-0.007	-0.004	-0.002	+0.002	+0.008
116. Ely, Nev.	-0.007	-0.001	+0.010	+0.020	+0.025	+0.033	+0.041
117. Guernsey, Wyo.	-0.015	-0.017	-0.018	-0.016	-0.015	-0.013	-0.010
118. Pierre, S. Dak.	-0.009	-0.010	-0.012	-0.013	-0.013	-0.014	-0.014
119. Fort Dodge, Iowa	+0.002	+0.002	+0.001	+0.002	+0.002	+0.002	+0.004
120. Keithsburg, Ill.	-0.005	-0.005	-0.003	-0.003	-0.002	-0.002	-0.001
121. Grand Rapids, Mich.	+0.001	+0.001	+0.002	+0.003	+0.004	+0.005	+0.006
122. Angola, Ind.	+0.006	+0.008	+0.010	+0.011	+0.012	+0.014	+0.015
123. Albany, N. Y.	-0.010	-0.010	-0.009	-0.006	-0.004	-0.001	+0.002
124. Port Jervis, N. Y.	-0.008	-0.006	-0.002	+0.003	+0.005	+0.009	+0.013
125. Atlantic City, N. J.	+0.007	+0.010	+0.014	+0.018	+0.021	+0.024	+0.028
126. Bridgehampton, N. Y.	+0.008	+0.011	+0.016	+0.020	+0.022	+0.026	+0.030
127. Chatham, Mass.	+0.010	+0.014	+0.019	+0.024	+0.027	+0.031	+0.036
128. Rockland, Me.	+0.004	+0.006	+0.008	+0.011	+0.012	+0.014	+0.017
129. Lancaster, N. H.	-0.006	-0.003	+0.002	+0.007	+0.009	+0.013	+0.017
130. Whitehall, N. Y.	-0.017	-0.016	-0.015	-0.012	-0.011	-0.008	-0.004
131. Little Falls, N. Y.	-0.014	-0.013	-0.010	-0.007	-0.005	-0.001	+0.003
132. Watertown, N. Y.	-0.002	-0.002	-0.001	+0.001	+0.002	+0.004	+0.005
133. Southport, N. Y.	-0.007	-0.005	-0.000	+0.004	+0.006	+0.010	+0.014
134. Erie, Pa.	-0.002	-0.001	-0.000	+0.001	+0.002	+0.003	+0.005
135. Parkersburg, W. Va.	-0.010	-0.009	-0.008	-0.006	-0.005	-0.003	-0.000
136. Columbus, Ohio	-0.002	-0.002	-0.001	+0.001	+0.002	+0.004	+0.006
137. Indianapolis, Ind.	-0.001	-0.000	+0.002	+0.003	+0.004	+0.006	+0.007
138. Springfield, Ill.	+0.004	+0.004	+0.004	+0.005	+0.005	+0.006	+0.006
139. Lebanon, Mo.	+0.007	+0.008	+0.010	+0.012	+0.012	+0.014	+0.016
140. Joplin, Mo.	-0.002	-0.001	-0.000	+0.001	+0.001	+0.003	+0.004
141. Fort Smith, Ark.	-0.006	-0.007	-0.008	-0.007	-0.007	-0.006	-0.005
142. Texarkana, Ark.	+0.001	+0.001	-0.000	+0.001	+0.001	+0.002	+0.002
143. Hot Springs, Ark.	+0.002	+0.002	+0.003	+0.004	+0.005	+0.006	+0.008
144. Alexandria, La.	+0.005	+0.006	+0.008	+0.009	+0.010	+0.012	+0.013
145. Laurel, Miss.	+0.005	+0.006	+0.009	+0.011	+0.013	+0.015	+0.017
146. Richmond, Va.	+0.004	+0.005	+0.007	+0.010	+0.011	+0.014	+0.017
147. Emporia, Va.	+0.007	+0.009	+0.012	+0.015	+0.017	+0.020	+0.023
148. Greenville, N. C.	+0.006	+0.010	+0.015	+0.019	+0.021	+0.025	+0.029
149. Wilmington, N. C.	+0.010	+0.013	+0.018	+0.023	+0.026	+0.030	+0.035
150. Cheraw, S. C.	+0.006	+0.007	+0.010	+0.013	+0.014	+0.017	+0.021
151. Charlotte, N. C.	+0.006	+0.008	+0.011	+0.015	+0.016	+0.020	+0.024
152. Asheville, N. C.	+0.004	+0.009	+0.018	+0.026	+0.029	+0.035	+0.041
153. Cleveland, Tenn.	-0.006	-0.004	-0.001	+0.002	+0.003	+0.006	+0.009
154. Winston-Salem, N. C.	+0.003	+0.005	+0.009	+0.012	+0.014	+0.018	+0.021
155. Knoxville, Tenn.	-0.007	-0.006	-0.004	-0.001	-0.000	+0.003	+0.006

Corrections for topography and isostatic compensation for given depths of compensation—Continued.

Number and name of station	Depth, 42.6 km.	Depth, 56.9 km.	Depth, 85.3 km.	Depth, 113.7 km.	Depth, 127.9 km.	Depth, 156.26 km.	Depth, 184.6 km.
156. Bristol, Va.	-0.002	+0.001	+0.007	+0.012	+0.014	+0.019	+0.024
157. Homestead, Fla.	+0.013	+0.016	+0.024	+0.029	+0.032	+0.037	+0.042
158. Sebring, Fla.	+0.010	+0.013	+0.018	+0.023	+0.026	+0.030	+0.034
159. Titusville, Fla.	+0.009	+0.012	+0.018	+0.023	+0.026	+0.030	+0.034
160. Leesburg, Fla.	+0.009	+0.012	+0.016	+0.021	+0.023	+0.027	+0.031
161. Cedar Keys, Fla.	+0.006	+0.008	+0.012	+0.016	+0.018	+0.022	+0.026
162. Macon, Ga.	+0.001	+0.002	+0.004	+0.007	+0.008	+0.010	+0.013
163. Albany, Ga.	+0.004	+0.005	+0.008	+0.011	+0.012	+0.015	+0.018
164. Pensacola, Fla.	+0.005	+0.007	+0.010	+0.014	+0.015	+0.018	+0.020
165. Opelika, Ala.	+0.007	+0.009	+0.013	+0.017	+0.018	+0.021	+0.024
166. Huntsville, Ala.	-0.003	-0.002	+0.001	+0.003	+0.005	+0.007	+0.010
167. Arkansas City, Ark.	+0.003	+0.003	+0.004	+0.005	+0.005	+0.006	+0.007
168. Memphis, Tenn.	+0.001	+0.001	+0.002	+0.002	+0.003	+0.003	+0.004
169. Mammoth Spring, Ark.	-0.004	-0.004	-0.003	-0.002	-0.001	0.000	+0.001
170. Hopkinsville, Ky.	+0.003	+0.003	+0.005	+0.006	+0.007	+0.008	+0.010
171. Danville, Ky.	+0.004	+0.005	+0.008	+0.011	+0.012	+0.015	+0.017
172. Clifton Forge, Va.	-0.014	-0.013	-0.007	-0.003	0.000	+0.005	+0.009
173. Greenville, Ala.	+0.009	+0.011	+0.014	+0.016	+0.018	+0.020	+0.022
174. Birmingham, Ala.	+0.003	+0.005	+0.008	+0.011	+0.012	+0.014	+0.017
175. Lexington, Va.	-0.004	-0.003	+0.001	+0.005	+0.007	+0.012	+0.016
176. Prestonsburg, Ky.	-0.010	-0.009	-0.007	-0.004	-0.003	-0.001	+0.002
177. Traverse City, Mich.	+0.001	+0.001	+0.001	+0.002	+0.003	+0.003	+0.004
178. Seney, Mich.	+0.004	+0.004	+0.006	+0.007	+0.007	+0.008	+0.010
179. Oconto, Wis.	0.000	-0.001	-0.001	-0.001	-0.001	0.000	+0.001
180. Grand Rapids, Wis.	+0.002	+0.003	+0.004	+0.005	+0.006	+0.007	+0.009
181. Winona, Minn.	-0.008	-0.008	-0.008	-0.008	-0.008	-0.008	-0.004
182. Baldwin, Wis.	+0.004	+0.005	+0.005	+0.006	+0.006	+0.008	+0.009
183. Cumberland, Wis.	+0.005	+0.005	+0.006	+0.008	+0.008	+0.009	+0.011
184. Cambridge, Minn.	+0.001	+0.001	+0.002	+0.002	+0.002	+0.003	+0.004
185. Brainerd, Minn.	+0.001	+0.001	+0.002	+0.003	+0.003	+0.004	+0.005
186. Aberdeen, S. Dak.	-0.004	-0.004	-0.005	-0.005	-0.005	-0.005	-0.005
187. Faith, S. Dak.	+0.005	+0.005	+0.006	+0.006	+0.006	+0.007	+0.008
188. Marmarth, N. Dak.	-0.005	-0.005	-0.004	-0.002	-0.001	0.000	+0.003
189. Towner, N. Dak.	-0.003	-0.004	-0.004	-0.004	-0.005	-0.004	-0.003
190. Crosby, N. Dak.	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.002
191. Crookston, Minn.	-0.004	-0.005	-0.006	-0.006	-0.007	-0.008	-0.008
192. Poplar, Mont.	-0.006	-0.007	-0.008	-0.009	-0.009	-0.009	-0.009
193. Miles City, Mont.	-0.019	-0.020	-0.021	-0.020	-0.020	-0.020	-0.018
194. Huntley, Mont.	-0.018	-0.020	-0.022	-0.022	-0.022	-0.022	-0.020
195. Lander, Wyo.	-0.037	-0.036	-0.033	-0.028	-0.025	-0.020	-0.013
196. Faribault, Minn.	-0.001	-0.001	0.000	0.000	+0.001	+0.002	+0.003
197. St. James, Minn.	+0.001	+0.001	+0.002	+0.002	+0.002	+0.003	+0.004
198. Edgemont, S. Dak.	-0.013	-0.014	-0.013	-0.012	-0.011	-0.009	-0.006
199. Dawson, Minn.	-0.003	-0.003	-0.003	-0.003	-0.003	-0.003	-0.002
200. Cokato, Minn.	+0.002	+0.002	+0.002	+0.003	+0.003	+0.003	+0.004
201. Wasta, S. Dak.	-0.010	-0.011	-0.013	-0.013	-0.013	-0.012	-0.012
202. Moorcroft, Wyo.	-0.001	-0.000	+0.002	+0.005	+0.006	+0.006	+0.013
203. Duluth, Minn.	-0.011	-0.011	-0.011	-0.010	-0.010	-0.009	-0.008
204. Osage, Iowa	+0.004	+0.004	+0.006	+0.007	+0.007	+0.009	+0.010
205. Randolph, Nebr.	+0.005	+0.005	+0.005	+0.005	+0.006	+0.006	+0.007
206. Valentine, Nebr.	0.000	0.000	+0.002	+0.004	+0.005	+0.006	+0.008
207. Wheeling, W. Va.	-0.009	-0.008	-0.006	-0.003	-0.002	0.000	+0.003
208. Leon, Iowa	+0.005	+0.005	+0.006	+0.007	+0.007	+0.009	+0.010
209. Laurel, Md.	+0.001	+0.002	+0.005	+0.007	+0.009	+0.011	+0.014
210. Harrisburg, Pa.	-0.004	-0.003	0.000	+0.002	+0.004	+0.007	+0.010
211. Pittsburg, Pa.	-0.005	-0.004	-0.002	0.000	+0.002	+0.004	+0.007
212. Rockville, Md.	+0.007	+0.008	+0.011	+0.013	+0.015	+0.017	+0.020
213. Upper Marlboro, Md.	+0.001	+0.002	+0.004	+0.007	+0.009	+0.011	+0.014
214. Fairfax, Va.	+0.006	+0.007	+0.009	+0.011	+0.012	+0.015	+0.018
215. Crisfield, Md.	+0.008	+0.010	+0.014	+0.019	+0.022	+0.026	+0.029
216. Fredericksburg, Va.	-0.001	0.000	+0.002	+0.004	+0.006	+0.008	+0.011
217. Dover, Del.	+0.004	+0.006	+0.009	+0.013	+0.014	+0.017	+0.021
218. North Tamarack, Mich.	+0.018	+0.019	+0.020	+0.020			
219. Hagerstown, Md.	-0.002	0.000	+0.002	+0.006	+0.007	+0.010	+0.014

The above table needs little comment. In general the effect of topography and compensation increases algebraically with an increase in depth. The largest change from depth of 42.6 to 184.6 km. is 0.071 dyne at station 114 (Truckee, Cal.). The next greatest change is 0.064, at station 43 (Pikes Peak, Colo.). There are some other changes of as much as 0.030 dyne. There are a few exceptions to the general rule that the effect of topography and compensation increases algebraically with an increase of depth. At station 56 (Seattle, Wash.) the correction of -0.009 dyne for depth 42.6 km. decreases algebraically to -0.018 dyne for depth 184.6 km. There is no other similar change in the above table greater than 0.005 dyne, except for the other Seattle station, No. 53.

The greatest changes occur at stations near the coast, especially when the deep water is not far distant, and in mountainous regions. Where the topography is comparatively level for some distance around the station, the total range in the values for the various depths is small. At station 40 (Ellsworth, Kans.) it is only 0.001 dyne. At station 191 (Crookston, Minn.) the range is only 0.003 dyne. At station 144 (Alexandria, La.) the range is 0.008 dyne. The average amount of change in the effect of topography and isostatic compensation due to a change in depth from 42.6 km. to 184.6 km. is 0.014 dyne.

GRAVITY ANOMALIES FOR VARIOUS DEPTHS OF COMPENSATION FOR STATIONS IN THE UNITED STATES.

There is given below a table which contains the anomalies of gravity at the 219 stations in the United States for various depths.

Anomalies for various depths of compensation.

Number of station	Depth, 42.6 km.		Depth, 56.9 km.		Depth, 60.0 km.	Depth, 85.3 km.		Depth, 113.7 km.		Depth, 127.9 km.		Depth, 156.25 km.		Depth, 184.6 km.	
	$g-g_0$	$g-g_0$ (g_0+12)	$g-g_0$	$g-g_0$ (g_0+11)	$g-g_0$ (g_0+10)	$g-g_0$	$g-g_0$ (g_0+9)	$g-g_0$	$g-g_0$ (g_0+8)	$g-g_0$	$g-g_0$ (g_0+5)	$g-g_0$	$g-g_0$ (g_0+2)	$g-g_0$	$g-g_0$ (g_0-1)
1.....	+0.031	+0.019	+0.026	+0.015	+0.015	+0.019	+0.010	+0.013	+0.007	+0.010	+0.005	+0.005	+0.003	+0.001	+0.002
2.....	+0.041	+0.029	+0.038	+0.027	+0.027	+0.032	+0.023	+0.026	+0.020	+0.024	+0.019	+0.019	+0.017	+0.014	+0.015
3.....	+0.030	+0.018	+0.028	+0.017	+0.017	+0.022	+0.013	+0.018	+0.012	+0.015	+0.010	+0.011	+0.009	+0.007	+0.009
4.....	+0.017	+0.005	+0.015	+0.004	+0.004	+0.011	+0.002	+0.008	+0.002	+0.006	+0.001	+0.003	+0.001	+0.000	+0.001
5.....	+0.003	-0.009	+0.001	-0.010	-0.010	-0.002	-0.011	-0.005	-0.011	-0.007	-0.012	-0.009	-0.011	-0.012	-0.011
6.....	+0.027	+0.015	+0.027	+0.016	+0.017	+0.026	+0.017	+0.024	+0.018	+0.024	+0.019	+0.022	+0.020	+0.021	+0.022
7.....	+0.043	+0.009	+0.002	-0.009	-0.008	+0.000	-0.009	-0.001	-0.007	-0.002	-0.002	-0.004	-0.006	-0.005	-0.004
8.....	+0.043	+0.031	+0.041	+0.030	+0.030	+0.037	+0.028	+0.035	+0.029	+0.033	+0.028	+0.031	+0.029	+0.029	+0.030
9.....	-0.013	-0.025	-0.012	-0.025	-0.022	-0.012	-0.021	-0.012	-0.018	-0.012	-0.017	-0.013	-0.015	-0.015	-0.014
10.....	+0.002	-0.010	+0.002	-0.009	-0.008	+0.001	-0.008	+0.000	-0.006	-0.001	-0.006	+0.001	-0.001	-0.003	-0.002
11.....	-0.000	-0.012	-0.000	-0.011	-0.010	-0.001	-0.010	-0.002	-0.008	-0.002	-0.007	-0.004	-0.006	-0.005	-0.004
12.....	-0.018	-0.030	-0.018	-0.029	-0.028	-0.018	-0.027	-0.019	-0.025	-0.019	-0.024	-0.020	-0.022	-0.021	-0.020
13.....	+0.036	+0.024	+0.037	+0.026	+0.027	+0.038	+0.029	+0.038	+0.032	+0.038	+0.033	+0.037	+0.035	+0.036	+0.037
14.....	+0.037	+0.025	+0.038	+0.026	+0.028	+0.036	+0.027	+0.034	+0.028	+0.033	+0.028	+0.031	+0.029	+0.029	+0.030
15.....	-0.009	-0.021	-0.010	-0.021	-0.021	-0.013	-0.022	-0.015	-0.021	-0.016	-0.021	-0.019	-0.021	-0.022	-0.021
16.....	+0.027	+0.015	+0.027	+0.016	+0.017	+0.026	+0.017	+0.023	+0.017	+0.021	+0.016	+0.019	+0.017	+0.016	+0.017
17.....	+0.043	+0.015	+0.005	-0.016	-0.016	-0.009	-0.018	-0.013	-0.019	-0.015	-0.020	-0.018	-0.020	-0.021	-0.020
18.....	+0.048	-0.004	+0.003	-0.008	-0.008	-0.005	-0.014	-0.013	-0.019	-0.017	-0.022	-0.023	-0.025	-0.028	-0.027
19.....	-0.001	-0.013	-0.001	-0.012	-0.011	-0.003	-0.012	-0.005	-0.011	-0.007	-0.012	-0.010	-0.012	-0.013	-0.012
20.....	+0.038	+0.026	+0.033	+0.022	+0.022	+0.024	+0.015	+0.018	+0.012	+0.015	+0.010	+0.010	+0.008	+0.005	+0.006
21.....	+0.049	+0.037	+0.048	+0.037	+0.038	+0.047	+0.038	+0.045	+0.039	+0.044	+0.039	+0.042	+0.040	+0.039	+0.040
22.....	+0.051	+0.039	+0.050	+0.039	+0.040	+0.049	+0.040	+0.047	+0.041	+0.045	+0.040	+0.043	+0.041	+0.040	+0.041
23.....	+0.002	-0.010	+0.002	-0.009	-0.008	-0.000	-0.009	-0.003	-0.009	-0.004	-0.009	-0.006	-0.008	-0.009	-0.008
24.....	+0.036	+0.024	+0.035	+0.024	+0.025	+0.033	+0.024	+0.030	+0.024	+0.028	+0.023	+0.025	+0.023	+0.022	+0.023
25.....	-0.005	-0.017	-0.006	-0.017	-0.016	-0.008	-0.017	-0.011	-0.017	-0.013	-0.018	-0.015	-0.017	-0.019	-0.018
26.....	+0.039	+0.027	+0.038	+0.027	+0.027	+0.035	+0.026	+0.032	+0.026	+0.030	+0.025	+0.028	+0.026	+0.024	+0.025
27.....	+0.037	+0.025	+0.036	+0.025	+0.025	+0.034	+0.025	+0.030	+0.024	+0.029	+0.024	+0.026	+0.024	+0.022	+0.023
28.....	-0.001	-0.013	-0.004	-0.015	-0.015	-0.007	-0.016	-0.012	-0.018	-0.014	-0.019	-0.018	-0.020	-0.022	-0.021
29.....	+0.021	+0.009	+0.019	+0.008	+0.008	+0.016	+0.007	+0.013	+0.007	+0.011	+0.006	+0.008	+0.006	+0.004	+0.005
30.....	+0.021	+0.009	+0.020	+0.009	+0.009	+0.016	+0.007	+0.013	+0.007	+0.011	+0.006	+0.008	+0.006	+0.004	+0.005
31.....	+0.005	-0.007	+0.004	-0.007	-0.007	+0.002	-0.007	-0.000	-0.006	-0.002	-0.007	-0.003	-0.005	-0.006	-0.005
32.....	-0.009	-0.021	-0.010	-0.021	-0.020	-0.012	-0.021	-0.015	-0.021	-0.016	-0.021	-0.019	-0.021	-0.022	-0.021
33.....	+0.007	-0.005	+0.007	-0.004	-0.003	+0.007	+0.002	+0.005	-0.001	+0.004	-0.001	+0.003	+0.001	+0.002	+0.003
34.....	-0.010	-0.022	-0.009	-0.020	-0.019	-0.010	-0.019	-0.011	-0.017	-0.012	-0.017	-0.014	-0.016	-0.016	-0.015
35.....	-0.000	-0.012	-0.000	-0.011	-0.010	-0.000	-0.009	-0.001	-0.007	-0.001	-0.006	-0.002	-0.004	-0.003	-0.002
36.....	+0.001	-0.011	+0.001	-0.010	-0.009	+0.002	-0.007	+0.001	-0.005	-0.000	-0.005	-0.001	-0.003	-0.003	-0.002
37.....	+0.005	-0.007	+0.005	-0.006	-0.005	+0.004	-0.005	+0.003	-0.003	+0.002	-0.003	+0.001	-0.001	-0.001	-0.000
38.....	+0.002	-0.010	+0.003	-0.008	-0.007	+0.003	-0.006	+0.003	-0.003	+0.003	-0.002	+0.002	-0.000	+0.002	+0.003
39.....	-0.009	-0.021	-0.008	-0.019	-0.018	-0.007	-0.016	-0.008	-0.014	-0.008	-0.013	-0.008	-0.010	-0.009	-0.008
40.....	+0.021	+0.009	+0.022	+0.011	+0.012	+0.022	+0.013	+0.022	+0.016	+0.022	+0.017	+0.022	+0.020	+0.021	+0.022
41.....	+0.003	-0.009	+0.002	-0.009	-0.009	-0.001	-0.010	-0.004	-0.010	-0.005	-0.010	-0.007	-0.009	-0.010	-0.009
42.....	+0.018	+0.006	+0.014	+0.003	+0.003	+0.008	-0.001	+0.001	-0.005	-0.002	-0.007	-0.008	-0.010	-0.016	-0.015
43.....	+0.069	+0.057	+0.057	+0.046	+0.045	+0.041	+0.032	+0.029	+0.023	+0.024	+0.019	+0.015	+0.013	+0.015	+0.006
44.....	-0.008	-0.020	-0.006	-0.017	-0.016	-0.005	-0.014	-0.008	-0.014	-0.010	-0.015	-0.014	-0.016	-0.019	-0.018
45.....	+0.051	+0.039	+0.048	+0.037	+0.037	+0.039	+0.030	+0.028	+0.022	+0.023	+0.018	+0.014	+0.012	+0.003	+0.004
46.....	+0.031	+0.019	+0.034	+0.023	+0.024	+0.035	+0.026	+0.032	+0.026	+0.030	+0.025	+0.027	+0.025	+0.021	+0.022
47.....	-0.020	-0.032	-0.016	-0.027	-0.026	-0.013	-0.022	-0.013	-0.019	-0.013	-0.018	-0.015	-0.017	-0.018	-0.017
48.....	+0.038	+0.026	+0.032	+0.021	+0.021	+0.022	+0.013	+0.012	+0.006	+0.008	+0.003	+0.001	-0.001	-0.006	-0.005
49.....	+0.021	+0.009	+0.021	+0.010	+0.011	+0.021	+0.012	+0.018	+0.012	+0.017	+0.012	+0.014	+0.012	+0.009	+0.010
50.....	+0.035	+0.023	+0.029	+0.018	+0.017	+0.017	+0.008	+0.006	-0.000	+0.001	-0.004	-0.007	-0.009	-0.016	-0.015
51.....	+0.055	+0.043	+0.049	+0.038	+0.038	+0.039	+0.030	+0.029	+0.023	+0.024	+0.019	+0.016	+0.014	+0.008	+0.009
52.....	+0.031	+0.019	+0.026	+0.015	+0.015	+0.008	+0.007	+0.001	-0.002	+0.002	-0.003	-0.005	-0.007	-0.014	-0.013
53.....	-0.093	-0.105	-0.090	-0.101	-0.100	-0.086	-0.095	-0.085	-0.091	-0.084	-0.089	-0.084	-0.086	-0.085	-0.084
54.....	+0.006	-0.006	+0.001	-0.010	-0.010	-0.008	-0.017	-0.015	-0.021	-0.018	-0.023	-0.023	-0.025	-0.028	-0.027
55.....	+0.033	+0.021	+0.025	+0.014	+0.013	+0.013	+0.004	+0.005	-0.001	+0.001	-0.004	-0.005	-0.007	-0.010	-0.009
56.....	-0.094	-0.106	-0.090	-0.101	-0.100	-0.086	-0.095	-0.085	-0.091	-0.085	-0.090	-0.085	-0.087	-0.085	-0.084
57.....	+0.054	+0.042	+0.052	+0.041	+0.041	+0.049	+0.040	+0.046	+0.040	+0.044	+0.039	+0.042	+0.040	+0.040	+0.041
58.....	+0.035	+0.023	+0.034	+0.023	+0.023	+0.032	+0.023	+0.031	+0.025	+0.030	+0.025	+0.029	+0.027	+0.027	+0.028
59.....	+0.024	+0.012	+0.025	+0.014	+0.015	+0.026	+0.017	+0.027	+0.021	+0.027	+0.022	+0.027	+0.025	+0.027	+0.028
60.....	+0.007	-0.005	+0.007	-0.004	-0.003	+0.008	-0.001	+0.009	+0.003	+0.009	+0.004	+0.009	+0.007	+0.009	+0.010

Anomalies for various depths of compensation—Continued.

Number of station	Depth, 42.6 km.		Depth, 56.9 km.		Depth, 60.0 km.	Depth, 85.3 km.		Depth, 113.7 km.		Depth, 127.9 km.		Depth, 156.25 km.		Depth, 184.6 km.	
	$\sigma-\sigma_0$	$\sigma-(\sigma_0+12)$	$\sigma-\sigma_0$	$\sigma-(\sigma_0+11)$	$\sigma-(\sigma_0+10)$	$\sigma-\sigma_0$	$\sigma-(\sigma_0+9)$	$\sigma-\sigma_0$	$\sigma-(\sigma_0+6)$	$\sigma-\sigma_0$	$\sigma-(\sigma_0+5)$	$\sigma-\sigma_0$	$\sigma-(\sigma_0+2)$	$\sigma-\sigma_0$	$\sigma-(\sigma_0-1)$
61.....	-0.015	-0.027	-0.017	-0.028	-0.028	-0.019	-0.028	-0.021	-0.027	-0.022	-0.027	-0.025	-0.027	-0.027	-0.026
62.....	+0.049	+0.037	+0.046	+0.035	+0.035	+0.042	+0.033	+0.039	+0.033	+0.037	+0.032	+0.034	+0.032	+0.031	+0.032
63.....	+0.021	+0.009	+0.020	+0.009	+0.010	+0.018	+0.009	+0.015	+0.009	+0.014	+0.009	+0.011	+0.009	+0.007	+0.008
64.....	-0.024	-0.036	-0.029	-0.040	-0.040	-0.036	-0.045	-0.042	-0.048	-0.044	-0.049	-0.048	-0.050	-0.053	-0.052
65.....	+0.015	+0.003	+0.016	+0.005	+0.006	+0.017	+0.008	+0.017	+0.011	+0.017	+0.012	+0.016	+0.014	+0.015	+0.016
66.....	-0.037	-0.049	-0.038	-0.049	-0.049	-0.040	-0.049	-0.042	-0.048	-0.044	-0.049	-0.047	-0.049	-0.051	-0.050
67.....	+0.016	+0.004	+0.010	-0.001	-0.001	+0.003	+0.003	-0.005	-0.011	-0.009	-0.014	-0.016	-0.018	-0.024	-0.023
68.....	+0.027	+0.015	+0.023	+0.012	+0.012	+0.016	+0.007	+0.009	+0.003	+0.006	+0.001	+0.001	-0.001	-0.007	-0.006
69.....	+0.012	+0.000	+0.010	-0.001	-0.001	+0.004	-0.005	-0.002	-0.008	-0.005	-0.010	-0.010	-0.012	-0.018	-0.017
70.....	+0.015	+0.003	+0.010	-0.001	-0.001	+0.003	-0.006	-0.005	-0.011	-0.009	-0.014	-0.015	-0.017	-0.023	-0.022
71.....	+0.032	+0.020	+0.027	+0.016	+0.016	+0.019	+0.010	+0.011	+0.005	+0.007	+0.002	+0.001	-0.001	-0.007	-0.006
72.....	+0.044	+0.032	+0.044	+0.033	+0.034	+0.042	+0.033	+0.040	+0.034	+0.039	+0.034	+0.038	+0.036	+0.035	+0.036
73.....	+0.014	+0.002	+0.014	+0.003	+0.004	+0.013	+0.004	+0.013	+0.007	+0.012	+0.007	+0.011	+0.009	+0.010	+0.011
74.....	+0.066	+0.054	+0.067	+0.056	+0.057	+0.067	+0.058	+0.067	+0.061	+0.067	+0.062	+0.067	+0.065	+0.066	+0.067
75.....	+0.079	+0.067	+0.073	+0.062	+0.062	+0.066	+0.057	+0.060	+0.054	+0.057	+0.052	+0.053	+0.051	+0.049	+0.050
76.....	+0.010	-0.002	+0.010	-0.001	-0.000	+0.011	+0.002	+0.010	+0.004	+0.010	+0.005	+0.010	+0.008	+0.009	+0.010
77.....	+0.032	+0.020	+0.034	+0.023	+0.023	+0.035	+0.026	+0.031	+0.031	+0.037	+0.032	+0.038	+0.036	+0.037	+0.038
78.....	+0.008	-0.004	+0.010	-0.001	-0.000	+0.011	+0.002	+0.010	+0.004	+0.010	+0.005	+0.008	+0.006	+0.006	+0.007
79.....	+0.009	-0.003	+0.012	+0.001	+0.002	+0.015	+0.006	+0.016	+0.010	+0.016	+0.011	+0.016	+0.014	+0.014	+0.015
80.....	+0.002	-0.010	+0.001	-0.010	-0.010	-0.002	-0.011	-0.005	-0.011	-0.005	-0.010	-0.008	-0.010	-0.010	-0.009
81.....	+0.028	+0.016	+0.021	+0.010	+0.009	+0.009	-0.000	-0.002	-0.008	-0.007	-0.012	-0.016	-0.018	-0.025	-0.024
82.....	+0.034	+0.022	+0.031	+0.020	+0.020	+0.027	+0.018	+0.015	+0.019	+0.014	+0.014	+0.014	+0.012	+0.007	+0.008
83.....	+0.004	-0.008	+0.005	-0.006	-0.005	+0.004	-0.005	+0.002	-0.004	+0.002	-0.003	-0.000	-0.002	-0.002	-0.001
84.....	+0.049	+0.037	+0.049	+0.038	+0.039	+0.047	+0.038	+0.045	+0.039	+0.044	+0.039	+0.042	+0.040	+0.039	+0.040
85.....	+0.007	-0.005	+0.008	-0.003	-0.002	+0.009	-0.000	+0.009	+0.003	+0.008	+0.003	+0.007	+0.005	+0.005	+0.006
86.....	+0.032	+0.020	+0.027	+0.016	+0.016	+0.020	+0.011	+0.014	+0.008	+0.012	+0.007	+0.007	+0.005	+0.003	+0.004
87.....	+0.032	+0.020	+0.031	+0.020	+0.021	+0.030	+0.021	+0.029	+0.023	+0.028	+0.023	+0.026	+0.024	+0.024	+0.025
88.....	-0.004	-0.016	-0.003	-0.014	-0.013	-0.002	-0.011	-0.002	-0.008	-0.003	-0.008	-0.003	-0.005	-0.004	-0.003
89.....	-0.008	-0.020	-0.009	-0.020	-0.019	-0.010	-0.019	-0.012	-0.018	-0.012	-0.017	-0.014	-0.016	-0.015	-0.014
90.....	-0.025	-0.037	-0.028	-0.039	-0.039	-0.034	-0.043	-0.040	-0.046	-0.043	-0.048	-0.047	-0.049	-0.052	-0.051
91.....	+0.049	+0.037	+0.049	+0.038	+0.038	+0.047	+0.038	+0.044	+0.038	+0.042	+0.037	+0.039	+0.037	+0.036	+0.037
92.....	+0.028	+0.016	+0.026	+0.015	+0.015	+0.022	+0.013	+0.018	+0.012	+0.016	+0.011	+0.012	+0.010	+0.009	+0.010
93.....	-0.029	-0.041	-0.031	-0.042	-0.042	-0.034	-0.043	-0.036	-0.042	-0.037	-0.042	-0.040	-0.042	-0.043	-0.042
94.....	-0.007	-0.019	-0.007	-0.018	-0.017	-0.008	-0.017	-0.009	-0.015	-0.010	-0.015	-0.011	-0.013	-0.013	-0.012
95.....	+0.007	-0.005	+0.008	-0.003	-0.002	+0.009	-0.000	+0.009	+0.003	+0.009	+0.004	+0.009	+0.007	+0.008	+0.009
96.....	-0.040	-0.052	-0.041	-0.052	-0.051	-0.042	-0.051	-0.044	-0.050	-0.044	-0.049	-0.046	-0.048	-0.047	-0.046
97.....	-0.003	-0.015	-0.003	-0.014	-0.013	-0.003	-0.012	-0.004	-0.010	-0.004	-0.009	-0.005	-0.007	-0.006	-0.005
98.....	+0.049	+0.037	+0.045	+0.034	+0.034	+0.037	+0.028	+0.029	+0.023	+0.026	+0.021	+0.020	+0.018	+0.014	+0.015
99.....	-0.000	-0.012	-0.002	-0.013	-0.013	-0.005	-0.014	-0.008	-0.014	-0.010	-0.015	-0.013	-0.015	-0.018	-0.017
100.....	-0.007	-0.019	-0.006	-0.017	-0.016	-0.007	-0.016	-0.009	-0.015	-0.010	-0.015	-0.012	-0.014	-0.015	-0.014
101.....	+0.058	+0.046	+0.056	+0.045	+0.045	+0.052	+0.043	+0.048	+0.042	+0.046	+0.041	+0.043	+0.041	+0.039	+0.040
102.....	+0.040	+0.028	+0.033	+0.022	+0.021	+0.021	+0.012	+0.012	+0.006	+0.008	+0.003	+0.001	-0.001	-0.005	-0.004
103.....	+0.006	-0.006	-0.001	-0.012	-0.012	-0.012	-0.021	-0.021	-0.027	-0.024	-0.029	-0.031	-0.033	-0.037	-0.036
104.....	-0.015	-0.027	-0.014	-0.025	-0.024	-0.015	-0.024	-0.016	-0.022	-0.017	-0.022	-0.019	-0.021	-0.022	-0.021
105.....	-0.005	-0.017	-0.006	-0.017	-0.017	-0.009	-0.018	-0.013	-0.019	-0.015	-0.020	-0.018	-0.020	-0.022	-0.021
106.....	-0.004	-0.016	-0.004	-0.015	-0.014	-0.004	-0.013	-0.005	-0.011	-0.006	-0.011	-0.007	-0.009	-0.009	-0.008
107.....	+0.039	+0.027	+0.037	+0.026	+0.026	+0.034	+0.025	+0.032	+0.026	+0.031	+0.026	+0.029	+0.027	+0.027	+0.028
108.....	+0.001	-0.011	+0.002	-0.009	-0.008	+0.002	-0.007	+0.002	-0.004	+0.002	-0.003	+0.002	-0.000	+0.001	+0.002
109.....	+0.044	+0.032	+0.045	+0.034	+0.035	+0.043	+0.034	+0.040	+0.034	+0.038	+0.033	+0.034	+0.032	+0.030	+0.031
110.....	+0.008	-0.004	+0.005	-0.006	-0.006	-0.001	-0.010	-0.007	-0.013	-0.009	-0.014	-0.014	-0.016	-0.020	-0.019
111.....	-0.004	-0.016	-0.008	-0.019	-0.019	-0.014	-0.023	-0.020	-0.026	-0.022	-0.027	-0.026	-0.028	-0.030	-0.029
112.....	+0.037	+0.025	+0.039	+0.028	+0.029	+0.041	+0.032	+0.041	+0.035	+0.040	+0.035	+0.040	+0.038	+0.038	+0.039
113.....	-0.021	-0.033	-0.020	-0.031	-0.030	-0.019	-0.028	-0.019	-0.025	-0.020	-0.025	-0.021	-0.023	-0.022	-0.021
114.....	+0.023	+0.011	+0.012	+0.001	-0.000	-0.006	-0.015	-0.020	-0.026	-0.027	-0.032	-0.037	-0.039	-0.048	-0.047
115.....	+0.003	-0.009	+0.004	-0.007	-0.006	+0.002	-0.007	-0.001	-0.007	-0.003	-0.008	-0.007	-0.009	-0.013	-0.012
116.....	+0.014	+0.002	+0.008	-0.003	-0.003	-0.003	-0.012	-0.013	-0.019	-0.018	-0.023	-0.026	-0.028	-0.034	-0.033
117.....	+0.043	+0.031	+0.045	+0.034	+0.035	+0.046	+0.037	+0.044	+0.038	+0.043	+0.038	+0.041	+0.039	+0.038	+0.039
118.....	+0.018	+0.006	+0.019	+0.008	+0.009	+0.021	+0.012	+0.022	+0.016	+0.022	+0.017	+0.023	+0.021	+0.023	+0.024
119.....	+0.023	+0.011	+0.023	+0.012	+0.013	+0.024	+0.015	+0.023	+0.017	+0.023	+0.018	+0.023	+0.021	+0.021	+0.022
120.....	+0.002	-0.010	+0.002	-0.009	-0.008	-0.000	-0.009	-0.000	-0.006	-0.001	-0.006	-0.001	-0.003	-0.002	-0.001
121.....	+0.012	+0.000	+0.012	+0.001	+0.002	+0.011	+0.002	+0.010	+0.004	+0.009	+0.004	+0.008	+0.006	+0.007	+0.008
122.....	+0.022	+0.010	+0.022	+0.011	+0.012	+0.020	+0.011	+0.019	+0.013	+0.018	+0.013	+0.016	+0.014	+0.015	+0.016
123.....	-0.031	-0.043	-0.031	-0.042	-0.041	-0.032	-0.041	-0.035	-0.041	-0.037	-0.042	-0.040	-0.042	-0.043	-0.042
124.....	-0.014	-0.026	-0.016	-0.027	-0.027	-0.020	-0.029	-0.025	-0.031	-0.027	-0.032	-0.031	-0.033	-0.035	-0.034
125.....	-0.004	-0.016	-0.007	-0.018	-0.018	-0.011	-0.020	-0.015	-0.021	-0.018	-0.023	-0.021	-0.023	-0.025	-0.024
126.....	-0.002	-0.014	-0.005	-0.016	-0.016	-0.010	-0.019	-0.014	-0.020	-0.016	-0.021	-0.020	-0.022	-0.024	-0.023
127.....	+0.008	-0.004	+0.004	-0.007	-0.007	-0.001	-0.010	-0.006	-0.012	-0.009	-0.014	-0.013	-0.015	-0.018	-0.017
128.....	-0.000	-0.012	-0.002	-0.013	-0.013	-0.004	-0.013	-0.007	-0.013	-0.008	-0.013	-0.010	-0.012	-0.013	-0.012
129.....	+0.003	-0.009	-0.000	-0.011	-0.011	-0.005	-0.014	-0.010	-0.016	-0.012	-0.017	-0.016	-0.018	-0.020	-0.019
130.....	-0.026	-0.038	-0.027	-0.038	-0.037	-0.028	-0.037	-0.031	-0.037	-0.032	-0.037	-0.035	-0.037	-0.039	-0.038
131.....	-0.009	-0.021	-0.010	-0.021	-0.021	-0.013	-0.022	-0.016	-0.022	-0.018	-0.023	-0.022	-0.024	-0.026	-0.025
132.....	-0.014	-0.026	-0.014	-0.025	-0.024	-0.015	-0.024	-0.017							

Anomalies for various depths of compensation—Continued.

Number of station	Depth, 42.6 km.		Depth, 56.9 km.		Depth, 60.0 km.	Depth, 85.3 km.		Depth, 113.7 km.		Depth, 127.9 km.	Depth, 156.25 km.		Depth, 184.6 km.	
	$\sigma - \sigma_0$	$\sigma - \sigma_0$ ($\sigma_0 + 12$)	$\sigma - \sigma_0$	$\sigma - \sigma_0$ ($\sigma_0 + 11$)	$\sigma - \sigma_0$ ($\sigma_0 + 10$)	$\sigma - \sigma_0$	$\sigma - \sigma_0$ ($\sigma_0 + 9$)	$\sigma - \sigma_0$	$\sigma - \sigma_0$ ($\sigma_0 + 6$)	$\sigma - \sigma_0$ ($\sigma_0 + 5$)	$\sigma - \sigma_0$	$\sigma - \sigma_0$ ($\sigma_0 + 2$)	$\sigma - \sigma_0$	$\sigma - \sigma_0$ ($\sigma_0 - 1$)
141	-0.009	-0.021	-0.008	-0.019	-0.018	-0.007	-0.016	-0.008	-0.014	-0.008	-0.013	-0.009	-0.011	-0.010
142	+0.019	+0.007	+0.019	+0.008	+0.009	+0.020	+0.011	+0.019	+0.013	+0.019	+0.014	+0.018	+0.016	+0.018
143	+0.028	+0.016	+0.028	+0.017	+0.018	+0.027	+0.018	+0.026	+0.020	+0.025	+0.020	+0.024	+0.022	+0.022
144	+0.006	+0.006	+0.005	+0.006	+0.005	+0.003	+0.006	+0.002	+0.004	+0.001	+0.004	+0.001	+0.003	+0.002
145	+0.028	+0.016	+0.027	+0.016	+0.016	+0.024	+0.015	+0.022	+0.016	+0.020	+0.015	+0.018	+0.016	+0.017
146	+0.017	+0.005	+0.016	+0.005	+0.005	+0.014	+0.005	+0.011	+0.005	+0.010	+0.005	+0.007	+0.005	+0.004
147	+0.029	+0.017	+0.027	+0.016	+0.016	+0.024	+0.015	+0.021	+0.015	+0.019	+0.014	+0.016	+0.014	+0.013
148	+0.001	+0.011	+0.001	+0.012	+0.006	+0.012	+0.015	+0.010	+0.016	+0.012	+0.017	+0.016	+0.018	+0.020
149	+0.010	+0.022	+0.013	+0.024	+0.024	+0.018	+0.027	+0.023	+0.029	+0.026	+0.031	+0.030	+0.032	+0.035
150	+0.017	+0.005	+0.016	+0.005	+0.005	+0.013	+0.004	+0.010	+0.004	+0.009	+0.004	+0.006	+0.004	+0.002
151	+0.042	+0.030	+0.040	+0.029	+0.029	+0.037	+0.028	+0.033	+0.027	+0.032	+0.027	+0.028	+0.026	+0.024
152	+0.025	+0.013	+0.020	+0.009	+0.009	+0.011	+0.002	+0.003	+0.003	+0.000	+0.005	+0.006	+0.008	+0.012
153	+0.007	+0.019	+0.009	+0.020	+0.020	+0.012	+0.021	+0.015	+0.021	+0.016	+0.021	+0.019	+0.021	+0.022
154	+0.021	+0.033	+0.023	+0.034	+0.034	+0.027	+0.036	+0.030	+0.036	+0.032	+0.037	+0.036	+0.038	+0.039
155	+0.007	+0.019	+0.008	+0.019	+0.019	+0.010	+0.019	+0.013	+0.019	+0.014	+0.019	+0.017	+0.019	+0.019
156	+0.007	+0.005	+0.004	+0.007	+0.007	+0.002	+0.011	+0.007	+0.013	+0.009	+0.014	+0.014	+0.016	+0.019
157	+0.012	+0.024	+0.015	+0.026	+0.026	+0.023	+0.032	+0.028	+0.034	+0.031	+0.036	+0.036	+0.038	+0.041
158	+0.004	+0.008	+0.001	+0.010	+0.010	+0.004	+0.013	+0.009	+0.015	+0.011	+0.016	+0.016	+0.018	+0.020
159	+0.021	+0.009	+0.018	+0.007	+0.007	+0.012	+0.003	+0.007	+0.001	+0.005	+0.000	+0.000	+0.002	+0.004
160	+0.006	+0.006	+0.003	+0.008	+0.008	+0.001	+0.010	+0.006	+0.012	+0.008	+0.013	+0.012	+0.014	+0.016
161	+0.003	+0.015	+0.005	+0.016	+0.016	+0.009	+0.018	+0.013	+0.019	+0.015	+0.020	+0.019	+0.021	+0.022
162	+0.033	+0.021	+0.032	+0.021	+0.021	+0.030	+0.021	+0.027	+0.021	+0.026	+0.021	+0.024	+0.022	+0.021
163	+0.017	+0.005	+0.016	+0.005	+0.005	+0.013	+0.004	+0.010	+0.004	+0.009	+0.004	+0.006	+0.004	+0.003
164	+0.003	+0.009	+0.001	+0.010	+0.010	+0.002	+0.011	+0.006	+0.012	+0.007	+0.012	+0.010	+0.012	+0.011
165	+0.007	+0.019	+0.009	+0.020	+0.020	+0.013	+0.022	+0.017	+0.023	+0.018	+0.023	+0.021	+0.023	+0.024
166	+0.009	+0.021	+0.010	+0.021	+0.021	+0.013	+0.022	+0.015	+0.021	+0.017	+0.022	+0.019	+0.021	+0.022
167	+0.002	+0.014	+0.002	+0.013	+0.013	+0.008	+0.012	+0.004	+0.010	+0.004	+0.006	+0.005	+0.007	+0.006
168	+0.022	+0.010	+0.022	+0.011	+0.012	+0.021	+0.012	+0.021	+0.015	+0.020	+0.015	+0.020	+0.018	+0.019
169	+0.023	+0.011	+0.023	+0.012	+0.013	+0.022	+0.013	+0.021	+0.015	+0.020	+0.015	+0.019	+0.017	+0.018
170	+0.017	+0.005	+0.017	+0.006	+0.007	+0.015	+0.006	+0.014	+0.008	+0.013	+0.008	+0.012	+0.010	+0.011
171	+0.014	+0.026	+0.015	+0.026	+0.026	+0.018	+0.027	+0.021	+0.027	+0.022	+0.027	+0.025	+0.027	+0.026
172	+0.015	+0.027	+0.016	+0.027	+0.027	+0.022	+0.031	+0.026	+0.032	+0.026	+0.034	+0.034	+0.036	+0.037
173	+0.004	+0.008	+0.002	+0.009	+0.009	+0.001	+0.010	+0.003	+0.009	+0.005	+0.010	+0.007	+0.009	+0.008
174	+0.017	+0.029	+0.019	+0.030	+0.030	+0.022	+0.031	+0.025	+0.031	+0.026	+0.031	+0.028	+0.030	+0.031
175	+0.007	+0.019	+0.008	+0.019	+0.019	+0.012	+0.021	+0.016	+0.022	+0.018	+0.023	+0.023	+0.025	+0.027
176	+0.010	+0.022	+0.011	+0.022	+0.022	+0.013	+0.022	+0.016	+0.022	+0.017	+0.022	+0.019	+0.021	+0.022
177	+0.010	+0.002	+0.010	+0.001	+0.000	+0.010	+0.001	+0.009	+0.003	+0.008	+0.003	+0.008	+0.006	+0.007
178	+0.012	+0.000	+0.012	+0.001	+0.002	+0.010	+0.001	+0.009	+0.003	+0.009	+0.004	+0.008	+0.006	+0.007
179	+0.018	+0.030	+0.017	+0.028	+0.027	+0.017	+0.026	+0.017	+0.023	+0.017	+0.022	+0.018	+0.020	+0.019
180	+0.031	+0.043	+0.032	+0.043	+0.042	+0.033	+0.042	+0.034	+0.040	+0.035	+0.040	+0.036	+0.038	+0.037
181	+0.025	+0.013	+0.025	+0.014	+0.015	+0.025	+0.016	+0.023	+0.017	+0.023	+0.018	+0.022	+0.020	+0.021
182	+0.040	+0.052	+0.041	+0.052	+0.051	+0.041	+0.050	+0.042	+0.048	+0.042	+0.047	+0.044	+0.046	+0.045
183	+0.038	+0.050	+0.038	+0.049	+0.048	+0.039	+0.048	+0.041	+0.047	+0.041	+0.046	+0.042	+0.044	+0.043
184	+0.018	+0.030	+0.018	+0.029	+0.028	+0.019	+0.028	+0.019	+0.025	+0.019	+0.024	+0.020	+0.022	+0.021
185	+0.022	+0.010	+0.022	+0.011	+0.012	+0.021	+0.012	+0.020	+0.014	+0.020	+0.015	+0.019	+0.017	+0.018
186	+0.019	+0.007	+0.019	+0.008	+0.009	+0.020	+0.011	+0.020	+0.014	+0.020	+0.015	+0.020	+0.018	+0.020
187	+0.024	+0.012	+0.024	+0.013	+0.014	+0.023	+0.014	+0.023	+0.017	+0.023	+0.018	+0.022	+0.020	+0.021
188	+0.046	+0.034	+0.046	+0.035	+0.036	+0.045	+0.036	+0.043	+0.037	+0.042	+0.037	+0.041	+0.039	+0.039
189	+0.039	+0.027	+0.040	+0.029	+0.030	+0.040	+0.031	+0.040	+0.034	+0.041	+0.036	+0.040	+0.038	+0.039
190	+0.025	+0.013	+0.025	+0.014	+0.015	+0.025	+0.016	+0.025	+0.019	+0.025	+0.020	+0.025	+0.023	+0.024
191	+0.017	+0.005	+0.018	+0.007	+0.008	+0.019	+0.010	+0.019	+0.013	+0.020	+0.015	+0.019	+0.017	+0.019
192	+0.024	+0.012	+0.025	+0.014	+0.015	+0.026	+0.017	+0.027	+0.021	+0.027	+0.022	+0.027	+0.025	+0.027
193	+0.037	+0.025	+0.038	+0.027	+0.028	+0.039	+0.030	+0.038	+0.032	+0.038	+0.033	+0.038	+0.036	+0.037
194	+0.015	+0.008	+0.017	+0.006	+0.007	+0.019	+0.010	+0.019	+0.013	+0.019	+0.014	+0.019	+0.017	+0.018
195	+0.036	+0.024	+0.035	+0.024	+0.024	+0.032	+0.023	+0.027	+0.021	+0.024	+0.019	+0.019	+0.017	+0.013
196	+0.045	+0.033	+0.045	+0.034	+0.035	+0.044	+0.035	+0.044	+0.038	+0.043	+0.038	+0.042	+0.040	+0.041
197	+0.015	+0.008	+0.015	+0.004	+0.005	+0.014	+0.005	+0.014	+0.008	+0.014	+0.009	+0.013	+0.011	+0.012
198	+0.063	+0.051	+0.064	+0.053	+0.054	+0.063	+0.054	+0.062	+0.056	+0.061	+0.056	+0.059	+0.057	+0.056
199	+0.025	+0.013	+0.025	+0.014	+0.015	+0.025	+0.016	+0.025	+0.019	+0.025	+0.020	+0.025	+0.023	+0.024
200	+0.015	+0.003	+0.015	+0.004	+0.005	+0.015	+0.006	+0.014	+0.008	+0.014	+0.009	+0.014	+0.012	+0.013
201	+0.035	+0.023	+0.036	+0.025	+0.026	+0.038	+0.029	+0.038	+0.032	+0.038	+0.033	+0.037	+0.035	+0.038
202	+0.035	+0.023	+0.034	+0.023	+0.024	+0.032	+0.023	+0.029	+0.023	+0.028	+0.023	+0.025	+0.023	+0.022
203	+0.059	+0.047	+0.059	+0.048	+0.049	+0.059	+0.050	+0.058	+0.052	+0.058	+0.053	+0.057	+0.055	+0.057
204	+0.015	+0.027	+0.015	+0.026	+0.025	+0.017	+0.026	+0.018	+0.024	+0.018	+0.023	+0.020	+0.022	+0.021
205	+0.010	+0.002	+0.010	+0.001	+0.000	+0.010	+0.001	+0.010	+0.004	+0.009	+0.004	+0.009	+0.007	+0.009
206	+0.030	+0.018	+0.030	+0.019	+0.020	+0.028	+0.019	+0.026	+0.020	+0.025	+0.020	+0.024	+0.022	+0.023
207	+0.016	+0.027	+0.016	+0.027	+0.026	+0.018	+0.027	+0.021	+0.027	+0.022	+0.027	+0.024	+0.026	+0.026
208	+0.002	+0.010	+0.002	+0.009	+0.008	+0.001	+0.008	+0.000	+0.006	+0.000	+0.005	+0.002	+0.004	+0.003
209	+0.048	+0.036	+0.047	+0.036	+0.036	+0.044	+0.035	+0.042	+0.036	+0.040	+0.035	+0.038	+0.036	+0.035
210	+0.015	+0.027	+0.016	+0.027	+0.027	+0.019	+0.028	+0.021	+0.027	+0.023	+0.028	+0.026	+0.028	+0.029
211	+0.010	+0.022	+0.011	+0.022	+0.022	+0.013	+0.022	+0.015	+0.021	+0.017	+0.022	+0.019	+0.021	+0.022
212	+0.060	+0.048	+0.059	+0.048	+0.048	+0.056	+0.047	+0.054	+0.048	+0.052	+0.047	+0.050	+0.048	+0.047
213	+0.027	+0.015	+0.026	+0.015	+0.016	+0.024	+0.015	+0.021	+0.015	+0.019	+0.014	+0.017	+0.015	+0.014
214	+0.049	+0.037	+0.048	+0.037	+0.037	+0.046	+0.037	+0.044	+0.038	+0.043	+0.038	+0.040	+0.038	+0.037
215	+0.010	+0.022	+0.012	+0.023	+0.023	+0.016	+0.025	+0.021	+0.027	+0.024	+0.029	+0.027	+0.029	+0.031
216	+0.018	+0.006	+0.017	+0.006	+0.007	+0.015	+0.006	+0.013	+0.007	+0.011	+0.006	+0.009	+0.007	+0.007
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SUMMARY OF MEAN ANOMALIES FOR VARIOUS DEPTHS OF COMPENSATION AND THE VARIOUS VALUES OF EQUATORIAL GRAVITY.

Depths of compensation.....	42.6 km.		56.9 km.		60.0 km.		85.3 km.	
Equatorial value of gravity.....	978.030	978.042	978.030	978.041	978.030	978.040	978.030	978.039
Mean anomalies with regard to sign, using groups.....	+0.012	0.000	+0.011	0.000	+0.010	0.000	+0.009	0.000
Mean anomalies without regard to sign, using groups.....	.019	.016	.018	.016			.018	.017
Mean anomalies with regard to sign, all stations.....	+ .012	.000	+ .011	.000		.000	+ .008	— .001
Mean anomalies without regard to sign, all stations.....	.022	.020	.021	.020		.020	.020	.020
Mean anomalies with regard to sign, all stations (Seattle stations omitted).....	+ .013	+ .001	+ .012	+ .001		+ .001	+ .009	.000
Mean anomalies without regard to sign, all stations (Seattle stations omitted).....	.021	.019	.020	.019		.019	.020	.019

Depths of compensation.....	113.7 km.		127.9 km.		156.25 km.		184.6 km.	
Equatorial value of gravity.....	978.030	978.036	978.030	978.035	978.030	978.032	978.030	978.029
Mean anomalies with regard to sign, using groups.....	+0.006	0.000	+0.005	0.000	+0.002	0.000	—0.001	0.000
Mean anomalies without regard to sign, using groups.....	.018	.017	.018	.017	.018	.018	.019	.019
Mean anomalies with regard to sign, all stations.....	+ .005	— .001	+ .004	— .001	+ .001	— .001	— .002	— .001
Mean anomalies without regard to sign, all stations.....	.020	.020	.020	.020	.020	.021	.021	.021
Mean anomalies with regard to sign, all stations (Seattle stations omitted).....	+ .006	.000	+ .005	.000	+ .002	.000	— .001	.000
Mean anomalies without regard to sign, all stations (Seattle stations omitted).....	.020	.019	.020	.019	.020	.020	.020	.020

The names, elevations, and locations of the stations are given in the table on pages 50–52. The values of $g-g_0$ for any depth are obtained by combining the correction for topography and compensation for that depth given in the table on pages 100–102, with the correction for the elevation of the station and the theoretical value of the gravity for the latitude of the station computed by the Helmert formula of 1901, which are given on pages 50–52. In this formula the value of the first term is 978.030. This is the value in dynes of the intensity of gravity at the equator. In order to get the Hayford 1912 anomalies (which were computed by a formula which is the same as that of Helmert of 1901, except that the first term is 978.038), add algebraically -0.008 to the $g-g_0$ values. For instance, the value of $g-g_0$ for station 25 and the depth 42.6 km. is -0.005 . The 1912 anomaly will be -0.013 dyne.

The difference at a station between the values of $g-g_0$ for any two depths is of the same amount, but of opposite sign, to the difference between the effects of topography and compensation for the same depths in the table on pages 100–102.

The differences, $g-g_0$, between the observed gravity and the computed gravity using a depth of compensation of 42.6 km. and the Helmert 1901 formula are shown in the second column of the preceding table. The mean value of $g-g_0$ for this depth was found to be $+0.012$ dyne. In obtaining this mean groups of stations within limited areas were combined and each group given unit weight. The third column of the preceding table contains the anomalies for the depth 42.6 km. after the mean of the second column, $+0.012$, has been applied as a correction to the first term of Helmert's formula. These are the most probable anomalies from observations in the United States if a depth of compensation of 42.6 km. and a flattening of $1/298.2$ are assumed. The anomalies for the other depths were obtained in a similar manner, except for the depth 60.0 km. The anomalies for this depth were obtained from the analytical solution 1c on page 123.

The use of 94 additional stations in the United States has changed the value of the first term of the United States Coast and Geodetic Survey gravity formula of 1912, based on a depth of 113.7 km., only from 978.038 to 978.036. The lowest value of the first term of the gravity formula as obtained in the preceding table is 978.029 for the depth of 184.6 km.

If individual stations are investigated, it will be found that those stations which are in mountainous regions and along the coast near deep water have the greatest range in the values of $g-g_0$ in the preceding table.

At the end of the table there is given a summary of the mean anomalies for various depths of compensation and the several values of equatorial gravity. This shows that the mean anomaly with regard to sign when stations near together are combined in groups has the same sign and is within 0.001 of the mean of all stations for each depth. It also shows that the Seattle stations at which the anomaly is -0.093 for each have little effect in deciding the character of the results. For the purpose of comparison the means with regard to sign are given below for

the formula derived from the investigation of which special publication No. 12 is a report. It has 978.038 as the first term, which is also the value of gravity at the equator.

The solution by least squares which gave from data in the United States the theoretically best value of gravity at the equator and the depth of compensation is discussed on pages 123 and 124. In the above table there are given the values of the anomalies for the depth thus determined, 60 km., although the depth, 56.9 km., gives nearly the same set of values.

The summary alone gives no strong evidence in favor of any one depth of compensation, for the means without regard to sign have little change from one depth to another while the mean with regard to sign is made the same (zero) for each depth.

The means with regard to sign of the anomalies for the different depths based upon the United States Coast and Geodetic Survey formula of 1912 are given in the following table:

Mean anomalies for various depths, based upon the United States Coast and Geodetic Survey formula of 1912, $\gamma_0 = 978.038 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi)$.

Depths of compensation	42.6 km.	56.9 km.	60.0 km.	85.3 km.	113.7 km.	127.9 km.	156.25 km.	184.6 km.
Mean anomaly with regard to sign, using groups	+0.004	+0.003	+0.002	+0.001	-0.002	-0.003	-0.006	-0.009
Mean anomaly with regard to sign, for all stations	+ .004	+ .003		.000	- .003	- .004	- .007	- .010
Mean anomaly with regard to sign, omitting Seattle stations ..	+ .005	+ .004		+ .001	- .002	- .003	- .006	- .009

This table is instructive only in showing how the computed value of gravity increases on an average with the depth of compensation.

THE RELATION BETWEEN THE DEPTH OF COMPENSATION AND THE TOPOGRAPHY.

While the mean anomalies with and without regard to sign, as shown in the summary above and the one on page 67, do not give any intimation as to which depth is the most probable one, the tables given below do seem to throw some light on this question.

The first part of the table shows the anomalies for the coast stations for the several depths, the second part has similar data for the mountainous stations below the general level, and the third one gives the data for mountainous stations above the general level, while the fourth and fifth parts of the table give the data for the stations near but not on the coasts and in the interior not in mountainous regions, respectively. The computed value in each case from which the anomalies were obtained depends upon the theoretical value of gravity at the equator, as obtained from all of the 216 stations for the particular depth.

Hayford anomalies for various depths of compensation arranged in groups according to topography.

Station number	Hayford anomaly for depth of compensation of—						
	42.6 km.	56.9 km.	85.3 km.	113.7 km.	127.9 km.	156.25 km.	184.6 km.
<i>Twenty-seven coast stations in the order of their distances from the 1000-fathom line:</i>							
54.....	-0.006	-0.010	-0.017	-0.021	-0.023	-0.025	-0.027
18.....	- .004	- .008	- .014	- .019	- .022	- .025	- .027
80.....	- .010	- .010	- .011	- .011	- .010	- .010	- .009
90.....	- .037	- .039	- .043	- .046	- .048	- .049	- .051
92.....	+ .016	+ .015	+ .013	+ .012	+ .011	+ .010	+ .010
1.....	+ .019	+ .015	+ .010	+ .007	+ .006	+ .003	+ .002
125.....	- .016	- .018	- .020	- .021	- .023	- .023	- .024
8.....	+ .031	+ .030	+ .028	+ .029	+ .028	+ .029	+ .030
126.....	- .014	- .016	- .019	- .020	- .021	- .022	- .023
215.....	- .022	- .023	- .025	- .027	- .029	- .029	- .030
149.....	- .022	- .024	- .027	- .029	- .031	- .032	- .034
164.....	- .009	- .010	- .011	- .012	- .012	- .012	- .011
127.....	- .004	- .007	- .010	- .012	- .014	- .015	- .017
5.....	- .009	- .010	- .011	- .011	- .012	- .011	- .011
4.....	+ .005	+ .004	+ .002	+ .002	+ .001	+ .001	+ .001
27.....	+ .025	+ .025	+ .025	+ .024	+ .024	+ .024	+ .023
28.....	+ .027	+ .027	+ .026	+ .026	+ .025	+ .025	+ .025
68.....	- .049	- .049	- .049	- .048	- .049	- .049	- .050
2.....	+ .029	+ .027	+ .023	+ .020	+ .019	+ .017	+ .015
161.....	- .015	- .016	- .018	- .019	- .020	- .021	- .021
3.....	+ .018	+ .017	+ .013	+ .012	+ .010	+ .009	+ .008
29.....	+ .009	+ .008	+ .007	+ .007	+ .006	+ .006	+ .005
30.....	+ .009	+ .009	+ .007	+ .007	+ .006	+ .006	+ .005
17.....	- .015	- .016	- .018	- .019	- .020	- .020	- .020
7.....	- .009	- .009	- .009	- .007	- .007	- .006	- .004
159.....	+ .009	+ .007	+ .003	+ .001	- .000	- .002	- .003
128.....	- .012	- .013	- .013	- .013	- .013	- .012	- .012
Mean with regard to sign.....	- .002	- .003	- .006	- .007	- .008	- .009	- .009
Mean without regard to sign.....	.017	.017	.017	.018	.018	.018	.018

Hayford anomalies for various depths of compensation arranged in groups according to topography—Continued.

Station number	Hayford anomaly for depth of compensation of—						
	42.6 km.	56.9 km.	85.3 km.	113.7 km.	127.9 km.	156.25 km.	184.6 km.
Thirty-six stations in mountainous regions and below the general level arranged in the order of their distances below the general level:							
70.....	+0.003	-0.001	-0.006	-0.011	-0.014	-0.017	-0.022
156.....	-0.005	-0.007	-0.011	-0.013	-0.014	-0.016	-0.018
105.....	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.021
202.....	+0.023	+0.023	+0.023	+0.023	+0.023	+0.023	+0.022
67.....	+0.004	-0.001	-0.006	-0.011	-0.014	-0.018	-0.023
153.....	-0.019	-0.020	-0.021	-0.021	-0.021	-0.021	-0.021
210.....	-0.027	-0.027	-0.028	-0.027	-0.028	-0.028	-0.028
175.....	-0.019	-0.019	-0.021	-0.022	-0.023	-0.025	-0.026
172.....	-0.027	-0.027	-0.031	-0.032	-0.034	-0.036	-0.037
85.....	-0.005	-0.003	-0.000	+0.003	+0.003	+0.005	+0.006
176.....	-0.022	-0.022	-0.022	-0.022	-0.022	-0.021	-0.021
131.....	-0.021	-0.021	-0.022	-0.022	-0.023	-0.024	-0.025
155.....	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019
201.....	+0.023	+0.025	+0.029	+0.032	+0.033	+0.035	+0.038
63.....	+0.009	+0.009	+0.009	+0.009	+0.009	+0.009	+0.008
198.....	+0.051	+0.053	+0.054	+0.056	+0.056	+0.057	+0.057
113.....	-0.033	-0.031	-0.028	-0.025	-0.025	-0.023	-0.021
130.....	-0.038	-0.038	-0.037	-0.037	-0.037	-0.037	-0.038
112.....	+0.025	+0.028	+0.032	+0.035	+0.035	+0.038	+0.039
110.....	-0.004	-0.006	-0.010	-0.013	-0.014	-0.016	-0.019
111.....	-0.016	-0.019	-0.023	-0.026	-0.027	-0.028	-0.029
117.....	+0.031	+0.034	+0.037	+0.038	+0.038	+0.039	+0.039
115.....	-0.009	-0.007	-0.007	-0.007	-0.008	-0.009	-0.012
109.....	+0.032	+0.034	+0.034	+0.034	+0.033	+0.032	+0.031
82.....	+0.022	+0.020	+0.018	+0.015	+0.014	+0.012	+0.008
45.....	+0.039	+0.037	+0.030	+0.022	+0.018	+0.012	+0.004
194.....	+0.003	+0.006	+0.010	+0.013	+0.014	+0.017	+0.018
42.....	+0.006	+0.003	-0.001	-0.005	-0.007	-0.010	-0.015
195.....	+0.024	+0.024	+0.023	+0.021	+0.019	+0.017	+0.013
49.....	+0.009	+0.010	+0.012	+0.012	+0.012	+0.012	+0.010
44.....	-0.020	-0.017	-0.014	-0.014	-0.015	-0.016	-0.018
79.....	-0.003	+0.001	+0.006	+0.010	+0.011	+0.014	+0.015
78.....	-0.004	-0.001	+0.002	+0.004	+0.005	+0.006	+0.007
69.....	-0.000	-0.001	+0.005	+0.008	+0.010	+0.012	+0.017
46.....	+0.019	+0.023	+0.026	+0.026	+0.025	+0.025	+0.022
47.....	-0.032	-0.027	-0.022	-0.019	-0.018	-0.017	-0.017
Mean with regard to sign.....	-0.000	-0.000	-0.000	-0.001	-0.001	-0.002	-0.003
Mean without regard to sign.....	-0.018	-0.018	-0.019	-0.020	-0.021	-0.021	-0.022
Twenty stations in mountainous regions and above the general level arranged in the order of their distances above the general level:							
129.....	-0.009	+0.011	-0.014	-0.016	-0.017	-0.018	-0.019
71.....	+0.020	+0.016	+0.010	+0.005	+0.002	-0.001	-0.006
116.....	+0.002	-0.003	-0.012	-0.019	-0.023	-0.028	-0.033
101.....	+0.046	+0.045	+0.043	+0.042	+0.041	+0.041	+0.040
52.....	+0.019	+0.015	+0.008	+0.001	-0.003	-0.007	-0.013
51.....	+0.043	+0.038	+0.030	+0.023	+0.019	+0.014	+0.009
48.....	+0.026	+0.021	+0.013	+0.006	+0.003	-0.001	-0.005
152.....	+0.013	+0.009	+0.002	-0.003	-0.005	-0.008	-0.011
50.....	+0.023	+0.018	+0.008	-0.000	-0.004	-0.009	-0.015
98.....	+0.037	+0.034	+0.028	+0.023	+0.021	+0.018	+0.015
64.....	-0.036	-0.040	-0.045	-0.048	-0.049	-0.050	-0.052
20.....	+0.026	+0.022	+0.015	+0.012	+0.010	+0.008	+0.006
86.....	+0.020	+0.016	+0.011	+0.008	+0.007	+0.005	+0.004
103.....	-0.006	-0.012	-0.021	-0.027	-0.029	-0.033	-0.036
75.....	+0.067	+0.062	+0.057	+0.054	+0.052	+0.051	+0.050
68.....	+0.015	+0.012	+0.007	+0.003	+0.001	-0.001	-0.006
114.....	+0.011	+0.001	-0.015	-0.026	-0.032	-0.039	-0.047
55.....	+0.021	+0.014	+0.004	-0.001	-0.004	-0.007	-0.009
102.....	+0.028	+0.022	+0.012	+0.006	+0.003	-0.001	-0.004
43.....	+0.057	+0.046	+0.032	+0.023	+0.019	+0.013	+0.006
Mean with regard to sign.....	+0.021	+0.016	+0.009	+0.003	+0.001	-0.003	-0.006
Mean without regard to sign.....	-0.026	-0.023	-0.019	-0.017	-0.017	-0.018	-0.019
Forty-six stations near the coast, in the order of their distances from the open coast:							
157.....	-0.024	-0.026	-0.032	-0.034	-0.036	-0.038	-0.040
31.....	-0.007	-0.007	-0.007	-0.006	-0.007	-0.005	-0.005
25.....	-0.017	-0.017	-0.017	-0.017	-0.018	-0.017	-0.018
93.....	-0.041	-0.042	-0.043	-0.042	-0.042	-0.042	-0.042
217.....	-0.005	-0.006	-0.007	-0.008	-0.008	-0.008	-0.009
23.....	-0.010	-0.009	-0.009	-0.009	-0.009	-0.008	-0.008
28.....	-0.013	-0.015	-0.016	-0.018	-0.019	-0.020	-0.021
160.....	-0.006	-0.008	-0.010	-0.012	-0.013	-0.014	-0.015
24.....	+0.024	+0.024	+0.024	+0.024	+0.023	+0.023	+0.023
124.....	-0.026	-0.027	-0.029	-0.031	-0.032	-0.033	-0.034

Hayford anomalies for various depths of compensation arranged in groups according to topography—Continued.

Station number					Hayford anomaly for depth of compensation of—							
Station number	Station number	Station number	Station number	Station number	42.6 km.	56.9 km.	85.3 km.	113.7 km.	127.9 km.	156.25 km.	184.6 km.	Station number
Forty-six stations near the coast, in the order of their distances from the open coast—Continued.												
158	158	158	158	158	0.008	0.010	-0.013	-0.015	-0.016	-0.018	-0.019	158
148	148	148	148	148	0.011	0.012	-0.015	-0.016	-0.017	-0.018	-0.019	148
81	81	81	81	81	0.016	0.010	0.000	-0.008	-0.012	-0.018	-0.024	81
147	147	147	147	147	0.017	0.016	+0.015	+0.015	+0.014	+0.014	+0.014	147
150	150	150	150	150	0.005	0.005	+0.004	+0.004	+0.004	+0.004	+0.003	150
146	146	146	146	146	0.005	0.005	+0.005	+0.005	+0.005	+0.005	+0.005	146
213	213	213	213	213	0.015	0.015	+0.015	+0.015	+0.014	+0.015	+0.015	213
173	173	173	173	173	0.008	0.009	-0.010	-0.009	-0.010	-0.009	-0.008	173
209	209	209	209	209	0.036	0.036	+0.035	+0.035	+0.035	+0.036	+0.036	209
21	21	21	21	21	0.037	0.037	+0.038	+0.039	+0.039	+0.040	+0.040	21
22	22	22	22	22	0.039	0.039	+0.040	+0.041	+0.040	+0.041	+0.041	22
163	163	163	163	163	0.005	0.005	+0.004	+0.004	+0.004	+0.004	+0.004	163
145	145	145	145	145	0.016	0.016	+0.015	+0.016	+0.015	+0.016	+0.017	145
84	84	84	84	84	0.037	0.038	+0.038	+0.039	+0.039	+0.040	+0.040	84
216	216	216	216	216	0.006	0.006	+0.006	+0.007	+0.006	+0.007	+0.007	216
144	144	144	144	144	0.006	0.006	-0.006	-0.004	-0.004	-0.003	-0.001	144
212	212	212	212	212	0.048	0.048	+0.047	+0.048	+0.048	+0.048	+0.048	212
214	214	214	214	214	0.037	0.037	+0.037	+0.038	+0.038	+0.038	+0.038	214
91	91	91	91	91	0.037	0.038	+0.038	+0.038	+0.037	+0.037	+0.037	91
9	9	9	9	9	0.025	0.025	-0.021	-0.018	-0.017	-0.015	-0.014	9
65	65	65	65	65	0.003	0.005	+0.008	+0.011	+0.012	+0.014	+0.016	65
97	97	97	97	97	0.015	0.014	-0.012	-0.010	-0.009	-0.007	-0.005	97
123	123	123	123	123	0.043	0.042	-0.041	-0.041	-0.042	-0.042	-0.042	123
16	16	16	16	16	0.015	0.016	+0.017	+0.017	+0.016	+0.017	+0.017	16
10	10	10	10	10	0.010	0.009	-0.008	-0.006	-0.006	-0.001	-0.002	10
11	11	11	11	11	0.012	0.011	-0.010	-0.008	-0.007	-0.006	-0.004	11
19	19	19	19	19	0.013	0.012	-0.012	-0.011	-0.012	-0.012	-0.012	19
151	151	151	151	151	0.030	0.029	+0.028	+0.027	+0.027	+0.026	+0.025	151
219	219	219	219	219	0.045	0.046	-0.046	-0.047	-0.047	-0.046	-0.048	219
162	162	162	162	162	0.021	0.021	+0.021	+0.021	+0.021	+0.022	+0.022	162
165	165	165	165	165	0.019	0.020	-0.022	-0.023	-0.023	-0.023	-0.023	165
32	32	32	32	32	0.021	0.021	-0.021	-0.021	-0.021	-0.021	-0.021	32
94	94	94	94	94	0.019	0.018	-0.017	-0.015	-0.015	-0.013	-0.012	94
62	62	62	62	62	0.037	0.035	+0.033	+0.033	+0.032	+0.032	+0.032	62
106	106	106	106	106	0.016	0.015	-0.013	-0.011	-0.011	-0.009	-0.008	106
6	6	6	6	6	0.015	0.016	+0.017	+0.018	+0.019	+0.020	+0.022	6
Mean with regard to sign.					0.002	0.002	+0.001	+0.001	+0.001	+0.001	+0.001	
Mean without regard to sign.					0.020	0.020	0.020	0.020	0.020	0.021	0.021	
Eighty-seven stations in the interior and not in mountainous regions, arranged in the order of elevation:												
167	167	167	167	167	0.014	0.013	-0.012	-0.010	-0.009	-0.007	-0.005	167
95	95	95	95	95	0.005	0.003	0.000	+0.003	+0.004	+0.007	+0.009	95
168	168	168	168	168	0.010	0.011	+0.012	+0.015	+0.015	+0.018	+0.020	168
88	88	88	88	88	0.016	0.014	-0.011	-0.008	-0.008	-0.005	-0.003	88
13	13	13	13	13	0.024	0.026	+0.029	+0.032	+0.033	+0.035	+0.037	13
142	142	142	142	142	0.007	0.008	+0.011	+0.013	+0.014	+0.016	+0.019	142
87	87	87	87	87	0.020	0.020	+0.021	+0.023	+0.023	+0.024	+0.025	87
141	141	141	141	141	0.021	0.019	-0.016	-0.014	-0.013	-0.011	-0.009	141
132	132	132	132	132	0.026	0.025	-0.024	-0.023	-0.023	-0.022	-0.020	132
35	35	35	35	35	0.012	0.011	-0.009	-0.007	-0.006	-0.004	-0.002	35
38	38	38	38	38	0.010	0.008	-0.006	-0.003	-0.002	0.000	0.003	38
169	169	169	169	169	0.011	0.012	+0.013	+0.015	+0.015	+0.017	+0.019	169
120	120	120	120	120	0.010	0.009	-0.009	-0.006	-0.006	-0.003	-0.001	120
170	170	170	170	170	0.005	0.006	+0.006	+0.008	+0.008	+0.010	+0.011	170
89	89	89	89	89	0.020	0.020	-0.019	-0.018	-0.017	-0.016	-0.014	89
174	174	174	174	174	0.029	0.030	-0.031	-0.031	-0.031	-0.030	-0.030	174
177	177	177	177	177	0.002	0.001	+0.001	+0.003	+0.003	+0.006	+0.008	177
179	179	179	179	179	0.030	0.028	-0.026	-0.023	-0.022	-0.020	-0.018	179
36	36	36	36	36	0.011	0.010	-0.007	-0.005	-0.005	-0.003	-0.002	36
138	138	138	138	138	0.019	0.018	-0.016	-0.014	-0.013	-0.011	-0.008	138
104	104	104	104	104	0.027	0.025	+0.024	+0.022	+0.022	+0.021	+0.021	104
135	135	135	135	135	0.024	0.024	-0.023	-0.022	-0.022	-0.021	-0.021	135
143	143	143	143	143	0.016	0.017	+0.018	+0.020	+0.020	+0.022	+0.023	143
134	134	134	134	134	0.028	0.028	-0.027	-0.025	-0.025	-0.023	-0.022	134
166	166	166	166	166	0.021	0.021	-0.022	-0.022	-0.022	-0.021	-0.021	166
181	181	181	181	181	0.013	0.014	+0.016	+0.017	+0.018	+0.020	+0.022	181
207	207	207	207	207	0.027	0.027	-0.027	-0.027	-0.027	-0.026	-0.026	207
14	14	14	14	14	0.025	0.026	-0.027	-0.028	-0.028	-0.029	-0.030	14
33	33	33	33	33	0.005	0.004	-0.002	-0.001	-0.001	-0.001	-0.003	33
203	203	203	203	203	0.048	0.050	+0.052	+0.053	+0.053	+0.055	+0.057	203
137	137	137	137	137	0.001	0.001	+0.001	+0.003	+0.003	+0.004	+0.006	137
178	178	178	178	178	0.000	0.001	+0.001	+0.003	+0.004	+0.006	+0.007	178
73	73	73	73	73	0.002	0.003	+0.004	+0.007	+0.007	+0.009	+0.011	73
136	136	136	136	136	0.013	0.012	-0.011	-0.010	-0.010	-0.009	-0.008	136
211	211	211	211	211	0.022	0.022	-0.021	-0.021	-0.021	-0.021	-0.021	211

Hayford anomalies for various depths of compensation arranged in groups according to topography—Continued.

Station number	Hayford anomaly for depth of compensation of—						
	42.6 km.	56.9 km.	85.3 km.	113.7 km.	127.9 km.	156.25 km.	184.6 km.
Eighty-seven stations in the interior and not in mountainous regions arranged in the order of elevation—Contd.							
121.....	0.000	+0.001	+0.002	+0.004	+0.004	+0.006	+0.006
12.....	-.030	-.029	-.027	-.025	-.024	-.022	-.020
59.....	+.012	+.014	+.017	+.021	+.022	+.025	+.028
34.....	-.022	-.020	-.019	-.017	-.017	-.016	-.015
74.....	+.064	+.066	+.058	+.061	+.062	+.065	+.067
191.....	+.005	+.007	+.010	+.013	+.015	+.017	+.020
133.....	-.023	-.024	-.027	-.028	-.029	-.030	-.031
37.....	-.007	-.006	-.005	-.003	-.003	-.001	-.000
39.....	-.021	-.019	-.016	-.014	-.013	-.010	-.008
154.....	-.033	-.034	-.036	-.036	-.037	-.038	-.038
171.....	-.026	-.026	-.027	-.027	-.027	-.027	-.026
196.....	+.033	+.034	+.035	+.038	+.038	+.040	+.042
140.....	+.015	+.015	+.016	+.018	+.019	+.020	+.022
154.....	-.030	-.029	-.028	-.025	-.024	-.022	-.020
180.....	-.043	-.043	-.042	-.040	-.040	-.038	-.037
122.....	+.010	+.011	+.011	+.013	+.013	+.014	+.016
200.....	+.003	+.004	+.006	+.008	+.009	+.012	+.014
199.....	+.013	+.014	+.016	+.019	+.020	+.023	+.025
15.....	-.021	-.021	-.022	-.021	-.021	-.021	-.021
197.....	+.003	+.004	+.005	+.008	+.009	+.011	+.013
119.....	+.011	+.012	+.015	+.017	+.018	+.021	+.022
182.....	-.052	-.052	-.050	-.048	-.047	-.046	-.044
206.....	-.010	-.009	-.008	-.006	-.005	-.004	-.002
204.....	-.027	-.026	-.026	-.024	-.023	-.022	-.020
108.....	-.011	-.009	-.007	-.004	-.003	.000	+.002
185.....	+.010	+.011	+.012	+.014	+.015	+.017	+.019
96.....	-.052	-.052	-.051	-.050	-.049	-.048	-.046
218 ^a	-.050	-.049	-.048	-.047	-.046	-.044	-.043
183.....	+.012	+.012	+.012	+.013	+.014	+.015	+.016
139.....	+.007	+.008	+.011	+.014	+.015	+.018	+.021
60.....	-.005	-.004	-.001	+.003	+.004	+.007	+.010
58.....	+.023	+.023	+.023	+.025	+.025	+.027	+.028
189.....	+.027	+.029	+.031	+.034	+.036	+.038	+.040
118.....	+.006	+.008	+.012	+.016	+.017	+.021	+.024
57.....	+.042	+.041	+.040	+.040	+.039	+.040	+.041
40.....	+.009	+.011	+.013	+.016	+.017	+.020	+.022
107.....	+.027	+.026	+.025	+.026	+.026	+.027	+.028
205.....	-.002	-.001	+.001	+.004	+.004	+.007	+.009
76.....	-.002	-.001	+.002	+.004	+.005	+.006	+.010
190.....	+.013	+.014	+.016	+.019	+.020	+.023	+.025
192.....	+.012	+.014	+.017	+.021	+.022	+.025	+.028
61.....	-.027	-.028	-.028	-.027	-.027	-.027	-.026
77.....	+.020	+.023	+.026	+.031	+.032	+.036	+.038
72.....	+.032	+.033	+.033	+.034	+.034	+.035	+.036
193.....	+.025	+.027	+.030	+.032	+.033	+.036	+.037
206.....	+.018	+.019	+.019	+.020	+.020	+.022	+.023
187.....	+.012	+.013	+.014	+.017	+.018	+.020	+.022
188.....	+.034	+.035	+.036	+.037	+.037	+.039	+.039
83.....	-.008	-.006	-.005	-.004	-.003	-.002	-.001
100.....	-.019	-.017	-.016	-.015	-.015	-.014	-.014
41.....	-.009	-.009	-.010	-.010	-.010	-.009	-.009
99.....	-.012	-.013	-.014	-.014	-.015	-.015	-.017
Mean with regard to sign.....	-.003	-.002	-.001	+.001	+.001	+.003	+.005
Mean without regard to sign.....	.018	.019	.019	.019	.019	.020	.021

^a Not computed.

The mean value of the anomalies with regard to sign for the extreme depths for the coast stations is -0.002 for a depth of 42.6 km., and -0.009 for the depth of 184.6 km. The intermediate depths have values which fall between those two. This is an indication that at the coast the smallest depth is nearest the truth. These stations show a negative mean value for each depth which agrees with what are called the Hayford 1912 anomalies. (See p. 63.) This is as might be expected on account of the lighter material in the Cenozoic formation which is generally present along the coast. (See p. 76.)

The second table shows mean anomalies with regard to sign which are very close to zero. These are at stations in mountainous regions below the general level. The total range is only 0.003. There is no one depth which seems to be much more probable than any other.

The third table shows that the means with regard to sign for the anomalies at mountain stations above the general level have a total range of 0.027. They vary from $+0.021$ for depth

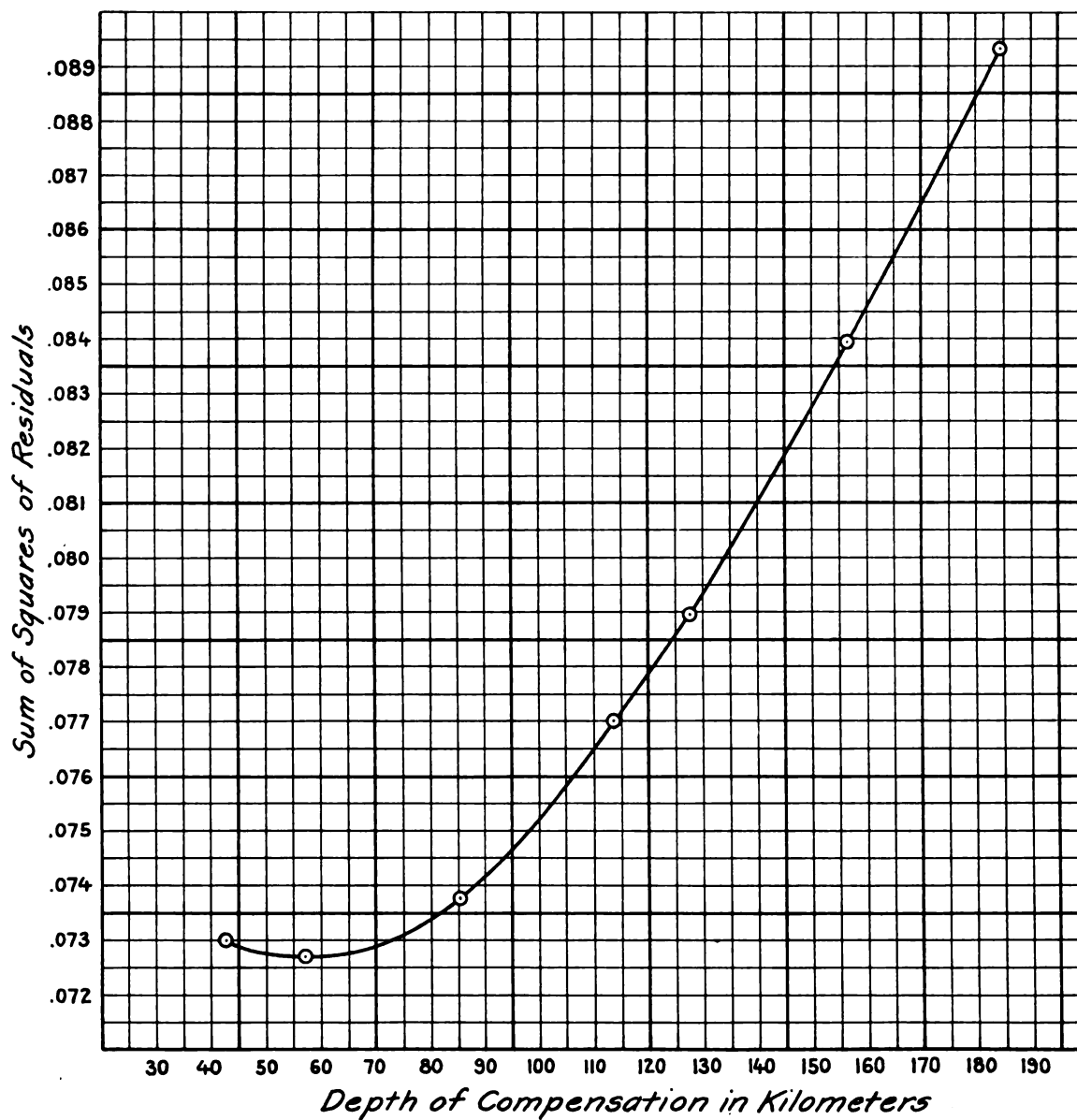


FIG. 5.—GRAPHIC DETERMINATION OF THE MOST PROBABLE DEPTH OF COMPENSATION FROM 216 STATIONS IN THE UNITED STATES.

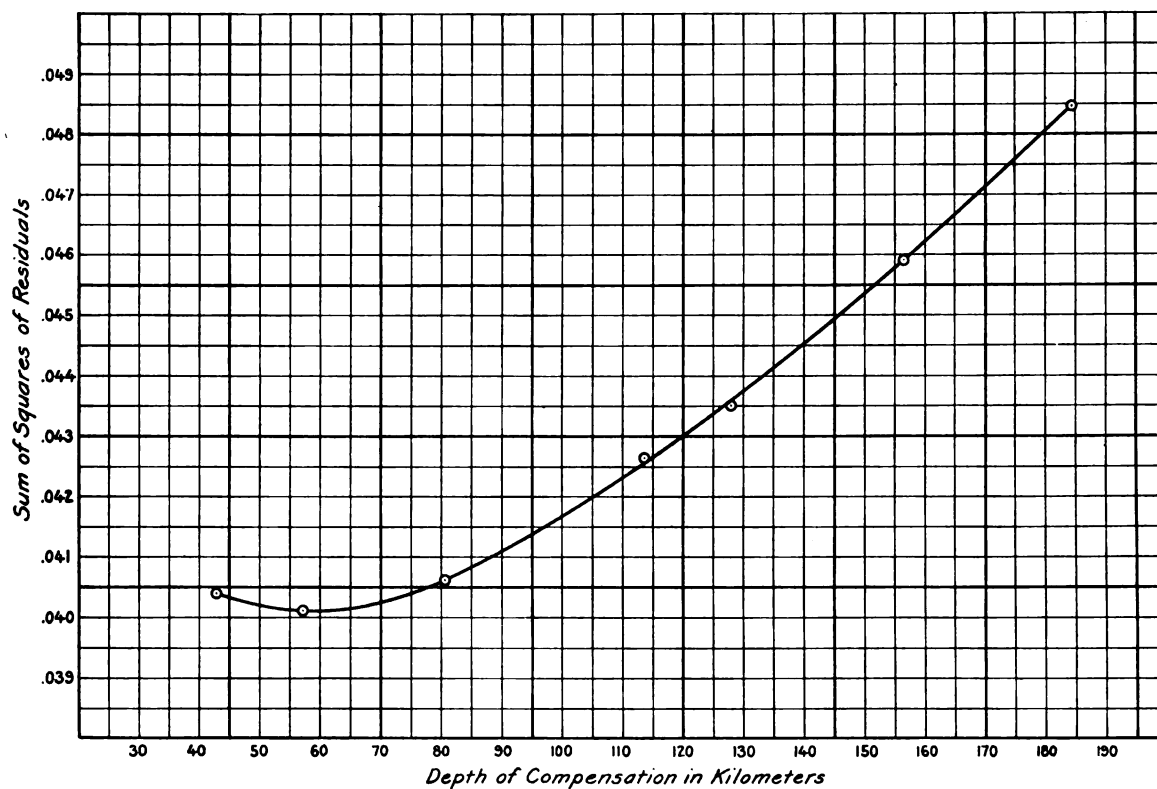


FIG. 6.—GRAPHIC DETERMINATION OF THE MOST PROBABLE DEPTH OF COMPENSATION FROM UNITED STATES STATIONS EAST OF THE NINETY-EIGHTH MERIDIAN.

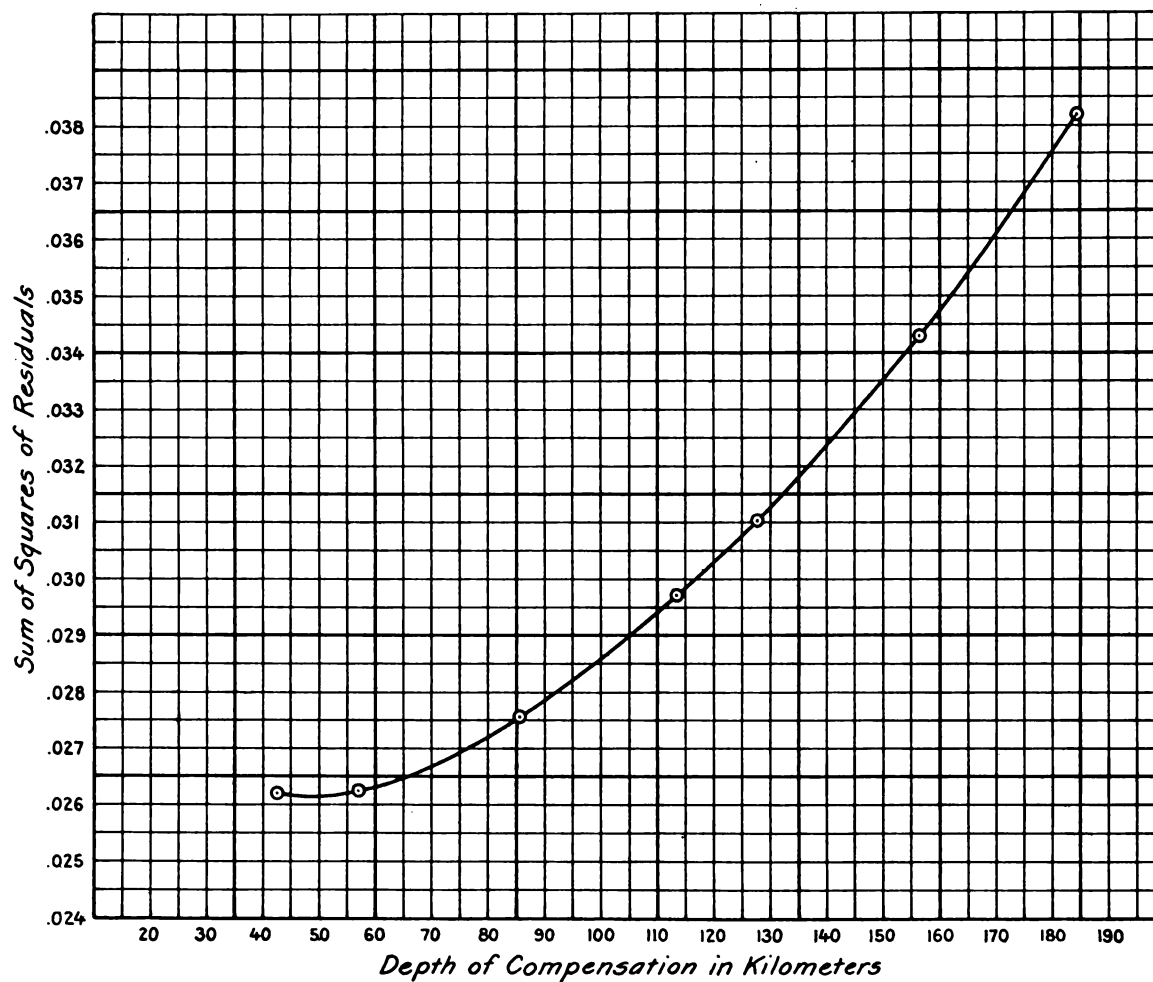


FIG. 7.—GRAPHIC DETERMINATION OF THE MOST PROBABLE DEPTH OF COMPENSATION FROM UNITED STATES STATIONS WEST OF THE NINETY-EIGHTH MERIDIAN.

42.6 km. to -0.006 for depth 184.6 km. The evidence here is strongly in favor of the greater depths.

The stations near but not on the coast have means which are close to zero for each depth. The range is from $+0.002$ for the depth 42.6 km. to $+0.001$ for the depth 184.6 km.

The stations in the interior not in mountainous regions have mean anomalies which range from -0.003 for the depth 42.6 km. to $+0.005$ for the depth 184.6 km. The intermediate depths have means which in no case are more than 0.003 from zero. The evidence from these stations is slightly in favor of the intermediate depths.

It is highly improbable that there should be two depths in mountainous regions, one for the higher land and one for the valleys, although it is possible that there may be a different depth in the mountainous regions than in the flat portions of the country.

We must conclude, therefore, that a depth of 42.6 or 56.9 km. is very improbable in the mountainous regions, for the mean values with regard to sign for the stations above the general level are $+0.021$ and $+0.016$ for those two depths, respectively, while for the stations below the general level the means are 0.000 and 0.000. There seems to be no evident explanation for this difference, aside from the effect of the depth, as the stations in any one of the topographic groups do not fall largely in any one geologic formation, as do the coast stations.

The depth 184.6 km. gives mean values of -0.006 for the high stations and -0.003 for the low ones. While these values agree quite closely, yet they differ an appreciable amount from the means of all of the 219 anomalies in the whole country.

The depth which seems to give the smallest mean values for the two groups is 127.9 km. The mean for the high stations in mountainous regions for this depth is $+0.001$ and for low stations it is -0.001 .

The data given in the table on pages 107 to 110, which show the relation between the anomalies and the topography indicate that the depths 42.6 and 184.6 km. are not so near the truth as are intermediate values. They also seem to indicate that the value is probably over 100 km. It is realized by the author that this conclusion is contrary to that arrived at from the determination of the most probable depth from the 216 stations by the method of least squares (see p. 123), which is 60 km. when the flattening, $1/298.2$, is held fixed, or 70.9 km. when the flattening also is determined by the solution. It is believed that the portion of the anomalies at coast stations due to the presence of the Cenozoic geologic formation with densities less than normal had a considerable part in making the depth from all the 216 stations as low as 60 km.

GRAPHIC DETERMINATION OF THE MOST PROBABLE DEPTH OF COMPENSATION.

According to the theory of probabilities the most probable depth of compensation is that one for which the sum of the squares of the residuals or anomalies is a minimum. The residuals are of course assumed to be due only to accidental errors, and hence are as apt to be positive as negative. The values in the table on pages 103-105, in the columns headed $g - (g_0 + 12)$, $g - (g_0 + 11)$, etc., were used in obtaining the sum of the squares of the anomalies for each of the depths.

The sum of the squares is smaller for the smallest two depths of compensation than for the other depths given in the table. The equation of the curve which most nearly fits the sums of the squares for the different depths was derived and its minimum point comes at the depth of 57.1 km.

The sums of the squares for the several depths were also plotted on figure 5, and a curve was drawn through the several points. The lowest point on the curve falls between the depths 42.6 km. and 56.9 km., and the value of the depth at the lowest point is 55.5 km., with an uncertainty from plotting and scaling of about 4 km. This value is only 1.6 km. from the minimum point of the curve as found above from its equation.

A depth for the eastern half of the United States (east of the ninety-eighth meridian) was determined by plotting the sum of the squares on figure 6. The lowest point of the curve falls at a depth of 62 km. The uncertainty of the plotting and scaling is not more than about 4 km.

Likewise a depth was determined for the western half of the United States, as shown in figure 7. Here the minimum point on the curve falls at the depth 48 km., with an uncertainty from plotting and scaling of about 4 km.

An analysis of the table giving the anomalies for the different topographic groups (see pp. 107 to 110) makes it apparent that the results at those stations near but not on the coast and at those in the interior which are not in mountainous regions above the general level, are not more strongly in favor of one depth than any other. This fact causes the influence of the mountain stations above the general level to be less than the plains stations in a determination of the most probable depth of compensation where all stations are involved. This is due to the fact that there are only 20 stations in mountainous regions above the general level, while there are 169 stations in the groups mentioned above.

As the mountain stations are more sensitive to a change in the depth of compensation, it was decided to determine graphically the most probable depth from those stations alone, 56 in number. The resulting curve for these stations is shown in figure 8. The plotted points are the sum of the squares of the residuals or anomalies. These are based on a value of gravity at the equator so derived from all stations in the United States as to make the mean anomaly for the United States zero. The depth determined from this curve is 104 km. which differs materially from the depths obtained from the other three curves (figs. 5, 6 and 7) which were between 48 and 62 km.

An analytical solution of the problem was also made. In this solution the mean flattening was held fixed as in the graphical determination, but the gravity at the equator was determined from the 56 stations themselves instead of from all the stations in the United States. The depth determined was 94.9 km., only 9 km. from the value obtained graphically in spite of the difference in methods and assumptions.

It is interesting that the depths obtained by Hayford from deflections of the vertical in several groups (Nos. 14, 8, 7, and 4) of stations in mountainous regions are 84, 66, 152, and 85 km. The value is 97 if a straight mean for the 4 groups is taken. This agrees well with the values determined analytically from gravity data for mountainous regions, which for the 56 stations is 94.9 km.

The sums of the squares of the anomalies, for the several depths, for the 20 stations in mountainous regions above the general level were plotted on figure 9 and the minimum point of the curve drawn through the plotted points gives the most probable depth as 124 km. This value is only 20 km. different from the most probable depth obtained graphically from the data for all mountain stations.

The values from the analytical determinations of the most probable depths of compensation from all of the stations in the United States, in the eastern half of this country, in the western half, and in the mountainous regions agree well with those from the graphic solutions discussed above. See pages 113 to 131 for the analytical determination of the depth of compensation, the flattening of the earth, and the theoretical value of gravity at the equator.

The stations not in the United States were not used to obtain the most probable depth of compensation, as the necessary data for them were not available.

The author is inclined to favor the depth of 94.9 km. as being nearer the truth than the lower depths, and besides it agrees more nearly with the depth as obtained from deflections of the vertical by Hayford.* We may conclude that the most probable depth of the compensation as derived from the gravity data is 94.9 km.

It is believed that the value, 97 km., obtained by Hayford from deflections of the vertical in mountainous regions is nearer the truth for the average depth of compensation than his values 113.7 and 120 km. If the depth from gravity data and the depth 97 km. mentioned above are given equal weight the mean depth of compensation is 96 km. which the author believes is the best one available from all geodetic data.

This value, of course, must not be considered as having extreme accuracy, for no doubt a depth determined from much more gravity and deflection data would be different. The author believes that future determinations of the depth from more extensive data will fall between 80 and 130 km.

* See Figure of the Earth and Isostasy from Measurements in the United States, and Supplementary Investigation in 1909 of the Figure of the Earth and Isostasy, J. F. Hayford, 1909.

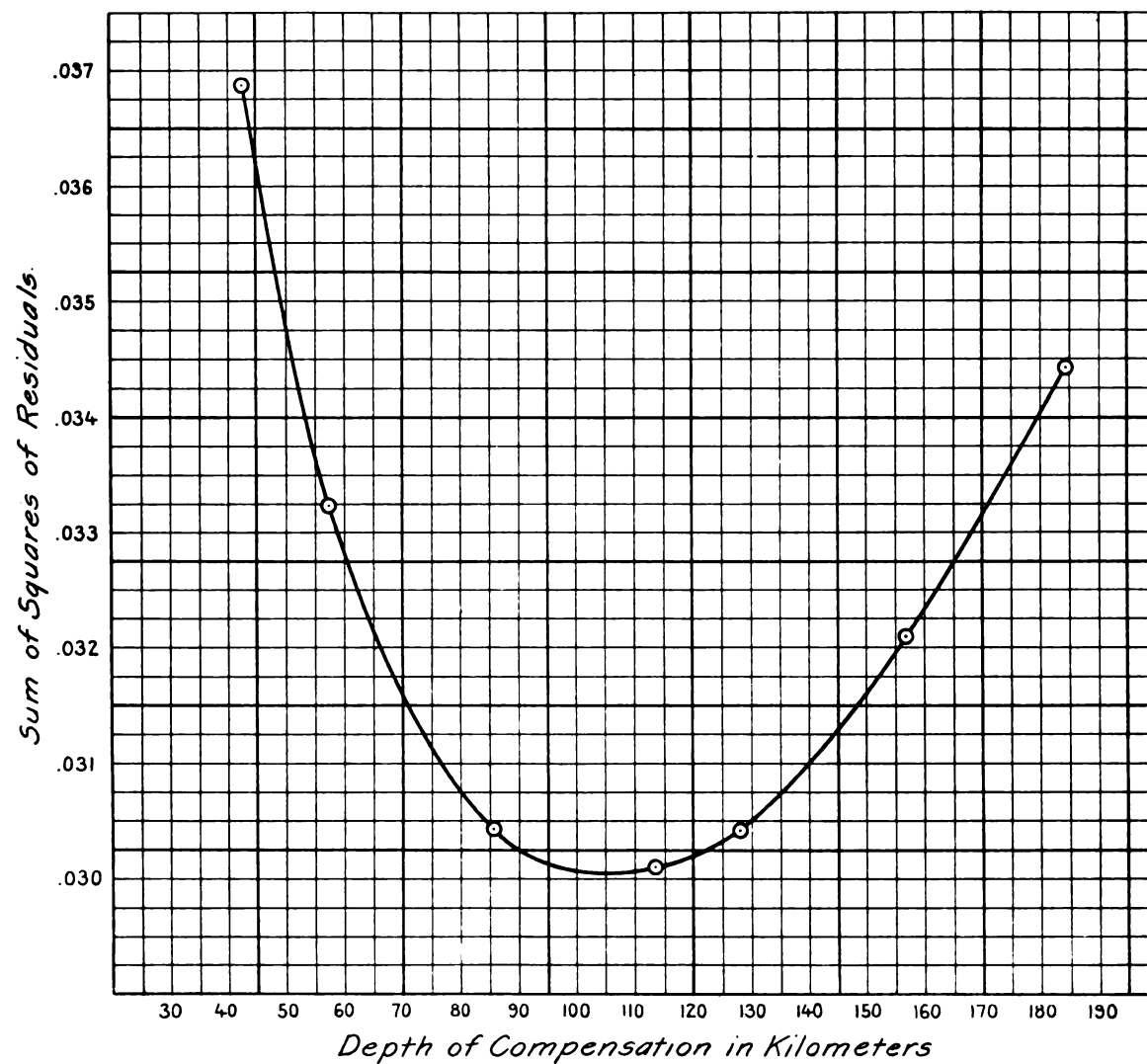


FIG. 8.—GRAPHIC DETERMINATION OF THE MOST PROBABLE DEPTH OF COMPENSATION FROM 56 UNITED STATES STATIONS IN MOUNTAINOUS REGIONS.

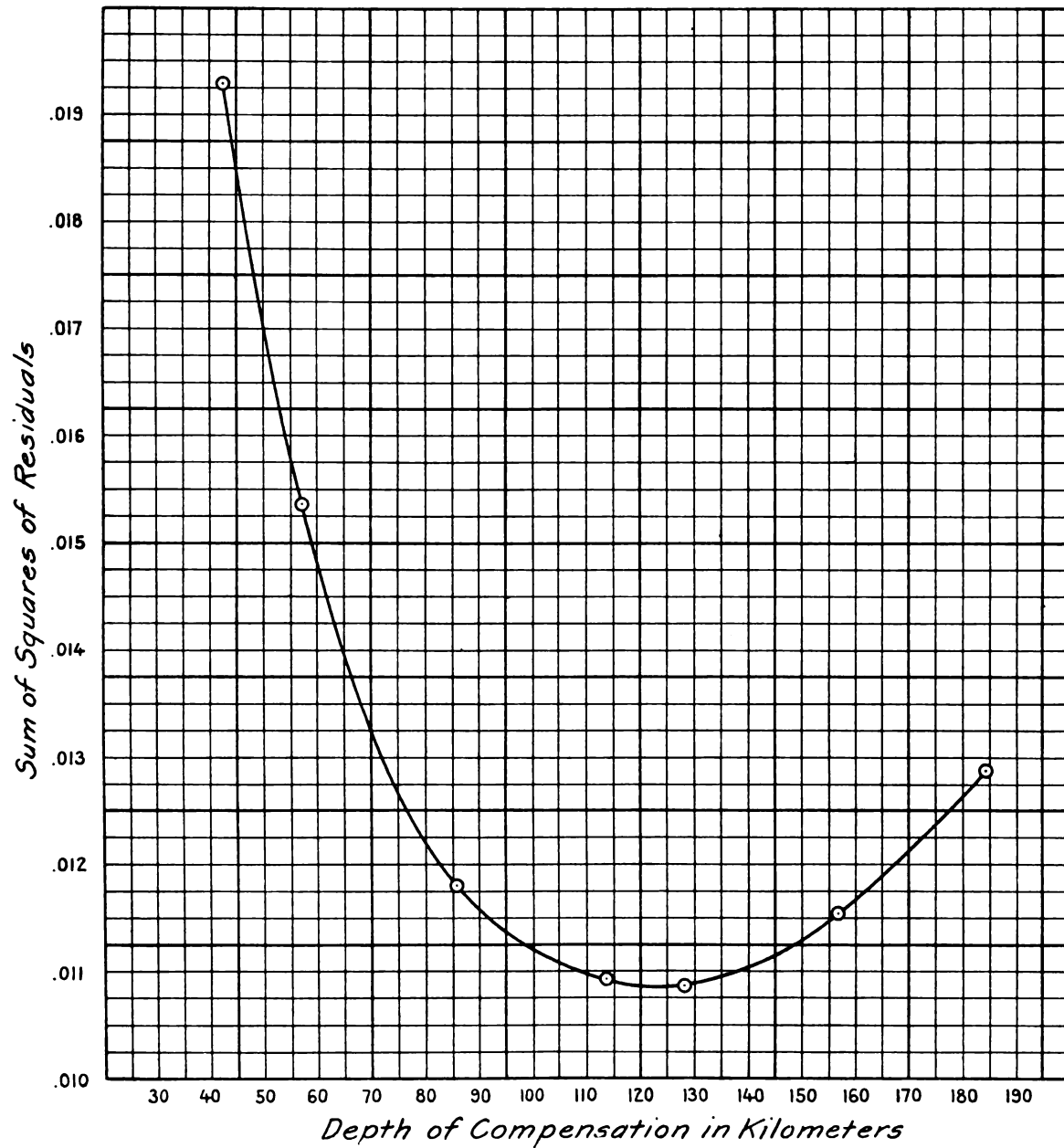


FIG. 9.—GRAPHIC DETERMINATION OF THE MOST PROBABLE DEPTH OF COMPENSATION FROM 20 UNITED STATES STATIONS IN MOUNTAINOUS REGIONS AND ABOVE THE GENERAL LEVEL.

CONSTANTS FOR THE GRAVITY FORMULAS AND THE MOST PROBABLE DEPTHS OF COMPENSATION DERIVED BY ANALYTICAL METHODS FROM GRAVITY DATA.

The method of computing the factors by which the effect of topography and compensation was obtained for various depths of compensation, together with the computed effects of these changes of depth and the anomalies for the several depths are given on pages 97-106. The following analytical solution was made to determine the constants for the gravity formulas and to determine the most probable depths of compensation.

The formula for γ_0 , the theoretical gravity at sea level in geographic latitude ϕ , may be written in the form

$$\gamma_0 = \gamma_e (1 + B \sin^2 \phi - \frac{1}{4} B_4 \sin^2 2\phi) \quad (1)$$

γ_e is the gravity at the equator at sea level, B and B_4 are coefficients, the former determined from gravity observations, the latter found theoretically by Darwin and Wiechert from the assumption that the internal strata of the earth have the same form as if they were completely fluid. Their results, based on different laws of internal density, agree in giving $\frac{1}{4} B_4 = 0.000007$, which will be used throughout the publication.

Helmert's determination of the constants gives for his formula of 1901 on the Potsdam system

$$\gamma_0 = 978.030 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi) \quad (2)$$

If a value be assumed for the equatorial radius of the earth, the ellipticity or flattening of the earth, denoted by f , may be found from the formula,

$$f = \frac{5}{2}m - B - \left(\frac{10}{3}m^2 - \frac{17}{14}mB - \frac{B^2}{21} - \frac{2}{21}B_4 \right) \quad (3)$$

In this formula B and B_4 are the same quantities as in formula (1) and m is the ratio of the centrifugal force of the earth's rotation at the equator to gravity at the equator, or $m = \frac{\omega^2 A}{\gamma_e}$. ω is the angular velocity in radians, expressed in the time unit used in γ_0 . A is the equatorial radius of the earth expressed in the linear unit used in γ_0 . The simple formula $f = \frac{5}{2}m - B$ is known as Clairaut's equation. The above formula is derived from Helmert (*Höhere Geodäsie*, Vol. II, p. 83), and may be termed Clairaut's formula, extended to terms of the second order. The value of $f = \frac{1}{298.3}$ was originally given by Helmert as derived from his formula of 1901. This is based on Bessel's equatorial radius of the earth. A larger value of this quantity such as best represents modern observations gives $f = \frac{1}{298.2}$. The value of A used in deriving the values from the gravity observations treated in this work is 6378388 meters, from Hayford's "Supplementary Investigation in 1909 of the Figure of the Earth and Isostasy," page 60.

Equation (1) may be transformed into a shape somewhat more convenient for the purpose in hand, namely,

$$\gamma_0 = G - b \cos 2\phi + d \cos^2 2\phi \quad (4a)$$

The significance of the constants of the new form and the relations between them and those of the old are,

$$G = \text{gravity at latitude } 45^\circ = \gamma_e \left(1 + \frac{B}{2} - \frac{B_4}{4} \right)$$

$$2b = \text{polar gravity minus equatorial gravity} = \gamma_e B$$

$d = \frac{1}{4} \gamma_e B_4$, which to the degree of accuracy involved in the theoretical developments for B_4 may, like B_4 , be considered as constant.

$$\text{Also } \gamma_e = G - b + d \quad (4b)$$

$$\text{And } B = \frac{2b}{G - b + d} \quad (4c)$$

Let the subscript zero affixed to G , B , and b denote those numerical values corresponding to Helmert's formula of 1901, also $G = G_0 + x$ and $b = b_0 + y$ signify the values determined from the observations; x is the correction to gravity at latitude 45° , y is half the correction to the quantity, polar gravity *minus* equatorial gravity.

Then,

$$G_0 = 980.61591 \text{ dynes and } b_0 = 2.59276 \text{ dynes}$$

With these Helmert values, equation (4) becomes

$$\gamma_0 = 980.61591 - 2.59276 \cos 2 \phi + 0.00685 \cos^2 2 \phi \quad (5)$$

or with the corrections applied

$$\gamma_0 = 980.61591 + x - (2.59276 + y) \cos 2 \phi + 0.00685 \cos^2 2 \phi \quad (6a)$$

Let g be the observed value of gravity and g_c' the value of gravity computed from (2) or its equivalent (5), including corrections for elevation, topography, and compensation for a fixed depth.

Let $n' = g - g_c'$ the gravity anomaly corresponding to formula (2) or (5). The value of gravity computed from the corrected formula is $g_c' + x - y \cos 2 \phi$

An observation of the general form is

Observed value *minus* computed value = residual (v)

whence

$$\left. \begin{aligned} g - (g_c' + x - y \cos 2 \phi) &= v \\ x - y \cos 2 \phi - n' &= -v \end{aligned} \right\} \quad (6b)$$

This is the form of an observation equation for a particular gravity station if the depth of compensation be considered fixed.

If the assumed depth (t) be considered subject to a correction (z), then n' depends on z . To put the equation in linear form, let c be the rate of change with regard to depth of the total correction for topography and compensation of the station in question or $c = \frac{\partial g_c}{\partial t}$ since it is only through this correction for topography and compensation that g_c is affected by a change in t . Then if g_c be the computed gravity at a depth $t + z$ sufficiently near to the assumed depth t

$$g_c = g_c' + cz$$

and replacing g_c' in (6b) by this value of g_c there results

$$x - y \cos 2 \phi + cz - n' = -v \quad (7)$$

which is the form of observation equation when a corrected depth of compensation is to be determined.

These observation equations are shown in the following table. Further explanations follow immediately after the table.

Observation equations for obtaining corrections to the coefficients of the gravity formula and to the depth of compensation.

Station number	Double latitude 2φ	Coefficient of—			Constant term for solution number—							
		<i>x</i>	<i>y</i>	<i>z</i>	1	2	3	4	5	6	7	8
17 In.....	37 47.5	+1	—0.790									—6.3
18 In.....	40 58.2	+1	— .755									— .6
5 In a.....	41 51.7	+1	— .745									—2.7
39 In a.....	42 00.0	+1	— .743									—2.0
88 In.....	42 27.9	+1	— .738									+ .2
26 In a.....	42 36.7	+1	— .736									—3.2
4 In.....	42 43.0	+1	— .735									+ .3
8 In a.....	42 56.3	+1	— .732									—3.1
50 In a.....	43 39.0	+1	— .724									—4.7
9 In a.....	43 48.3	+1	— .722									—3.9
13 In a.....	44 07.8	+1	— .718									—1.4
98 In.....	44 11.0	+1	— .717									—3.7
99 In a.....	44 23.0	+1	— .715									—2.4
72 In a.....	44 26.7	+1	— .714									— .5
73 In a.....	44 47.3	+1	— .710									+1.9
65 In a.....	45 06.3	+1	— .706									+1.4
37 In a.....	45 30.0	+1	— .701									—2.1
84 In a.....	45 33.4	+1	— .700									— .9
43 In a.....	46 17.8	+1	— .691									—3.1
106 In a.....	46 22.0	+1	— .690									+1.0
12 In a.....	46 31.9	+1	— .688									—2.2
91 In.....	46 46.2	+1	— .685									—3.1
107 In a.....	47 03.2	+1	— .681									—3.0
20 In a.....	47 39.8	+1	— .673									— .4
48 In a.....	47 40.8	+1	— .673									— .8
97 In a.....	47 43.6	+1	— .673									—1.1
19 In a.....	48 04.2	+1	— .668									—2.5
45 In a.....	48 14.4	+1	— .666									—4.0
14 In a.....	48 21.4	+1	— .664									—2.6
16 In a.....	48 25.3	+1	— .664									— .5
59 In a.....	48 31.3	+1	— .662									+ .3
41 In a.....	49 03.9	+1	— .655									— .2
1.....	49 07.2	+1	— .654	+0.75	—2.6	—1.3	—4.8	—2.6		—1.3		—1.3
31 In a.....	49 17.6	+1	— .652									—2.0
55 In a.....	49 23.0	+1	— .651									+ .1
29 In.....	49 35.4	+1	— .648									— .3
96 In a.....	49 54.7	+1	— .644									— .9
52 In a.....	50 04.9	+1	— .642									—3.9
67 In a.....	50 34.1	+1	— .635									+ .5
70 In.....	50 45.8	+1	— .633									+2.5
103 In a.....	50 51.7	+1	— .631									—2.9
3 In.....	50 51.8	+1	— .631									— .9
42 In a.....	50 54.1	+1	— .631									—1.5
157.....	50 56.8	+1	— .630	+ .70	+1.5	+2.8	— .1	+1.5		+2.8		+2.8
6 In a.....	51 08.3	+1	— .627									+2.8
15 In a.....	51 09.4	+1	— .627									+1.4
8.....	52 09.4	+1	— .614	+ .37	—4.1	—3.5	—5.0	—4.1		—3.5		—3.5
78 In a.....	52 14.2	+1	— .612									+4.2
33 In a.....	52 27.9	+1	— .609									+ .7
60 In a.....	52 35.5	+1	— .608									+5.7
40 In a.....	53 02.5	+1	— .601									+2.0
101 In a.....	53 23.6	+1	— .596									+3.9
24 In a.....	53 24.0	+1	— .596									+ .5
2.....	53 25.6	+1	— .596	+ .63	—3.8	—2.6	—5.7	—3.8		—2.6		—2.6
32 In a.....	53 29.9	+1	— .595									+7.0
3 a.....	53 52.4	+1	— .590	+ .53	—2.8	—1.8	—3.8	—2.8		—1.8		—1.8
96 In a.....	54 12.2	+1	— .585									—5.4
1 In a.....	54 20.7	+1	— .583									—1.7
77 In a.....	54 56.8	+1	— .574									—1.5
158 a.....	55 00.4	+1	— .573	+ .53	— .1	+ .9	—1.4	— .1		+ .9		+ .9
9.....	55 01.0	+1	— .573	— .09	+1.2	+1.2	+ .9		+1.2		+1.2	+1.2
85 In a.....	55 13.7	+1	— .570									—1.1
2 In a.....	55 47.1	+1	— .562									+ .6
51 In a.....	56 28.6	+1	— .552									+1.9
38 In.....	56 33.1	+1	— .551									—3.8
30 In a.....	57 06.1	+1	— .543									— .5
159.....	57 13.4	+1	— .541	+ .56	—1.8	— .7	—3.0	—1.8		— .7		— .7
160.....	57 37.2	+1	— .536	+ .45	— .3	+ .6	—1.5	— .3		+ .6		+ .6
161.....	58 16.6	+1	— .526	+ .41	+ .5	+1.3	— .3	+ .5		+1.3		+1.3
7.....	58 36.4	+1	— .521	+ .20	— .2	+ .1	— .6	— .2		+ .1		+ .1
44 In.....	59 01.8	+1	— .515									+ .7
100 In a.....	59 05.5	+1	— .514									+5.8
4.....	59 27.0	+1	— .508	+ .39	—1.5	— .8	—2.3	—1.5		— .8		— .8
93 In a.....	59 44.7	+1	— .504									+4.4
5.....	59 54.0	+1	— .502	+ .34	— .1	+ .5	— .8	— .1		+ .5		+ .5

a This station is used only with near-by stations to give a single observation equation. See table of groups on p. 119.

Observation equations for obtaining corrections to the coefficients of the gravity formula and to the depth of compensation—Con.

Station number	Double latitude 2 ϕ	Coefficient of—			Constant term for solution number—							
		x	y	z	1	2	3	4	5	6	7	8
62.....	60 02.6	+1	-.499	+0.39	-4.6	-3.9	-5.2		-4.6		-3.9	-3.9
87 In a.....	60 24.5	+1	-.494									
10 a.....	60 33.0	+1	-.492	+ .11	-.2			-0.2		0.0		
11 a.....	60 34.4	+1	-.491	+ .11								
22 In a.....	60 39.0	+1	-.490									
98.....	60 43.0	+1	-.489	+ .85	-4.5	-2.9	-6.2		-4.5		-2.9	-2.9
89 In a.....	60 48.4	+1	-.488									
164.....	60 49.0	+1	-.488	+ .31	-.1	+ .6	-.8	-.1		+ .6		+ .6
75 In a.....	60 55.2	+1	-.486									
71 In.....	61 19.6	+1	-.480									
92.....	61 20.4	+1	-.480	+ .41	-2.6	-1.8	-3.5	-2.6		-1.8		-1.8
93 a.....	61 38.4	+1	-.475	+ .28	+3.1	+3.6	+1.8	+3.1		+3.6		+3.6
144.....	62 37.2	+1	-.460	+ .17	-.5							
64.....	62 42.6	+1	-.458	+ .67	+2.9	+4.2			+2.9		+4.2	+4.2
66 In.....	63 03.2	+1	-.453									
163.....	63 08.6	+1	-.452	+ .33	-1.6	-1.0	-2.1	-1.6		-1.0		-1.0
97.....	63 12.4	+1	-.451	+ .03	+ .3	+ .4	-.4	+ .3		+ .4		+ .4
145 a.....	63 23.0	+1	-.448	+ .30	-2.7	-2.2	-3.3	-2.7		-2.2		-2.2
63.....	63 32.6	+1	-.446	+ .19	-2.0	-1.5	-1.6		-2.0		-1.5	-1.5
173.....	63 38.8	+1	-.444	+ .29	-.2	+ .3	-1.3	-.2		+ .3		+ .3
6.....	64 56.0	+1	-.424	+ .12	-2.7	-2.4	-3.2	-2.7		-2.4		-2.4
61.....	64 56.8	+1	-.423	+ .26	+1.7	+2.1	+1.2		+1.7		+2.1	+2.1
165.....	65 17.0	+1	-.418	+ .45	+ .9	+1.8	+ .1	+ .9		+1.8		+1.8
65.....	65 26.6	+1	-.416	-.13	-1.6	-1.7	-.7		-1.6		-1.7	-1.7
17.....	65 34.4	+1	-.414	+ .38	+ .5	+1.3	-.3	+ .5		+1.3		+1.3
162 a.....	65 39.6	+1	-.412	+ .25	-3.2	-2.7	-3.4	-3.2		-2.7		-2.7
94.....	66 15.2	+1	-.403	+ .06	+ .7	+ .9	+ .1	+ .7		+ .9		+ .9
142.....	66 51.0	+1	-.393	-.06	-1.9	-1.9	-2.0	-1.9		-1.9		-1.9
174.....	67 01.6	+1	-.390	+ .31	+1.9	+2.5	+1.4	+1.9		+2.5		+2.5
167.....	67 13.0	+1	-.387	+ .07	+ .2	+ .4	-.1	+ .2		+ .4		+ .4
15 a.....	67 30.0	+1	-.383	+ .24	+1.0	+1.5	+ .1	+1.0		+1.5		+1.5
73.....	67 30.6	+1	-.383	+ .07	-1.4	-1.3	-1.2	-1.4		-1.3		-1.3
66.....	67 46.8	+1	-.378	+ .19	+3.8	+4.2	+4.2	+3.8		+4.2		+4.2
16.....	67 49.6	+1	-.377	+ .13	-2.7	-2.3	-3.5	-2.7		-2.3		-2.3
149.....	68 28.4	+1	-.367	+ .55	+1.3	+2.3		+1.3		+2.3		+2.3
99.....	68 46.4	+1	-.362	+ .31	+ .2	+ .8	-.3		+ .2		+ .8	+ .8
143 a.....	69 00.2	+1	-.358	+ .07	-2.8	-2.6	-3.0	-2.8		-2.6		-2.6
96 a.....	69 10.4	+1	-.356	+ .16	+4.1	+4.4	+2.9	+4.1		+4.4		+4.4
150.....	69 24.0	+1	-.352	+ .28	-1.6	-1.0	-2.3	-1.6		-1.0		-1.0
18.....	69 26.2	+1	-.351	+ .85	-.3	+1.3	-2.3	-.3		+1.3		+1.3
166 a.....	69 27.6	+1	-.351	+ .27	+1.0	+1.5	+1.2	+1.0		+1.5		+1.5
13 a.....	69 30.0	+1	-.350	-.06	-3.7	-3.8	-3.9	-3.7		-3.8		-3.8
12.....	69 52.4	+1	-.344	-.02	+1.8	+1.9	+1.8	+1.8		+1.9		+1.9
168.....	70 17.6	+1	-.337	+ .08	-2.2	-2.1	-2.3	-2.2		-2.1		-2.1
153.....	70 18.8	+1	-.337	+ .37	+ .9	+1.5	+1.3	+ .9		+1.5		+1.5
72.....	70 25.6	+1	-.335	+ .19	-4.4	-4.0	-4.7		-4.4		-4.0	-4.0
151 a.....	70 27.6	+1	-.334	+ .29	-4.0	-3.3	-4.8	-4.0		-3.3		-3.3
141 a.....	70 46.6	+1	-.329	-.05	+ .8	+ .8	+1.5	+ .8		+ .8		+ .8
70.....	71 03.6	+1	-.325	+ .76	-1.0	+ .5	-.9		-1.0		+ .5	+ .5
71.....	71 11.6	+1	-.322	+ .82	-2.7	-1.1	-2.8		-2.7		-1.1	-1.1
152.....	71 11.8	+1	-.322	+ .89	-2.0	-.3	-2.9	-2.0		-.3		-.3
14 a.....	71 13.4	+1	-.322	+ .06	-3.8	-3.4	-4.0	-3.8		-3.4		-3.4
148.....	71 13.6	+1	-.322	+ .44	+ .1	+1.0	-.9	+ .1		+1.0		+1.0
155 a.....	71 55.4	+1	-.310	+ .25	+ .8	+1.3	+1.4	+ .8		+1.3		+1.3
91.....	72 00.4	+1	-.309	+ .23	-4.9	-4.4	-5.8	-4.9		-4.4		-4.4
68 a.....	72 07.8	+1	-.307	+ .73	-2.3	-.9	-4.3		-2.3		-.9	-.9
99 a.....	72 10.6	+1	-.306	+ .56	-1.0	+ .2	+9.8		-1.0		+ .2	+ .2
154 a.....	72 12.2	+1	-.306	+ .43	+2.3	+3.0	+1.8	+2.3		+3.0		+3.0
102 a.....	72 12.4	+1	-.306	+1.15	-3.3	-1.2	-14.2	-3.3		-1.2		-1.2
101 a.....	72 17.0	+1	-.304	+1.10	+ .1	+2.1	-3.2	+ .1		+2.1		+2.1
169.....	72 51.8	+1	-.295	+ .41	-5.6	-4.8	-6.3	-5.6		-4.8		-4.8
156 a.....	72 58.6	+1	-.293	+ .11	-2.3	-2.1	-1.9	-2.3		-2.1		-2.1
85.....	73 11.0	+1	-.289	+ .58	-.4	+ .7	-.5	-.4		+ .7		+ .7
147 a.....	73 20.4	+1	-.287	+ .30	-2.7	-2.1	-3.6	-2.7		-2.1		-2.1
100.....	73 21.4	+1	-.286	+ .08	+ .6	+ .9	+1.0		+ .6		+ .9	+ .9
90.....	73 41.0	+1	-.281	+ .61	+2.8	+4.0	+1.5	+2.8		+4.0		+4.0
170.....	73 43.2	+1	-.280	+ .12	-1.7	-1.4	-2.0	-1.7		-1.4		-1.4
140.....	74 10.8	+1	-.273	+ .12	-2.6	-2.4	-2.5	-2.6		-2.4		-2.4
55 a.....	74 40.8	+1	-.264	+1.15	-2.5	-.5	-12.5		-2.5		-.5	-.5
146 a.....	75 04.4	+1	-.258	+ .22	-1.6	-1.1	-2.1	-1.6		-1.1		-1.1
171.....	75 17.8	+1	-.254	+ .30	+1.5	+2.2	+1.0	+1.5		+2.2		+2.2
176.....	75 21.2	+1	-.253	+ .22	+1.1	+1.6	+2.0	+1.1		+1.6		+1.6
139.....	75 22.2	+1	-.253	+ .23	-2.3	-1.9	-3.1	-2.3		-1.9		-1.9
67.....	75 24.4	+1	-.252	+ .78	-1.0	+ .5	-2.2		-1.0		+ .5	+ .5
175 a.....	75 34.4	+1	-.240	+ .42	+ .8	+1.6	+1.1	+ .8		+1.6		+1.6
54 a.....	75 35.0	+1	-.249	+ .89	-.1	+1.5	-3.0		-.1		+1.5	+1.5
172 a.....	75 38.2	+1	-.248	+ .59	+1.6	+2.6	+2.9	+1.6		+2.6		+2.6
215.....	75 57.6	+1	-.243	+ .43	+1.2	+2.1	+ .2	+1.2		+2.1		+2.1

* This station is used only with near-by stations to give a single observation equation. See table of groups on p. 119.

Observation equations for obtaining corrections to the coefficients of the gravity formula and to the depth of compensation—Con.

Station number	Double latitude 2ϕ	Coefficient of—			Constant term for solution number—							
		x	y	z	1	2	3	4	5	6	7	8
19.....	76 04.0	+1	-0.241	+0.18	+0.1	+0.5	+0.3	+0.1		+0.5		+0.5
216.....	76 36.2	+1	-.232	+ .20	-1.7	-1.3	-1.7	-1.7		-1.3		-1.3
104 a.....	76 41.8	+1	-.230	+ .03	+1.4	+1.6	+2.6	+1.4		+1.6		+1.6
25 M.....	76 54.6	+1	-.236									+6.6
45.....	77 05.2	+1	-.223	+ .90	-4.8	-2.8	-2.7		-4.8		-2.8	-2.8
38.....	77 16.0	+1	-.220	-.03	-.3	-.3	-.4	-.3		-.3		-.3
40.....	77 27.4	+1	-.217	-.02	-2.2	-2.2	-1.6		-2.2		-2.2	-2.2
214 a.....	77 35.4	+1	-.215	+ .21	-4.8	-4.4	-5.5	-4.8		-4.4		-4.4
213 a.....	77 38.0	+1	-.214	+ .20	-2.6	-2.1	-2.8	-2.6		-2.1		-2.1
43 a.....	77 40.6	+1	-.213	+1.61	-5.7	-2.9	-21.6		-5.7		-2.9	-2.9
42 a.....	77 41.4	+1	-.213	+ .66	-1.4	-1	+ .6		-1.4		-1	-1
21 a.....	77 46.4	+1	-.212	+ .13	-4.8	-4.5	-4.9	-4.8		-4.5		-4.5
22 a.....	77 46.6	+1	-.212	+ .13	-5.0	-4.7	-5.0	-5.0		-4.7		-4.7
41.....	77 49.4	+1	-.211	+ .25	-.2	+ .4	+ .4		-.2		+ .4	+ .4
84 a.....	77 52.6	+1	-.210	+ .13	-4.9	-4.5	-5.7	-4.9		-4.5		-4.5
47 a.....	77 58.8	+1	-.208	-.34	+1.6	+1.3	+5.6		+1.6		+1.3	+1.3
46.....	78 08.4	+1	-.206	-.06	-3.4	-3.2	+1.9		-3.4		-3.2	-3.2
212 a.....	78 09.8	+1	-.205	+ .23	-5.9	-5.4	-6.7	-5.9		-5.4		-5.4
39.....	78 11.6	+1	-.205	-.05	+ .8	+ .8	+ .9	+ .8		+ .8		+ .8
209 a.....	78 12.6	+1	-.204	+ .23	-4.7	-4.2	-4.9	-4.7		-4.2		-4.2
34.....	78 16.6	+1	-.203	+ .03	+ .9	+1.1	+ .9	+ .9		+1.1		+1.1
217.....	78 19.4	+1	-.202	+ .28	-.5	+ .2	-1.1	-.5		+ .2		+ .2
116.....	78 29.8	+1	-.199	+1.10	-.8	+1.3	-1.7		-.8		+1.3	+1.3
135 a.....	78 32.0	+1	-.199	+ .13	+1.3	+1.6	+2.2	+1.3		+1.6		+1.6
23 a.....	78 35.6	+1	-.198	+ .20	-2	-1.3	-3	-.2		+ .3		+ .3
114.....	78 39.2	+1	-.197	+1.75	-1.2	+2.0	-3.7		-1.2		+2.0	+2.0
125 a.....	78 43.8	+1	-.195	+ .42	+ .7	+1.5	-3	+ .7		+1.5		+1.5
20.....	78 50.0	+1	-.194	+ .82	-3.3	-1.8	-5.9	-3.3		-1.8		-1.8
35.....	78 57.4	+1	-.192	-.01	-.0	+1.1	-1.0	-.0		+1.1		+1.1
219 a.....	79 17.0	+1	-.186	+ .27	+3.5	+4.1	+3.5	+3.5		+4.1		+4.1
44 a.....	79 21.2	+1	-.185	+ .07	+ .6	+ .8	+2.3		+ .6		+ .8	+ .8
137.....	79 31.8	+1	-.182	+ .17	-1.2	-1.2	-1.2	-1.2		-.9		-.9
139.....	79 35.4	+1	-.181	+ .03	+ .7	+ .8	+ .3	+ .7		+ .8		+ .8
48 a.....	79 41.6	+1	-.179	+1.00	-3.2	-1.2	-3.6	-3.2		-3.0		-3.0
24 a.....	79 54.2	+1	-.175	+ .19	-3.5	-3.0	-3.9	-3.5		-3.0		-3.0
136.....	79 55.6	+1	-.175	+ .12	+ .1	+ .4	+ .3	+ .1		+ .4		+ .4
207 a.....	80 08.0	+1	-.171	+ .20	+1.6	+2.1	+2.4	+1.6		+2.1		+2.1
210 a.....	80 32.0	+1	-.164	+ .22	+1.6	+2.1	+1.9	+1.6		+2.1		+2.1
25 a.....	80 42.0	+1	-.162	+ .19	+ .6	+1.1	-.2	+ .6		+1.1		+1.1
211 a.....	80 54.8	+1	-.158	+ .22	+1.1	+1.5	+1.5	+1.1		+1.5		+1.5
26 a.....	81 28.0	+1	-.148	+ .23	-3.8	-3.2	-4.0	-3.8		-3.2		-3.2
29 a.....	81 29.2	+1	-.148	+ .13	-2	-.0	-.7	-.2		-.0		-.0
40.....	81 32.2	+1	-.147	+ .06	-2.1	-1.8	+2.3		-2.1		-1.8	-1.8
105.....	81 35.8	+1	-.146	+ .30	+ .6	+1.3	+ .3	+ .6		+1.3		+1.3
27 a.....	81 37.0	+1	-.146	+ .24	-3.6	-3.0	-4.1	-3.6		-3.0		-3.0
130.....	81 62.0	+1	-.141	+ .41	+ .5	+1.4	-.6	+ .5		+1.4		+1.4
115.....	81 56.8	+1	-.140	+ .13	-.4	+ .1	+ .5		-.4		+ .1	+ .1
120.....	82 12.8	+1	-.135	+ .14	-.2	-.0	+ .3	-.2		-.0		-.0
83.....	82 14.8	+1	-.135	+ .09	-.5	-.2	-.4		-.5		-.2	-.2
81.....	82 36.6	+1	-.129	+1.15	-2.1	+ .2	-1.3		-2.1		+ .2	+ .2
114.....	82 44.8	+1	-.126	+ .40	+1.6	+2.5	+2.2	+1.6		+2.5		+2.5
31.....	83 00.8	+1	-.122	+ .08	-.7	-.5	-.5	-.7		-.5		-.5
82.....	83 10.2	+1	-.119	+ .44	-3.1	-2.1	-2.0		-3.1		-2.1	-2.1
122.....	83 15.4	+1	-.117	+ .12	-2.2	-1.9	-3.0	-2.2		-1.9		-1.9
127.....	83 21.4	+1	-.116	+ .50	-.4	+ .6	-1.8	-.4		+ .6		+ .6
36.....	83 34.8	+1	-.112	-.10	-.1	-.1	-.8	-.1		-.1		-.1
37 M.....	83 47.0	+1	-.108									-5.9
133 a.....	84 07.4	+1	-.102	+ .44	+1.3	+2.2	+1.8	+1.3		+2.2		+2.2
134 b.....	84 15.6	+1	-.100	+ .07	+1.7	+1.9	+1.8	+1.7		+1.9		+1.9
117.....	84 32.2	+1	-.095	-.11	-4.5	-4.4	-2.8		-4.5		-4.4	-4.4
28 a.....	84 35.0	+1	-.095	+ .38	+ .4	+1.2	-.6	+ .4		+1.2		+1.2
18 C.....	84 38.5	+1	-.093			-2.0	-2.0			-2.0		-2.0
29 a.....	84 43.2	+1	-.092	+ .28	-1.9	-1.3	-2.6	-1.9		-1.3		-1.3
30 a.....	84 45.6	+1	-.091	+ .33	-2.0	-1.3	-2.3	-2.0		-1.3		-1.3
205.....	84 46.0	+1	-.091	-.03	-1.0	-1.0	-1.5	-1.0		-1.0		-1.0
32 a.....	84 54.2	+1	-.089	+ .21	+1.0	+1.5	+1.0	+1.0		+1.5		+1.5
119.....	85 01.6	+1	-.087	-.03	-2.3	-2.3	-2.5	-2.3		-2.3		-2.3
123 a.....	85 18.2	+1	-.082	+ .15	+3.1	+3.5	+4.1	+3.1		+3.5		+3.5
195.....	85 40.0	+1	-.078	+ .34	-3.5	-2.7	+ .1		-3.5		-2.7	-2.7
206.....	85 44.6	+1	-.074	+ .14	-3.0	-2.6	-3.0		-3.0		-2.6	-2.6
121.....	85 56.0	+1	-.071	+ .08	-1.2	-1.0	-1.3	-1.2		-1.0		-1.0
131.....	86 05.4	+1	-.068	+ .35	+1.0	+1.6	+2.3	+1.0		+1.6		+1.6
37.....	86 09.2	+1	-.067	+ .08	-.5	-.3	-.6	-.5		-.3		-.3
17 C a.....	86 17.1	+1	-.065			+ .4	+ .6			+ .4		+ .4
204.....	86 33.6	+1	-.060	+ .17	+1.5	+1.8	+1.1	+1.5		+1.8		+1.8
198 a.....	86 35.4	+1	-.059	+ .07	-6.4	-6.2	-5.0		-6.4		-6.2	-6.2
88 a.....	86 36.8	+1	-.059	+ .10	+ .3	+ .2	+ .4	+ .3		+ .2		+ .2
130 a.....	87 06.0	+1	-.051	+ .14	+2.7	+3.1	+4.3	+2.7		+3.1		+3.1
79.....	87 14.4	+1	-.048	-.34	-1.2	-1.6	+2.6		-1.2		-1.6	-1.6
60.....	87 23.6	+1	-.045	-.07	-.7	-.9	-.3		-.7		-.9	-.9
38 M.....	87 30.4	+1	-.044									-6.8
25 C.....	87 40.2	+1	-.041			-1.9	-3.3			-1.9		-1.9
16 C a.....	87 45.4	+1	-.039			+2.6	+3.0			+2.6		+2.6
132 d.....	87 56.6	+1	-.036	+ .11	+1.4	+1.7	+1.6	+1.4		+1.7		+1.7
197.....	87 57.2	+1	-.036	+ .02	-1.5	-1.4	-1.6	-1.5		-1.4		-1.4

a This station is used only with near-by stations to give a single observation equation. See table of groups on p. 119.

b Station 134 enters by itself only in solutions 1 and 4; as a part of group 6 C, p. 120, in solutions 2, 3, 6, and 8.

c Station 88 enters by itself only in solutions 1 and 4; as a part of group 5 C, p. 120, in solutions 2, 3, 6, and 8.

d Station 132 enters solutions 1 and 4 as a part of group 3; solutions 2, 3, 6, and 8 as a part of group 4 C, p. 120.

Observation equations for obtaining corrections to the coefficients of the gravity formula and to the depth of compensation—Con.

Station number	Double latitude 2 <i>φ</i>	Coefficient of—			Constant term for solution number—							
		<i>z</i>	<i>y</i>	<i>z</i>	1	2	3	4	5	6	7	8
181.....	88 06.4	+1	—0.033	+0.02	—2.5	—2.3	—1.7	—2.5	—3.6	—2.3	—3.8	—2.3
201 ^a	88 08.4	+1	—0.032	—0.17	—3.6	—3.8	—2.5	—4	—3.6	—3.8	—3.8	—3.8
128.....	88 12.6	+1	—0.031	+0.27	+0.2	+0.7	+0.4	+0.2	+0.7	+0.7	+0.7	+0.7
3 C ^a	88 29.2	+1	—0.026	—0.026	—3.4	—2.9	—3.4	—4	—3.4	+0.4	—2.9	+0.4
202.....	88 31.0	+1	—0.025	+0.19	—2.7	—1.4	—4.6	—2.7	—3.4	—1.4	—2.9	—1.4
86 ^a	88 35.0	+1	—0.025	+0.08	—4.5	—4.4	—4.4	—4.5	—4.4	—4.4	—4.4	—4.4
196.....	88 35.6	+1	—0.023	+0.73	—7.3	—6.0	—10.4	—7.3	—7.3	—6.0	—6.0	—6.0
75 ^a	88 42.2	+1	—0.022	—0.19	—1.9	—2.2	—9	—1.9	—1.9	—2.2	—2.2	—2.2
118.....	88 43.8	+1	—0.021	+0.12	+3.2	+3.4	+2.9	+3.2	—1.9	+3.4	—2.2	+3.4
180.....	88 47.2	+1	—0.018	—0.52	—0	+1.0	+0.3	—0	—2.6	+1.0	—0.7	+1.0
40 M.....	88 58.4	+1	—0.018	+0.95	—2.6	—7	—3.5	—3.1	—2.6	+1.0	—0.7	+1.0
129.....	88 59.0	+1	—0.015	+0.07	—3.1	—2.9	—2.5	—3.1	—2.9	+1.0	—0.7	+1.0
52 ^a	89 06.8	+1	—0.012	—0.11	—0.11	+2.1	+1.3	—2.9	—2.9	+1.0	—0.7	+1.0
87 ^b	89 20.2	+1	—0.010	+1.21	—2.9	—6	—4.4	—2.9	—2.9	+1.0	—0.7	+1.0
24 C ^a	89 21.6	+1	—0.009	+1.05	—4.9	—2.9	—6.0	—4.9	—4.9	+1.0	—0.7	+1.0
50 ^a	89 26.6	+1	—0.008	—0.06	—1.0	—4.0	—1.1	—1.0	—4.9	—4.9	—2.9	—2.9
51 ^a	89 28.4	+1	—0.007	+0.18	—4.5	—4.0	—9	—4.5	—4.5	—4.0	—4.0	—4.0
177.....	89 31.6	+1	—0.006	—0.09	—8	—9	—0	—8	—9	—9	—9	—9
109.....	89 36.0	+1	—0.004	+0.01	+1.7	+1.7	+1.8	+1.7	+1.7	+1.7	+1.7	+1.7
85 ^a	89 38.2	+1	—0.002	—0.02	—2.5	—2.5	—2.2	—2.5	—2.5	—2.5	—2.5	—2.5
179.....	89 46.4	+1	—0.001	+0.08	+4.1	+4.2	+3.6	+4.1	+4.1	+4.2	+4.2	+4.2
199.....	89 51.6	+1	—0.001	—0.07	—6.7	—6.7	—6.2	—6.7	—6.7	—6.7	—6.7	—6.7
182 ^a	89 55.6	+1	—0.001	—0.07	—6.7	—6.7	—6.2	—6.7	—6.7	—6.7	—6.7	—6.7
74 ^a	89 57.4	+1	—0.001	—0.07	—6.7	—6.7	—6.2	—6.7	—6.7	—6.7	—6.7	—6.7
187 ^a	90 02.6	+1	+0.001	+0.08	—2.4	—2.3	—2.9	—2.4	—2.4	—2.3	—2.3	—2.3
89.....	90 07.6	+1	+0.002	+0.07	+0.9	+1.2	+1.7	+0.9	+1.2	+1.2	+1.2	+1.2
200.....	90 09.0	+1	+0.003	+0.02	—1.5	—1.4	—1.7	—1.5	—1.4	—1.4	—1.4	—1.4
31.....	90 22.4	+1	+0.007	+0.22	—0.4	—0	—1.0	—0.4	—0	—0	—0	—0
19 C.....	90 32.1	+1	+0.009	—0.08	+2.0	+1.9	+2.6	+2.0	+2.0	+1.9	+1.9	+1.9
15 C.....	90 38.1	+1	+0.011	—0.08	+2.0	+1.9	+2.6	+2.0	+2.0	+1.9	+1.9	+1.9
113.....	90 42.8	+1	+0.012	—0.08	+2.0	+1.9	+2.6	+2.0	+2.0	+1.9	+1.9	+1.9
23 C ^a	90 43.3	+1	+0.013	—0.08	+2.0	+1.9	+2.6	+2.0	+2.0	+1.9	+1.9	+1.9
1 C ^a	90 47.3	+1	+0.014	—0.09	—1.9	—2.0	—1.5	—1.9	—1.9	—2.0	—2.0	—2.0
8 C ^a	90 48.9	+1	+0.014	—0.09	—1.9	—2.0	—1.5	—1.9	—1.9	—2.0	—2.0	—2.0
186.....	90 55.0	+1	+0.016	—0.09	—1.9	—2.0	—1.5	—1.9	—1.9	—2.0	—2.0	—2.0
183 ^a	91 04.8	+1	+0.019	+0.12	+3.8	+4.1	+3.3	+3.8	+4.1	+4.1	+4.1	+4.1
107.....	91 05.2	+1	+0.019	+0.27	—3.7	—3.2	—4.2	—3.7	—3.2	—3.2	—3.2	—3.2
184 ^a	91 08.0	+1	+0.020	+0.05	+1.8	+1.9	+1.7	+1.8	+1.9	+1.9	+1.9	+1.9
7 C ^a	91 33.1	+1	+0.027	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
33 M ^a	91 44.2	+1	+0.030	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
194.....	91 48.0	+1	+0.031	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
35 M ^a	91 52.6	+1	+0.033	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
11 M ^a	91 58.0	+1	+0.034	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
36 M ^a	91 59.0	+1	+0.035	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
12 M ^a	91 59.2	+1	+0.035	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
13 M ^a	92 03.0	+1	+0.036	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
20 C.....	92 10.1	+1	+0.038	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
57.....	92 10.8	+1	+0.038	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
22 C.....	92 16.7	+1	+0.040	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
26 C.....	92 18.1	+1	+0.040	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
80.....	92 22.6	+1	+0.041	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
30 M ^a	92 25.0	+1	+0.042	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
18 M ^a	92 26.0	+1	+0.042	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
21 C.....	92 27.8	+1	+0.043	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
28 M ^a	92 28.2	+1	+0.043	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
110.....	92 28.4	+1	+0.043	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
32 M ^a	92 29.8	+1	+0.044	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
108.....	92 34.4	+1	+0.045	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
29 M ^a	92 35.2	+1	+0.045	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
188.....	92 36.8	+1	+0.046	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
9 C.....	92 37.4	+1	+0.046	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
34 M ^a	92 38.6	+1	+0.046	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
15 M ^a	92 39.4	+1	+0.046	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
178.....	92 41.6	+1	+0.047	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
185.....	92 42.6	+1	+0.047	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
2 C.....	92 44.9	+1	+0.048	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
14 M ^a	92 45.8	+1	+0.048	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
31 M ^a	92 46.4	+1	+0.048	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
8 M ^a	92 48.2	+1	+0.049	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
193.....	92 48.4	+1	+0.049	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
17 M ^a	92 48.4	+1	+0.049	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
16 M ^a	92 50.4	+1	+0.050	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
7 M ^a	92 52.0	+1	+0.050	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
12 C.....	93 00.9	+1	+0.053	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
1 M ^a	93 03.6	+1	+0.053	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
2 M ^a	93 04.0	+1	+0.054	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
6 C.....	93 25.1	+1	+0.060	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
203.....	93 34.0	+1	+0.062	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9
76.....	93 37.0	+1	+0.063	—0.23	—1.7	—1.9	+0.3	—1.7	—1.7	—1.9	—1.9	—1.9

^a This station is used only with near-by stations to give a single observation equation. See table of groups on p. 119.
^b Station 87 enters solutions 1 and 4 as a part of group 3; solutions 2, 3, 6, and 8 as a part of group 9 C, p. 120.

Observation equations for obtaining corrections to the coefficients of the gravity formula and to the depth of compensation—Con.

Station number	Double latitude 2 ϕ	Coefficient of—			Constant term for solution number—							
		x	y	z	1	2	3	4	5	6	7	8
10 M a.....	94 00.2	+1	+0.070									-3.2
9 M a.....	94 02.8	+1	+ .071									-4.4
112.....	94 06.8	+1	+ .072	-.15	-3.9	-4.1	-2.9		-3.9		-4.1	-4.1
106 b.....	94 29.8	+1	+ .078	.00	+ .4	+ .5	+ .4	+ .4		+ .5		+ .5
218.....	94 31.6	+1	+ .079			-3.9	-5.9			-3.9		-3.9
27 C a.....	94 44.0	+1	+ .083			+ .3	+ 1.3			+ .3		+ .3
10 C.....	95 01.1	+1	+ .087			- .6	- .2			- .6		- .6
28 C.....	95 14.3	+1	+ .091			+1.8	+ 1.8			+1.8		+1.8
111.....	95 24.8	+1	+ .094	+ .62	+ .8	+2.0	+ 6.7		+ .8		+2.0	+2.0
191.....	95 32.4	+1	+ .097	- .09	-1.8	-1.9	-1.3	-1.8		-1.9		-1.9
58.....	95 37.2	+1	+ .098	+ .22	-3.4	-3.1	-3.9	-3.4		-3.1		-3.1
13 C.....	95 40.9	+1	+ .099			-1.2	-2.4			-1.2		-1.2
192.....	96 13.6	+1	+ .108	-.07	-2.5	-2.7	-1.8		-2.5		-2.7	-2.7
5 C.....	96 16.8	+1	+ .109			- .9	- .5			- .9		- .9
78.....	96 32.8	+1	+ .114	-.12	-1.0	-1.0	+ 3.4		-1.0		-1.0	-1.0
189.....	96 40.6	+1	+ .116	-.04	-4.0	-4.0	-3.6		-4.0		-4.0	-4.0
77.....	96 47.6	+1	+ .118	-.14	-3.4	-3.7	-2.0		-3.4		-3.7	-3.7
14 C.....	96 52.0	+1	+ .120			+3.7	+ 5.1			+3.7		+3.7
4 C.....	97 01.8	+1	+ .122			+2.0	+ 3.5			+2.0		+2.0
29 C.....	97 03.1	+1	+ .123			-1.6	-1.4			-1.6		-1.6
190.....	97 49.4	+1	+ .136	.00	-2.5	-2.5	-2.6		-2.5		-2.5	-2.5
59.....	97 56.2	+1	+ .138	-.13	-2.5	-2.7	-1.8	-2.5		-2.7		-2.7
11 C.....	98 07.5	+1	+ .141			+1.4	+ 1.8		+1.4		+1.4	+1.4
42 C.....	98 33.6	+1	+ .149			+ .8	+ 5.4			+ .8		+ .8
30 C.....	99 32.0	+1	+ .166			- .9	-2.7		- .9		- .9	- .9
32 C.....	99 41.8	+1	+ .168			-1.5	-1.3			-1.5		-1.5
40 C.....	99 44.6	+1	+ .169			.0	+12.2			.0		.0
31 C.....	99 48.8	+1	+ .170			+ .1	- .1		+ .1		+ .1	+ .1
34 C.....	100 04.8	+1	+ .175			- .2	.0			- .2		- .2
33 C.....	100 46.9	+1	+ .187			- .3	- .6			- .3		- .3
39 C.....	101 21.4	+1	+ .197			+ .1	+ 7.4			+ .1		+ .1
3 M a.....	101 28.4	+1	+ .199									-2.9
4 M a.....	101 31.4	+1	+ .200									-1.9
38 C a.....	101 59.6	+1	+ .208			+3.5	+11.5			+3.5		+3.5
35 C.....	102 05.4	+1	+ .209			- .4	+ 1.8			- .4		- .4
36 C a.....	102 21.8	+1	+ .214			-1.5	-1.3			-1.5		-1.5
41 C a.....	102 31.5	+1	+ .217			-1.0	+ 5.6			-1.0		-1.0
37 C a.....	102 47.4	+1	+ .221			+ .3	+ 6.3			+ .3		+ .3
5 M a.....	103 36.0	+1	+ .235									-5.3
6 M a.....	103 40.0	+1	+ .236									-5.2

a This station is used only with near-by stations to give a single observation equation. See table of groups below.

b Station 106 enters alone only in solutions 1 and 4; as a part of group 3 C, p. 120, in solutions 2, 3, 6, and 8.

ARRANGEMENT OF GROUPS.

Group number	Including stations	Coefficient of—			Constant term for solution number—							
		x	y	z	1	2	3	4	5	6	7	8
1 In.....	5 In, 26 In.....	+1	-0.740									-3.0
2 In.....	8 In, 39 In, 50 In.....	+1	-.733									-3.8
3 In.....	9 In, 99 In.....	+1	-.718									-3.2
4 In.....	13 In, 84 In.....	+1	-.709									-1.2
5 In.....	65 In, 72 In, 73 In, 106 In.....	+1	-.705									+1.0
6 In.....	12 In, 37 In.....	+1	-.694									-2.2
7 In.....	20 In, 43 In.....	+1	-.682									-1.8
8 In.....	48 In, 69 In, 107 In.....	+1	-.672									-1.2
9 In.....	14 In, 55 In, 97 In.....	+1	-.663									-1.2
10 In.....	31 In, 45 In.....	+1	-.659									-3.0
11 In.....	19 In, 41 In, 96 In.....	+1	-.656									-1.2
12 In.....	16 In, 52 In.....	+1	-.653									-2.2
13 In.....	15 In, 67 In.....	+1	-.631									+1.0
14 In.....	33 In, 42 In, 103 In.....	+1	-.624									-1.2
15 In.....	6 In, 78 In.....	+1	-.620									+3.5
16 In.....	32 In, 60 In.....	+1	-.602									+6.4
17 In.....	40 In, 96 In, 101 In.....	+1	-.594									+ .2
18.....	3, 188.....	+1	-.582	+0.53	-1.4	-0.4	-2.6	-1.4		-0.4		- .4
18 In.....	1 In, 24 In, 35 In, 77 In.....	+1	-.581									-1.0
19 In.....	2 In, 30 In, 51 In.....	+1	-.552									+ .7
20 In.....	87 In, 100 In.....	+1	-.504									+2.4
24.....	10, 11.....	+1	-.492	+ .11	-.1	+ .1	+ .3	- .1		+ .1		+ .1
21 In.....	22 In, 75 In, 89 In, 93 In.....	+1	-.485									+ .7
20.....	93, 145.....	+1	-.462	+ .29	+ .2	+ .7	- .8	+ .2		+ .7		+ .7
17.....	15, 162.....	+1	-.398	+ .24	-1.1	- .6	-1.6	-1.1		- .6		- .6
25.....	13, 143.....	+1	-.354	.00	-3.2	-3.2	-3.4	-3.2		-3.2		-3.2
23.....	96, 141.....	+1	-.342	+ .06	+2.4	+2.6	+2.2	+2.4		+2.6		+2.6
19.....	14, 166.....	+1	-.336	+ .16	-1.4	-1.0	-1.4	-1.4		-1.0		-1.0
16.....	151, 154.....	+1	-.320	+ .36	- .8	- .2	-1.5	- .8		- .2		- .2
31.....	68, 69.....	+1	-.308	+ .64	-1.6	- .4	+2.8		-1.6	-0.4		- .4
14.....	101, 155.....	+1	-.302	+ .33	-2.4	-1.8	-2.4	-2.4		-1.8		-1.8

Observation equations for obtaining corrections to the coefficients of the gravity formula and to the depth of compensation—Con.

ARRANGEMENT OF GROUPS—Continued.

Group number	Including stations	Coefficient of—			Constant term for solution number—							
		<i>z</i>	<i>y</i>	<i>z</i>	1	2	3	4	5	6	7	8
15.....	102, 103, 156.....	+1	−0.297	+0.85	−1.0	+0.6	−4.6	−1.0		+0.6		+0.6
10.....	146, 147.....	+1	−.272	+ .26	−2.2	−1.6	−2.8	−2.2		−1.6		−1.6
33.....	54, 55.....	+1	−.256	+1.02	−1.3	+ .5	−7.8		−1.3		+0.5	+ .5
11.....	172, 175.....	+1	−.248	+ .50	+1.2	+2.1	+2.0	+1.2		+2.1		+2.1
13.....	104, 135.....	+1	−.214	+ .08	+1.4	+1.6	+2.4	+1.4		+1.6		+1.6
9.....	{ 21, 22, 23, 84, 209, 212, 213, 214 }	+1	−.208	+ .20	−3.8	−3.4	−4.2	−3.8		−3.4		−3.4
28.....	42, 43, 44.....	+1	−.204	+ .73	−2.2	−.7	−6.2		−2.2		−.7	−.7
30.....	47, 48.....	+1	−.194	+ .33	−.8	.0	+1.0		−.8		.0	.0
7.....	24, 125.....	+1	−.185	+ .30	−1.4	−.8	−2.1	−1.4		−.8		−.8
8.....	210, 219.....	+1	−.175	+ .24	+2.6	+3.1	+2.7	+2.6		+3.1		+3.1
12.....	207, 211.....	+1	−.164	+ .21	+1.4	+1.8	+2.0	+1.4		+1.8		+1.8
6.....	25, 26, 27.....	+1	−.154	+ .21	−1.6	−1.0	−2.1	−1.6		−1.0		−1.0
5.....	32, 133.....	+1	−.096	+ .32	+1.2	+1.8	+1.4	+1.2		+1.8		+1.8
1.....	28, 29, 30.....	+1	−.093	+ .34	−.8	.0	−1.5	−.8		.0		.0
6C.....	17C, 134.....	+1	−.082			+1.1	+1.2			+1.1		+1.1
4.....	123, 130.....	+1	−.066	+ .14	+2.9	+3.3	+4.2	+2.9		+3.3		+3.3
5C.....	16C, 88.....	+1	−.049			+1.4	+1.7			+1.4		+1.4
27.....	75, 198.....	+1	−.041	+ .40	−6.8	−6.1	−7.7		−6.8		−6.1	−6.1
4C.....	3C, 132.....	+1	−.031			+1.0	+ .6			+1.0		+1.0
3.....	87, 132.....	+1	−.024	+ .09	−.8			−.8				
2.....	85, 86.....	+1	−.016	+ .32	−1.8	−1.2	−2.3	−1.8		−1.2		−1.2
26.....	187, 201.....	+1	−.016	−.04	−3.0	−3.0	−2.7		−3.0		−3.0	−3.0
29.....	50, 51, 52.....	+1	−.011	+1.07	−3.5	−1.4	−4.6		−3.5		−1.4	−1.4
9C.....	1C, 87.....	+1	+ .001			−1.0	−.8			−1.0		−1.0
2C.....	23C, 24C.....	+1	+ .001			+1.0	−.2			+1.0		+1.0
22.....	182, 183.....	+1	+ .009	+ .10	+4.0	+4.2	+3.4	+4.0		+4.2		+4.2
21.....	74, 184.....	+1	+ .010	−.01	−2.4	−2.4	−2.2	−2.4		−2.4		−2.4
1C.....	7C, 8C.....	+1	+ .020			−1.6	−2.1			−1.6		−1.6
5M.....	{ 18M, 28M, 31M, 33M, 34M, 35M }	+1	+ .039									
6M.....	{ 11M, 12M, 13M, 14M, 15M, 16M, 17M, 29M, 30M, 32M, 36M }	+1	+ .044									
1M.....	1M, 2M.....	+1	+ .053									+1.2
4M.....	7M, 8M, 9M, 10M.....	+1	+ .060									−3.0
3C.....	27C, 106.....	+1	+ .080			+ .4	+ .8			+ .4		+ .4
2M.....	3M, 4M.....	+1	+ .199									−2.4
8C.....	38C, 41C.....	+1	+ .212			+1.2	+8.6				+1.2	+1.2
7C.....	36C, 37C.....	+1	+ .218			−.6	+3.0				−.6	−.6
3M.....	5M, 6M.....	+1	+ .236									−5.2

The first column of the table on pages 115–119 contains the number of the station. Numbers without any letters appended refer to the United States stations given in the list on pages 50–52; the numbers followed by the letter “C” refer to the Canadian stations on page 54; the numbers followed by the letters “In” refer to the Indian stations given in the list on page 56; and the numbers followed by the letter “M” refer to the stations in the list on page 57.

The data in the above tables come from pages 50–60 and 103–105. All stations having anomalies numerically greater than 0.070 dyne have been excluded. For convenience the unit of n' , and therefore of the other quantities involved, has been taken as 0.01 dyne. The unit distance in terms of which z is expressed in these equations is 28.4 km.; that is, the interval between the depths at which the various anomalies for stations in the United States are tabulated on pages 103–105. If the correction for topography and compensation be assumed to change uniformly with changing depth of compensation, that is, if $c = \frac{\partial z}{\partial t}$ is constant, then the value of c , with the units adopted, is the difference between the total corrections for topography and compensation for two depths differing 28.4 km., expressed in units of hundredths of a dyne. An examination of the differences in the table on pages 100–102 will show that these are fairly constant, allowance being made for the effect of omitted decimals. When the observation equations were formed, these quantities carried to one more decimal place than is given on pages 100–102 were available. A specimen of such data is given in connection with station 195, Lander, Wyo., on page 99. From the data for this station the following mean rates of change, in the units adopted, are deduced:

From 42.6 km. to 56.9 km.	= 2 (−3.62+3.70) = +0.16
From 56.9 km. to 85.3 km.	= −3.28+3.62 = +0.34
From 85.3 km. to 113.7 km.	= −2.75+3.28 = +0.53
From 113.7 km. to 127.9 km.	= 2 (−2.48+2.75) = +0.54
From 127.9 km. to 156.25 km.	= −1.98+2.48 = +0.50
From 156.25 km. to 184.6 km.	= −1.33+1.98 = +0.65

A preliminary investigation indicated that the depths of compensation in nearly all solutions would fall between 56.9 km. and 85.3 km., or else very little below 56.9 km. The values of c used in the table of observation equations are therefore the mean rates of change between 56.9 km. and 85.3 km. These c 's are to be used only in connection with solutions for which the depth of compensation is determined. In these solutions the constant term, $-n'$, is based on a depth of 56.9 km. In the second solution for mountain stations, in which the resulting depth is 94.9 km., the anomalies for depth 113.7 km. and the corresponding c 's were used. These are not shown in the table of observation equations.

In order not to give too great influence to a small region that might contain many gravity stations, the following arbitrary procedure was adopted. A solitary station having no other station within 1 degree of it, either in latitude or longitude, gave a single observation equation of weight unity. If a number of stations occurred so that their latitudes were all within 1 degree of one another, and likewise their longitudes, these stations were made to constitute a group and the mean of the observation equations of the separate stations of the group was taken as the observation equation of the group, with weight unity. In taking this mean for the group, stations within a radius of 8 miles were treated as a single station by taking their mean, and giving the mean only the weight of a single station in averaging it with the other members of the group. An example of this is group 1, which contains stations 28, 29, and 30, which are, respectively, Worcester, Boston, and Cambridge. The mean of the anomalies at Boston and Cambridge is $+0.013$ dyne and this is given equal weight in combining with the anomaly at Worcester of -0.012 dyne, giving a final mean for the group of 0.000 dyne. In the list of observation equations, stations that are used only as part of a group are designated by a reference mark which refers to a footnote when the details of the grouping require special mention. The latter part of the list of observation equations is made up of the mean equations for the various groups. When the observations were combined into zones of latitude, the mean of a group was given the same weight as a solitary station, the group being assigned to a zone according to the average latitude of its component members.

The normal equations were made up in the usual way. The probable error of z is found in the usual way from the solution of the normal equations. The quantities γ , B , and f are functions of x and y . Their probable errors are found by methods given in standard text books on the method of least squares.* (See note, p. 98.) These methods all require a knowledge of the numerical values of the derivatives of the functions in question with respect to the unknown quantities of the observation equations.

The formulas (partial derivatives), easily obtained from (4b) and (3) on page 113, and from the definitions of x and y near top of page 114, are

$$\left. \begin{aligned} \frac{\partial \gamma}{\partial x} &= +1 \\ \frac{\partial \gamma}{\partial y} &= -1 \\ \frac{\partial \gamma}{\partial z} &= 0 \dagger \end{aligned} \right\} \quad (8)$$

$$\left. \begin{aligned} \frac{\partial B}{\partial x} &= -\frac{B}{\gamma} \\ \frac{\partial B}{\partial y} &= \frac{2+B}{\gamma} \\ \frac{\partial B}{\partial z} &= 0 \end{aligned} \right\} \quad (9)$$

* For example, Wright and Hayford, *Adjustment of Observations*, p. 137, or Helmert, "Die Ausgleichungsrechnung," 2te auflage, p. 180.

† x and y are independent of z , according to assumption, and therefore γ , which depends only on x and y , is also independent of z ; similarly for B and f . As a matter of fact, the redistribution of attracting matter implied in the correction for isostatic compensation will change somewhat the form of the level surfaces and the intensity of gravity. For the earth considered as a whole the change is slight. Prof. de Sitter (in the Koninklijke Akademie van Wetenschappen te Amsterdam, Proceedings of the Section of Sciences, Vol. XVII, pt. 2, p. 1295) makes some approximate mechanical quadratures and concludes that for the geoid as idealized by isostatic compensation to a depth of 114 km. $1/f$ will be 0.14 less than for the actual geoid. The effect on gravity at the equator is to make the idealized gravity greater than the true by less than 0.001 dyne. For smaller changes in depth the effects would be correspondingly less, and the assumptions made are evidently not seriously vitiated.

$$\left. \begin{aligned}
 \frac{\partial m}{\partial x} &= -\frac{m}{\gamma_0} \\
 \frac{\partial m}{\partial y} &= \frac{m}{\gamma_0} \\
 \frac{\partial f}{\partial m} &= \frac{5}{2} - \frac{20}{3}m + \frac{17}{14}B \\
 \frac{\partial f}{\partial B} &= -1 + \frac{17}{14}m + \frac{2}{21}B \\
 \frac{\partial f}{\partial x} &= \frac{\partial f}{\partial m} \frac{\partial m}{\partial x} + \frac{\partial f}{\partial B} \frac{\partial B}{\partial x} \\
 \frac{\partial f}{\partial y} &= \frac{\partial f}{\partial m} \frac{\partial m}{\partial y} + \frac{\partial f}{\partial B} \frac{\partial B}{\partial y} \\
 \frac{\partial f}{\partial z} &= 0
 \end{aligned} \right\} \quad (10)$$

These derivatives are so nearly constant that for the purpose in hand they could be computed once for all with average values of the quantities involved.

It will be found that the flattening depends almost wholly on y , for $\frac{\partial f}{\partial y}$ is about -0.0000203

(in the units used in forming the observation equations) as against $\frac{\partial f}{\partial x} = -0.000000034$. A change of unity (i. e., 0.01 dyne) in the value of x will appear only in the third decimal of $1/f$, so if it is desired to hold the flattening unchanged in the determinations it will be sufficient to make $y=0$, or, if some other flattening be fixed on in advance, in the adjustment the corresponding value of y may be determined without regard to the possible change in x . This was done in solutions 1c, 1d, and some others.

In comparing various gravity formulas, which differ among themselves in every term, the most convenient single number to afford a basis of comparison is the mean value of γ_0 over the unit sphere. The general expression for this is

$$\text{Mean value} = \gamma_0 \left(1 + \frac{B}{3} - \frac{2B^2}{15}\right) \quad (11)$$

In the case of the solutions given here this is equivalent to

$$\text{Mean value} = 979.75485 + x - \frac{1}{2}y \quad (12)$$

x and y being expressed in dynes instead of in units of 0.01 dyne, as in the observation and normal equations. The mean values resulting from the various adjustments are given on page 129.

The set of solutions numbered "1" in the preceding table was derived from all stations situated in the United States proper, except No. 218, North Tamarack, Mich., for which the data were not available in time, and stations 53 and 56 in Seattle, Wash., which were excluded because of their large anomalies. In all these stations the constant terms are for depth 56.9 km. and the z 's are corrections to that depth. In solution 1a each solitary station and each group of stations is given equal weight. The normal equations are

$$173x - 34.572y + 42.17z - 182.3 = 0$$

$$-34.572x + 13.2991y - 11.8632z + 26.6250 = 0$$

$$42.17x - 11.8632y + 26.3941z - 46.181 = 0$$

From these $x = +1.2934$, $y = +1.7989$, $z = +0.4918$, and the formula for γ_0 is

$$\begin{aligned}
 \gamma_0 &= 978.025(1 + 0.005339 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\
 &\quad \pm 5 \qquad \qquad \pm 11
 \end{aligned}$$

The depth of compensation is 70.9 ± 10.0 km. and the reciprocal of the flattening is 301.4 ± 1.0 .

In solution 1b the stations or groups were assigned to seven zones and each station or group was given a weight inversely proportional to the number of stations and groups in the zone. This process must be substituted for the simpler one of using a mean equation for each zone, which would be practically equivalent if no depth of compensation were to be determined, because the c 's, unlike the other coefficients, vary widely within the zone.

The boundaries of the zones are in latitude 31° , 34° , 37° , 40° , 43° , 46° , and 49° , the latter being the northern boundary of the United States. The zones are all three degrees in width, except the southernmost, which extends from station 1 (Key West, Fla.) in latitude $24^\circ 33'.6$ to latitude $31^\circ 00'$. It was widened in order to include a sufficient number of stations to be representative.

The normal equations are:

$$7x - 1.5606y + 1.7424z - 7.5950 = 0$$

$$-1.5606x + 0.6498y - 0.5448z + 1.2431 = 0$$

$$1.7424x - 0.5448y + 1.0503z - 1.8980 = 0$$

From these $x = +1.3574$, $y = +1.7233$, $z = +0.4490$. The formula for γ_0 is

$$\gamma_0 = 978.026(1 + 0.005337 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 5 \qquad \pm 11$$

The depth of compensation is 69.6 ± 10.4 km. and the reciprocal of the flattening 301.3 ± 1.0 .

The flattenings deduced from 1a and 1b are not supported by determinations from other methods, which would indicate that the assumed flattening of $1/298.2$ is more nearly correct. It was therefore decided to hold the flattening at this figure. This may be done with sufficient accuracy by letting $y = 0$.

Using separate stations and groups, we have for solution 1c, by omitting the second equation in 1a and putting $y = 0$ in the others,

$$173x + 42.17z - 182.3 = 0$$

$$42.17x + 26.3941z - 46.181 = 0$$

From these $x = +1.0274$, $z = +0.1082$, and the formula for γ_0 is

$$\gamma_0 = 978.040(1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 1$$

The depth of compensation is 60.0 ± 9.5 km.

This formula is referred to as the Coast and Geodetic Survey formula of 1916 for the United States.

If the anomalies at stations in the United States were due only to erroneous values of the equatorial gravity and of the depth of compensation used in the computation of the theoretical gravity, then this formula would be perhaps the best obtainable from the data at hand. But, as is shown on page 63, under the heading "Relation between the gravity anomalies and the topography," and on page 70, under the heading "Relation between the gravity anomalies and the geologic formation," the prevailing sign of the anomalies at stations on the seacoast and on Cenozoic formations is evidently due in part to some deviation from the normal of the densities in the strata of the upper crust which is systematic in its nature. The depth computed from the anomalies may be, and probably is, greatly influenced by this systematic effect. It is shown in other parts of this volume that a larger depth than 60 km. is probably nearer the truth. The equatorial value of gravity is not affected materially by the negative anomalies which predominate at the stations near the coast and in Cenozoic formation, as they are offset in great part by the anomalies in other formations which tend to be positive. (See pp. 70 to 78.) The anomalies (called the Hayford 1916 anomalies) based on the Coast and Geodetic Survey formula for 1916 for the

United States are shown in the table on pages 103-106 for purposes of comparison with the anomalies by the 1912 formula of the Coast and Geodetic Survey (called the Hayford 1912 anomalies), which is based on the greater depth of compensation, 113.7 km.

From other data a flattening of 1/297 has been determined. To use this flattening in determining x and z (solution 1d), put $y = -0.642$ in the first and third equations of 1a. The resulting equations are:

$$173x + 42.17z - 160.10 = 0$$

$$42.17x + 26.3941z - 38.565 = 0$$

From these $x = +0.9322$, $z = -0.0286$ and the formula for γ_o is

$$\gamma_o = 978.046 (1 + 0.005289 \sin^2 \phi - 0.000007 \sin^2 2\phi) \pm 1$$

and the depth of compensation is 56.1 ± 9.7 km.

In solution 1e the flattening is held at 1/298.2 and the stations are grouped by zones, as in solution 1b.

The normal equations for 1e are:

$$7x + 1.7424z - 7.5950 = 0$$

$$1.7424x + 1.0503z - 1.8980 = 0$$

From these $x = +1.0820$, $z = +0.0122$, and the formula for γ_o is

$$\gamma_o = 978.041 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi) \pm 1$$

The depth of compensation is 57.2 ± 9.8 km.

The solutions numbered 2a and 2b include stations in the United States proper and the Dominion of Canada. No determination of the depth was possible, since no information as to the correction for topography and compensation of the Canadian stations was available for depths other than 113.7 km. In solution 2a each station and each group was given unit weight.

The normal equations for this solution are:^a

$$208x - 31.281y - 96.1 = 0$$

$$-31.281x + 13.808183y + 3.2079 = 0$$

From these $x = +0.6478$, $y = +1.2351$, and the formula for γ_o is

$$\gamma_o = 978.024 (1 + 0.005327 \sin^2 \phi - 0.000007 \sin^2 2\phi) \pm 4 \pm 9$$

The reciprocal of the flattening is 300.4 ± 0.8 .

Solution 2b is the same as 2a, except that zones were used as in 1b, though with somewhat different boundaries for the zones.

The normal equations are:

$$7x - 1.32y - 2.676 = 0$$

$$-1.32x + 0.56230y + 0.060917 = 0$$

From these $x = +0.6493$, $y = +1.4158$, and the formula for γ_o is

$$\gamma_o = 978.022 (1 + 0.005331 \sin^2 \phi - 0.000007 \sin^2 2\phi) \pm 4 \pm 9$$

The reciprocal of the flattening is 300.7 ± 0.8 .

^a In forming these normal equations the data used for the stations in Canada were those first communicated to the Survey. Afterwards revised values were sent, which appear in the table of observation equations. The corrections are too slight to affect the result seriously.

In the solutions numbered 3a and 3b the anomalies are found by the free-air method of reduction (correction for elevation, but not for topography and compensation). The stations are the same as those in solutions 2a and 2b. In solution 3a each station and each group is given unit weight, and the resulting normal equations are:^a

$$\begin{aligned} 208x - 31.281y - 161.1 &= 0 \\ -31.281x + 13.8082y + 52.8456 &= 0 \end{aligned}$$

From these $x = +0.3018$, $y = -3.1435$, and the resulting formula for γ_0 is

$$\gamma_0 = 978.064 (1 + 0.005238 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 5 \qquad \qquad \pm 12$$

The reciprocal of the flattening is 292.6 ± 1.0 .

In solution 3b each zone is given equal weight, the zones being the same as in solution 2b. The normal equations are:

$$\begin{aligned} 7x - 1.320y - 5.563 &= 0 \\ -1.320x + 0.56230y + 1.954694 &= 0 \end{aligned}$$

From these $x = +0.2498$, $y = -2.8899$, and the formula for γ_0 is

$$\gamma_0 = 978.061 (1 + 0.005243 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 7 \qquad \qquad \pm 17$$

The reciprocal of the flattening is 293.0 ± 1.4 .

In order to test the constancy of the depth of compensation in various regions, the stations in the United States lying east of the ninety-eighth meridian were treated separately from those lying west of it. Solutions 4a and 4b are based on those stations east of the ninety-eighth meridian. In solution 4a each station and each group is given unit weight, and a depth of compensation, a value for the flattening, and the equatorial value are determined. The values of $-n'$ are for depth of 56.9 km. The normal equations for 4a are:

$$\begin{aligned} 118x - 26.723y + 26.21z - 80.1 &= 0 \\ -26.723x + 10.265y - 8.167z + 17.691 &= 0 \\ 26.21x - 8.167y + 11.505z - 17.241 &= 0 \end{aligned}$$

From these $x = +0.7100$, $y = +0.0698$, $z = -0.0695$, and the formula for γ_0 is

$$\gamma_0 = 978.036 (1 + 0.005303 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 6 \qquad \qquad \pm 14$$

The depth of compensation is 54.9 ± 16.8 km., and the reciprocal of the flattening is 298.3 ± 1.2 .

In solution 4b the conditions are the same as for 4a except that the flattening is held as $1/298.2$, the value resulting from Helmert's formula of 1901. The normal equations are

$$\begin{aligned} 118x + 26.21z - 80.1 &= 0 \\ 26.21x + 11.505z - 17.241 &= 0 \end{aligned}$$

From these $x = +0.7004$, $z = -0.0970$, the formula for γ_0 is

$$\gamma_0 = 978.037 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 2$$

and the depth of compensation is 54.1 ± 14.9 km.

The solutions numbered 5a and 5b are based on stations in the United States west of the ninety-eighth meridian, treated in a way similar to those used in solutions 4a and 4b. In

^a See footnote on p. 124.

solution 5a each station and each group is given unit weight. The values of $-n'$ are for depth 56.9 km. The normal equations are:

$$\begin{aligned} 55x - 7.849y + 15.96z - 102.2 &= 0 \\ -7.849x + 3.0345y - 3.6967z + 8.9343 &= 0 \\ 15.96x - 3.6967y + 14.8890z - 28.940 &= 0 \end{aligned}$$

From these $x = +2.2099$, $y = +3.2312$, $z = +0.3772$, and the formula for γ_0 is

$$\gamma_0 = 978.020 (1 + 0.005368 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 10 \qquad \qquad \pm 22$$

The depth of compensation is 67.6 ± 12.9 km., and the reciprocal of the flattening is 304.1 ± 2.0 .

In solution 5b the conditions are the same as for 5a except that the flattening is held fixed at $1/298.2$. The equations, giving unit weight to each station and group, are

$$\begin{aligned} 55x + 15.96z - 102.2 &= 0 \\ 15.96x + 14.8890z - 28.940 &= 0 \end{aligned}$$

From these $x = +1.8784$, $z = -0.0698$, and the value of γ_0 is given by

$$\gamma_0 = 978.049 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 2$$

The depth of compensation is 54.9 ± 12.6 km.

The solutions with separate stations in mountainous regions gave greater depths than other solutions for other groups of stations in the United States, and as it is reasonably certain that the single-station method gives a better value of the depth than the group method, it was decided to make solutions for the stations in the United States west of the ninety-eighth meridian without groups; that is, by the separate-station method. In the first of the two solutions, called 5c, the equatorial gravity, the flattening, and the depth of compensation were determined.

The normal equations are

$$\begin{aligned} 64x - 9.092y + 21.92z - 127.1 &= 0 \\ -9.092x + 3.319338y - 4.54995z + 11.2513 &= 0 \\ 21.92x - 4.54995y + 22.6422z - 53.946 &= 0 \end{aligned}$$

From these $x = +2.2016$, $y = +4.1200$, $z = +1.0790$, and γ_0 is given by

$$\gamma_0 = 978.011 (1 + 0.005387 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 19 \qquad \qquad \pm 21$$

The depth of compensation is 87.5 ± 10.6 km. and the reciprocal of the flattening is 305.8 ± 1.9 .

In the solution 5d the flattening was held at $1/298.2$. The normal equations are:

$$\begin{aligned} 64x + 21.92z - 127.1 &= 0 \\ 21.92x + 22.6422z - 53.946 &= 0 \end{aligned}$$

From these $x = +1.7503$, $z = +0.6881$ and γ_0 is given by

$$\gamma_0 = 978.048 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 2$$

The depth of compensation is 76.4 ± 10.8 km.

If the Canadian stations east of the ninety-eighth meridian be joined with those in the United States, no determination of the depth of compensation is possible, since the only depth for which the corrections for topography and isostatic compensation are available for Canadian stations is 113.7 km. In solution 6 this depth is used and each station or group east of the ninety-eighth meridian in Canada or the United States is given unit weight. The normal equations are then *

$$\begin{aligned} 146x - 25.174y - 35.6 &= 0 \\ -25.174x + 10.455634y + 2.5569 &= 0 \end{aligned}$$

* See footnote on p. 124.

From these $x = +0.3448$, $y = +0.5857$, and the formula for γ_0 is

$$\gamma_0 = 978.028 (1 + 0.005314 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 4 \quad \pm 11$$

The reciprocal on the flattening is 299.2 ± 1.0 .

Solution 7 is based on stations in the United States and Canada west of the ninety-eighth meridian. The depth is fixed at 113.7 km. and each station or group is given equal weight. The normal equations are

$$62x - 6.107y - 59.3 = 0 \\ -6.107x + 3.352549y + 0.8568 = 0$$

From these $x = +1.1349$, $y = +1.8118$, and the formula for γ_0 is

$$\gamma_0 = 978.023 (1 + 0.005339 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 8 \quad \pm 17$$

The reciprocal of the flattening is 301.5 ± 1.5 .

The solutions numbered 8a and 8b are based on all available stations in the world between the latitudes of station 179In, Bombay (India) and station 6 M, Scharfenstein (Germany). The only depth of compensation for which data are available is 113.7 km., and this has therefore been held fixed. Stations with an anomaly numerically exceeding 0.070 dyne based on Helmert's formula of 1901 were excluded. It was found that 358 stations could be used. For solution 8a the stations and groups of stations were divided into 11 zones each 3 degrees of latitude in width; the southernmost zone includes Bombay and extends to the twenty-second parallel. The other bounding parallels are the twenty-fifth, twenty-eighth, etc. All stations used in these solutions are in north latitude.

Results for the individual zones.

Zone.	Bounding parallels.	Number of stations or groups.	Mean value of $-\cos 2\phi$	Mean anomaly.	Zone.	Bounding parallels.	Number of stations or groups.	Mean value of $-\cos 2\phi$	Mean anomaly.
				<i>Dynes.</i>					<i>Dynes.</i>
1.....	22	6	-0.748	+0.0212	7.....	37-40	33	-0.218	-0.0014
2.....	22-25	14	-.680	+ .0176	8.....	40-43	27	-.115	+ .0069
3.....	25-28	13	-.609	-.0062	9.....	43-46	41	-.017	+ .0099
4.....	28-31	17	-.510	+ .0048	10.....	46-49	41	+ .074	+ .0108
5.....	31-34	21	-.420	-.0009	11.....	49-52	14	+ .185	+ .0066
6.....	34-37	26	-.323	+ .0026					

There is a total of 252 separate stations and groups of stations. Each zone was given unit weight. The normal equations that follow from these are

$$11x - 3.381y - 7.09 = 0 \\ -3.381x + 2.034353y + 2.57810 = 0$$

From these $x = +0.5213$, $y = -0.4008$, and the formula for γ_0 is

$$\gamma_0 = 978.039 (1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi) \\ \pm 4 \quad \pm 12$$

The reciprocal of the flattening is 297.4 ± 1.0 .

The fact that the mean anomalies for some of the zones are based on comparatively few stations or groups of stations as compared with the other zones suggests that it would be of interest to weight each zone proportionately to the number of stations it contains. This process is (except for probable errors) almost exactly equivalent to that of giving each station and each group unit weight. With weights thus taken, the normal equations for solution 8b, are

$$252x - 52.855y - 149.1 = 0 \\ -52.855x + 28.027y + 23.9 = 0$$

From these $x = +0.6829$, $y = +0.4352$, and the formula for γ_0 is

$$\gamma_0 = 978.032 (1 + 0.005311 \sin^2 \phi - 0.000007 \sin^2 2 \phi) \\ \pm 4 \qquad \qquad \pm 11$$

The reciprocal of the flattening is 298.9 ± 1.0 .

On pages 63-67 is given a list of anomalies at stations in the United States computed from the United States Coast and Geodetic Survey formula of 1916; that is, for solution 1c. This formula with depth 60.0 km. represents the observations somewhat better than the 1912 formula with depth 113.7 km. except for the 20 stations in mountainous regions above the general level, for which the average anomaly with regard to sign is $+0.016$ dyne by the 1916 formula. It is therefore natural to inquire what formula and what depth would fit those stations better. The effect of the change of depth on the computed compensation is large for these stations, so that a depth of compensation would be better determined from them than from an equal number of stations elsewhere. However, it seemed to be illogical to take only the stations above the general level and to exclude other stations in the same regions, perhaps within a few miles. Therefore the 36 stations in mountainous regions below the general level (see p. 108) were likewise included in the adjustment. There is no separate column for the constant terms of this solution in the table of observation equations on pages 115 to 120.

This adjustment was made in two ways. First the groups were broken up, each station being taken by itself, and only the 56 stations in mountainous regions were included. Second, where the stations occurred near together groups were used, just as in other cases. These groups included four stations not in mountainous regions.

When the groups were broken up and each station was given unit weight the normal equations for this solution (called 9a) became:

$$\begin{aligned} 56x - 9.017y + 27.48z - 38.2 &= 0 \\ -9.017x + 2.6091714y - 5.18505z + 1.6404 &= 0 \\ 27.48x - 5.18505y + 18.7226z - 15.279 &= 0 \end{aligned}$$

From these $x = +1.3506$, $y = +3.8278$, $z = -0.1061$. The anomalies and the c 's in this solution are computed for the depth of 113.7 km. and the z is a correction to that depth. The resulting formula for γ_0 is

$$\gamma_0 = 978.005 (1 + 0.005380 \sin^2 \phi - 0.000007 \sin^2 2 \phi) \\ \pm 14 \qquad \qquad \pm 31$$

The reciprocal of the flattening is 305.2 ± 2.9 and the depth of compensation is 110.7 ± 20.3 km.

Solution 9b is based on the same data, but the flattening was held fixed at $1/298.2$. The normal equations for solution 9b are

$$\begin{aligned} 56x + 27.48z - 38.2 &= 0 \\ 27.48x + 18.7226z - 15.279 &= 0 \end{aligned}$$

From these $x = +1.0066$ and $y = -0.6613$. The formula for γ_0 is

$$\gamma_0 = 978.040 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2 \phi) \\ \pm 4$$

The depth of compensation is 94.9 ± 19.7 km.

When the usual groups are taken, the normal equations for the solution (called 9c) are

$$\begin{aligned} 44x - 6.879y + 19.25z - 64.9 &= 0 \\ -6.879x + 2.056157y - 4.23457z + 9.057 &= 0 \\ 19.25x - 4.23457y + 16.2641z - 29.779 &= 0 \end{aligned}$$

From these $x = +1.5433$, $y = +1.6542$, $z = +0.4350$. The anomalies and c 's in this solution

are computed for the depth 56.9 km. and the z is a correction to this depth. The resulting formula for γ_0 is

$$\gamma_0 = 978.029 (1 + 0.005336 \sin^2 \phi - 0.000007 \sin^2 2\phi)$$

The reciprocal of the flattening is 301.2, and the depth of compensation is 69.3 km.

In solution 9d the flattening is held fixed at $1/298.2$ but the remaining conditions are the same as in the solution 9c. The normal equations for solution 9d are

$$\begin{aligned} 44x + 19.25z - 64.9 &= 0 \\ 19.25x + 16.2641z - 29.779 &= 0 \end{aligned}$$

From these $x = +1.3977$, and $z = +0.1766$. The resulting formula for γ_0 is

$$\gamma_0 = 978.044 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi)$$

and the depth of compensation is 61.9 km.

It is evident that the method of grouping high and low stations in forming the equations destroys the peculiar sensitiveness of the high stations to a change in depth. Therefore the values of the depth by the group solution (9c) should not be considered as having a strong weight as compared with the values of the depth by the single-station solution (9b).

The author believes that the depths derived from the single-station solution for mountainous regions are nearer the truth even for the whole United States than any other depth determined from other groups of gravity stations. (See p. 112.) The solutions of separate stations in the western part of the United States give values for the depth of compensation which are greater than for other solutions except those mentioned above. The stations in the West are, in general, either in mountainous regions or on high plains.

The results of the foregoing solutions are summarized in the following table, which also contains some additional items of information, namely, the mean value of gravity and the probable error of an observation of unit weight. Except in the column for the mean value of gravity and in the lines for solutions 9c and 9d the presence of a value for the probable error of a quantity indicates that the quantity in question was determined by the solution itself, and the absence of a value for the probable error indicates that the quantity was fixed in advance.

Constants of the gravity formulas and related quantities as derived from the various solutions.

Solution No.	Equatorial value of gravity.	Coefficient of $\sin^2 \phi$.	Mean value of gravity for the earth.	Reciprocal of flattening.	Depth of compensation.	Probable error of an observation of unit weight.
	<i>Dynes.</i>		<i>Dynes.</i>		<i>Km.</i>	<i>Dynes.</i>
1a.....	978.025 $\pm$ 4.9	0.005339 $\pm$ 11.5	979.762	301.4 $\pm$ 1.0	70.9 $\pm$ 10.0	$\pm$ 0.0133
1b.....	978.026 $\pm$ 4.6	.005337 $\pm$ 10.7	979.763	301.3 $\pm$ 1.0	69.6 $\pm$ 10.4	$\pm$.0027
1c.....	978.040 $\pm$ 1.3	.005302	979.765	298.2	60.0 $\pm$ 9.5	$\pm$.0135
1d.....	978.046 $\pm$ 1.3	.005289	979.766	297.0	56.1 $\pm$ 9.7	$\pm$.0137
1e.....	978.041 $\pm$ 1.3	.005302	979.766	298.2	57.2 $\pm$ 9.8	$\pm$.0027
2a.....	978.024 $\pm$ 3.9	.005327 $\pm$ 9.0	979.757	300.4 $\pm$ 0.8	113.7	$\pm$.0133
2b.....	978.022 $\pm$ 3.7	.005331 $\pm$ 9.2	979.757	300.7 $\pm$ 0.8	113.7	$\pm$.0025
3a.....	978.064 $\pm$ 5.1	.005238 $\pm$ 12.0	979.768	292.6 $\pm$ 1.0		$\pm$.0176
3b.....	978.061 $\pm$ 6.8	.005243 $\pm$ 16.6	979.767	293.0 $\pm$ 1.4		$\pm$.0045
4a.....	978.036 $\pm$ 6.1	.005303 $\pm$ 14.1	979.762	298.3 $\pm$ 1.2	54.9 $\pm$ 16.8	$\pm$.0126
4b.....	978.037 $\pm$ 1.6	.005302	979.762	298.2	54.1 $\pm$ 14.9	$\pm$.0125
5a.....	978.020 $\pm$ 9.7	.005368 $\pm$ 21.6	979.766	304.1 $\pm$ 2.0	67.6 $\pm$ 12.9	$\pm$.0138
5b.....	978.049 $\pm$ 2.3	.005302	979.774	298.2	54.9 $\pm$ 12.6	$\pm$.0142
5c.....	978.011 $\pm$ 9.5	.005387 $\pm$ 21.1	979.763	305.8 $\pm$ 1.9	87.5 $\pm$ 10.6	$\pm$.0141
5d.....	978.048 $\pm$ 2.3	.005302	979.772	298.2	76.4 $\pm$ 10.8	$\pm$.0148
6.....	978.028 $\pm$ 4.5	.005314 $\pm$ 10.8	979.756	299.2 $\pm$ 1.0	113.7	$\pm$.0130
7.....	978.023 $\pm$ 7.6	.005339 $\pm$ 16.8	979.760	301.5 $\pm$ 1.5	113.7	$\pm$.0136
8a.....	978.039 $\pm$ 4.3	.005294 $\pm$ 11.8	979.761	297.4 $\pm$ 1.0	113.7	$\pm$.0057
8b.....	978.032 $\pm$ 4.4	.005311 $\pm$ 10.9	979.760	298.9 $\pm$ 1.0	113.7	$\pm$.0220
9a.....	978.005 $\pm$ 14.4	.005380 $\pm$ 31.2	979.756	305.2 $\pm$ 2.9	110.7 $\pm$ 20.3	$\pm$.0156
9b.....	978.040 $\pm$ 4.0	.005302	979.765	298.2	94.9 $\pm$ 19.7	$\pm$.0158
9c.....	978.029	.005336	979.765	301.2	69.3	
9d.....	978.044	.005302	979.769	298.2	61.9	

* The observation of unit weight is a zone.

STATEMENT CONCERNING THE VARIOUS SOLUTIONS THE RESULTS OF WHICH ARE GIVEN IN THE ABOVE TABLE.

In the solutions in which separate stations and groups of stations were used, each separate station and each group of stations was given unit weight.

In the solutions in which the stations were taken by zones, each zone was given unit weight, except in solution 8b.

UNITED STATES STATIONS, SOLUTIONS 1a TO 1e.

- 1a. Separate stations and groups of stations were used in the determination of equatorial gravity, the flattening and the depth of compensation.
- 1b. Zones were used in the determination of equatorial gravity, the flattening, and the depth of compensation.
- 1c. Separate stations and groups of stations were used and the flattening was held fixed at $1/298.2$ in the determination of equatorial gravity and the depth of compensation.
- 1d. Separate stations and groups of stations were used and the flattening was held fixed at $1/297$ in the determination of equatorial gravity and the depth of compensation.
- 1e. Zones were used and the flattening was held fixed at $1/298.2$ in the determination of equatorial gravity and the depth of compensation.

UNITED STATES AND CANADIAN STATIONS, SOLUTIONS 2a AND 2b.

- 2a. Separate stations and groups of stations were used and the depth was held fixed at 113.7 km. in the determination of equatorial gravity and the flattening.
- 2b. Zones were used and the depth was held fixed at 113.7 km. in the determination of equatorial gravity and the flattening.

UNITED STATES AND CANADIAN STATIONS BY THE FREE-AIR METHOD OF REDUCTION, SOLUTIONS 3a AND 3b.

- 3a. Separate stations and groups of stations were used in the determination of equatorial gravity and the flattening.
- 3b. Zones were used in the determination of equatorial gravity and the flattening.

UNITED STATES STATIONS EAST OF THE NINETY-EIGHTH MERIDIAN, SOLUTIONS 4a AND 4b.

- 4a. Separate stations and groups of stations were used in the determination of equatorial gravity, the flattening, and the depth of compensation.
- 4b. Separate stations and groups of stations were used and the flattening was held fixed at $1/298.2$ in the determination of equatorial gravity and the depth of compensation.

UNITED STATES STATIONS WEST OF THE NINETY-EIGHTH MERIDIAN, SOLUTIONS 5a TO 5d.

- 5a. Separate stations and groups of stations were used in the determination of equatorial gravity, the flattening, and the depth of compensation.
- 5b. Separate stations and groups of stations were used and the flattening was held fixed at $1/298.2$ in the determination of equatorial gravity and the depth of compensation.
- 5c. Separate stations only were used in the determination of equatorial gravity, the flattening, and the depth of compensation.
- 5d. Separate stations only were used and the flattening was held fixed at $1/298.2$ in the determination of equatorial gravity and the depth of compensation.

UNITED STATES AND CANADIAN STATIONS EAST OF THE NINETY-EIGHTH MERIDIAN, SOLUTION 6.

- 6. Separate stations and groups of stations were used and the depth was held fixed at 113.7 km. in the determination of equatorial gravity and the flattening.

UNITED STATES AND CANADIAN STATIONS WEST OF THE NINETY-EIGHTH MERIDIAN, SOLUTION 7.

- 7. Separate stations and groups of stations were used and the depth was held fixed at 113.7 km. in the determination of equatorial gravity and the flattening.

STATIONS IN THE UNITED STATES, CANADA, SWITZERLAND, INDIA, ITALY, GERMANY, AND AUSTRIA, SOLUTIONS 8a AND 8b.

- 8a. Zones were used, the zones having equal weight, and the depth was held fixed at 113.7 km. in the determination of the equatorial gravity and the flattening.
- 8b. Zones were used, the zones weighted according to the aggregate number of stations and groups in a zone, and the depth was held fixed at 113.7 km. in the determination of equatorial gravity and the flattening.

UNITED STATES STATIONS IN MOUNTAINOUS REGIONS, SOLUTIONS 9a TO 9d.

- 9a. Separate stations only were used in the determination of equatorial gravity, the flattening, and the depth of compensation.
- 9b. Separate stations only were used and the flattening was held fixed at $1/298.2$ in the determination of equatorial gravity and the depth of compensation.
- 9c. Separate stations and groups of stations were used in the determination of equatorial gravity, the flattening, and the depth of compensation.
- 9d. Separate stations and groups of stations were used and the flattening was held fixed at $1/298.2$ in the determination of equatorial gravity and the depth of compensation.

For completeness and for comparison with the above formulas for the intensity of gravity there is given here Helmert's most recent formula.^a With probable errors attached it reads:

$$g_0 = 978.052 \left[1 + 0.005285 \sin^2 \phi - 0.000007 \sin^2 2\phi + 0.000018 \cos^2 \phi \cos 2(\lambda + 17^\circ) \right]$$

± 3
 ± 5
 ± 3
 ± 4

in which ϕ , as usual, is the geographic latitude and λ is the longitude from Greenwich, east longitude being positive. The formula corresponds to a spheroid with three unequal axes, the shorter equatorial axis being in longitude 73° east from Greenwich and the longer, which exceeds the shorter by 230 m., in longitude 17° west of Greenwich. The reciprocal of the mean polar flattening is 296.7 ± 0.4 . The mean value of gravity over the sphere is 979.771 dynes. The formula is based upon 410 stations in all parts of the world selected for being neither too near to the coast nor to mountainous regions and upon certain coast stations which were given reduced weight. The coefficient of $\sin^2 2\phi$ is based on theory. (See p. 113.) The coast stations were used in determining all other constants except the first one, which from coast stations alone had the special value of 978.068 dynes. The precise number of coast stations is not given. The formula, when the first coefficient is used as 978.052, represents gravity reduced by the free-air method for stations in the interior and not in mountainous regions. No tests have yet been made to determine how well this formula represents gravity in the United States.

HELMERT'S DEPTH OF COMPENSATION FROM GRAVITY OBSERVATIONS.

Helmert derived a depth of compensation of about 120 km. from data for 51 selected coast stations distributed throughout the earth's surface.^b He used in his determination the differences between the observed values of gravity reduced to sea level by the free-air method and the values at sea level computed by his 1901 formula. The observed values were in general considerably greater than those computed.

The stations were arranged in several groups, each group containing the stations in some special type of topography, and a depth was derived from the data for each group, namely, that depth for which the correction for topography and isostatic compensation would account for the mean observed free-air anomaly of the group. For group 1 it was 107 km., for group 2 it was 124 km., and for groups 3 and 4 together 123 km.; the mean value was 118 km.

If the free-air method of reduction is used, Helmert's formula of 1901 should represent, on the average, gravity at stations in the interior, not in mountainous regions. But for stations in this class in the United States the average anomaly (free air) is $+0.009$ dyne. (See p. 67.) If the equatorial constant were increased to 978.039 to represent this class of stations better, the anomalies of the coast stations would be correspondingly reduced and the depths indicated would be: Group 1, 80 km.; group 2, 89 km.; groups 3 and 4 together, 78 km., with a mean of 83 km. Helmert's 1915 formula indicates that gravity in the United States is slightly below normal, for according to the formula minimum gravity occurs in longitude 107° west, and if allowance were made for this the previous correction of $+0.009$ dyne would be further increased and the resulting depth further diminished. A rough estimate of the effect of using Helmert's 1915 formula may be obtained by noting that according to it

^a Sitzungsberichte der Königlich Preussischen Akademie der Wissenschaften, No. 41 (1915), p. 676, entitled "Neue Formeln für den Verlauf der Schwerkraft im Meeresniveau beim Festlande."

^b Encyclopédie der Mathematischen Wissenschaften Band VI 1B, Heft. 2 Die Schwerkraft und die Massenverteilung der Erde, p. 140.

average gravity over the unit sphere is 0.016 dyne greater than according to his 1901 formula. If the anomalies in each group are diminished by 0.016 dyne, the depths implied are: Group 1, 62 km.; group 2, 64 km.; groups 3 and 4 together, 46 km., making the mean 58 km., which is about the value found by the various solutions for the United States, except the solution from the 56 stations in mountainous regions. This 58 km. by Helmert's method is of course based on anomalies at coast (and probably largely Cenozoic) stations, which, as is indicated in other parts of this volume, are subject to systematic errors due to smaller densities than normal in the upper strata of the earth's crust. While the value of 58 km. agrees well with the depth given for the Coast and Geodetic Survey formula for 1916 for the United States, it should not necessarily be considered as being nearer the truth than the greater depths.

Chapter IX.—SUMMARY.

The group of publications of the Coast and Geodetic Survey dealing with deflections and gravity values shows that isostasy exists in a form nearly perfect in the United States as a whole, also that there is nearly perfect isostasy in areas which form comparatively small percentages of the area of the entire country.

The conclusions which may be drawn from the investigation reported in this volume substantiate to a great extent the conclusions arrived at from previous investigations. This is an important fact, for 70 per cent more gravity stations in the United States were used at this time than in the preceding gravity investigation and many stations in Canada, India, and Europe, for which data were available, were also used.

The depth of compensation was derived from the 216 stations in the United States and was found to be 60 km. When the stations were divided into different groups, other depths were obtained. They agreed in general with the value determined from all of the stations. An exception is in the case of the stations in mountainous regions, 56 in all. The values of the depth of compensation determined from these are 111 km. and 95 km. on two somewhat different assumptions. Owing to the fact that at stations in mountainous regions above the general level the values of gravity are very sensitive to a change in depth, it is believed that the value of the depth determined from the stations in mountainous regions has greater strength than the other values.

The author believes that the best value for the depth of compensation is the mean of the Hayford value^a of 97 km., which was obtained from deflection data at stations in mountainous regions and the value of 95 km. derived from gravity data at stations in mountainous regions. This mean is 96 km. The author believes that future values of the depth of compensation derived from much more extensive data will fall between 80 and 130 km. (See p. 112 and fig. 8.)

For the United States there was found a decided relation between the sign of the Hayford gravity anomalies and the coast. The reason for this is explained in the following paragraphs. There was no relation found between the sign and the size of the Hayford anomalies and any other class of topography. There were found the usual relations between the elevations of the stations and the gravity anomalies based upon the Bouguer and the free air methods. (See p. 61 and figs. 13 and 14.)

Decided relations were found in the United States and in India between the sign of the gravity anomalies and the Cenozoic geologic formation. The anomalies at stations located on this formation tend to be negative. In the United States a number of the Cenozoic stations are located on or very near the coast. As stated above, there appeared to be a relation between the gravity anomalies and the coast. This is probably explained by the presence of the very light material of the Cenozoic formations, which is present along nearly all the Atlantic and Gulf coasts of the United States. It seems probable that the negative anomalies at Cenozoic stations are in large part due to the presence of subnormal densities in the upper crust below sea level.

There were found decided relations between the pre-Cambrian, Paleozoic, and Mesozoic formations and the sign of the gravity anomalies for the area of the United States. No very definite relations were observed in Canada and in India. (See pp. 70-84.)

It was found as a result of certain computations and investigations that local distribution of the compensation of a topographic feature is in general nearer the truth than regional distribution of the compensation out to the outer limit of zone O (167 km.). It is not clear whether local distribution is more probable than the regional distribution out to the limit of zone M (59 km.). (See pp. 91 and 92.)

^a From A Supplemental Investigation in 1906 of the Figure of the Earth and Isostasy.

The difference in the anomalies at two stations which are close together horizontally, but which have a large difference in the elevations, seemed to indicate some error in the height formula used to compute the correction to gravity for the elevation of the station above sea level. A careful study of the matter showed no error in the formula, but it seemed to indicate that the difference in the anomalies could result from the combination of several causes no one of which could alone make the difference. (See pp. 93-96.)

The best formula resulting from this investigation with which to obtain the theoretical value of gravity at any latitude in any part of the world was derived from 216 stations in the United States, 42 in Canada, 73 in India, and 17 in Europe, 348 stations in all. (See solution 8a, p. 127.) For each of these stations the reduction for topography and isostatic compensation had been made by the Hayford method, using the same or very similar tables to those in Special Publication No. 10.

The formula is

$$\gamma_0 = 978.039 (1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi)$$

in which γ_0 is the value of gravity sought and ϕ is the latitude of the station.

The first term of the formula is the theoretical value of gravity at the equator. From the constants of this formula was derived a value for the reciprocal of the flattening of the earth, which is 297.4. This value of the flattening is very close to other values recently derived from geodetic data in the United States and elsewhere. In the author's opinion it may be considered as at least equal in strength to any other value derived from geodetic data. It is only 0.4 larger than Hayford's best value from deflections, 297.0. It is only 0.8 less than Helmert's value of 1901, and only 0.6 lower than the author's value of 1912. It is only 0.7 larger than Helmert's value of 1915.

The values of the terms in the other gravity formulas and for other depths of compensation are of interest and value as showing how conditions may be different in different parts of the country. The table of values shown on page 129 is remarkable in showing values which are so accordant although derived from data under different conditions and in different areas.

If we assume that all the differences between the observed and computed values of gravity in the United States are due to errors in the assumed equatorial gravity and the depth of compensation, then the most probable gravity formula derived from data in this country alone is

$$\gamma_0 = 978.040 (1 + 0.005302 \sin^2 \phi - 0.000007 \sin^2 2\phi)$$

and the derived depth of compensation is 60 km. The equatorial value of gravity in this formula agrees well with the world formula. It is from this formula that the 1916 Hayford anomalies were computed.

From the various evidence it may be concluded that the average depth is probably greater than 60 km. As stated above, it is probably not far from being 96 km.

The cause of the greater part of the anomalies is believed to be in general the deviation from normal in the densities in the upper crust probably not far below sea level.

The study of the tables and maps accompanying this volume will convince one that in the regions considered the deviation of the earth's crust from a state of perfect isostasy is slight, even for areas of comparatively small size.

The evidence near Seattle, Wash., Minneapolis, Minn., and Washington, D. C., is conclusive that the cause of an anomaly is not regional in extent. If it were, the anomalies which are close together would not show such changes in sign and size.

A problem presents itself to the geodesists of the world which can be easily solved. It is that each nation reduce its own gravity stations for topography and isostatic compensation by some rational method and publish the results. It will be well if the same system is employed by each nation, and to this end the International Geodetic Association will no doubt gladly lend its aid. If this work were done, the results would be of very great value to many branches of science.

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No claim to exhaustiveness is made for the following list of articles and passages in books and memoirs dealing with isostasy and related subjects. No attempt has been made to cover the more general field of articles treating of the constitution of the interior of the earth.

The arrangement of articles is approximately chronological, according to the date of publication.

There were premonitions of the idea of isostasy long before it was definitely formulated. The French expedition to Peru observed latitudes north and south of Mount Chimborazo, and Bouguer ^a expresses surprise at the small deflection of the vertical produced by the mountain, as compared with what he had been led to expect by his calculations from its size and density. He speculates on the possibility of cavities, but does not elaborate much on the subject. A more modern instance is that of Petit, who found the effect of the attraction of the Pyrenees on the latitude of Toulouse small but opposite in sign to what he had expected.^b Boscovich,^c in attempting to explain the phenomena, approaches the modern idea rather more closely. Commenting on Bouguer's result, he expresses the opinion that the mountains are swellings caused by the earth's internal heat. "If this be the case," he says, "*no matter is added there and the empty space within the vitals compensates all the visible matter that rears itself up into the mountain mass.*" Probably examples of other premonitions could be gathered, but the subject passes beyond mere speculation only when some attempt is made to get a numerical estimate of the effects involved. Extensive calculation on the subject began with Archdeacon Pratt, whose name therefore heads the list.

The name "isostasy" seems to have been proposed and first used by Maj. C. E. Dutton. (See list for 1889 under his name.) Lowthian Green has been referred to as an early advocate of the idea of isostasy. His book, "Vestiges of the Molten Globe," London, 1873, is not available at this writing and references to it do not make plain whether he used the word "isostasy" or not. In any case Maj. Dutton seems to have coined the word independently.

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PART II.—SUMMARIES OF GRAVITY OBSERVATIONS AND DESCRIPTIONS OF STATIONS.



CHAPTER I.—ABSTRACTS OF RESULTS.

In this part of the volume are given the abstracts of the observations made at the base station in the office of the United States Coast and Geodetic Survey at Washington, D. C., and at the field stations in the United States established in 1909 and later years, for which similar data have not already been published in the various reports of the Survey. There are also given the descriptions of all the stations.

An index on page 187 gives the names of the stations and the pages of the various publications in which gravity data may be found.

STANDARDIZATION OF THE PENDULUMS AND METHODS OF OBSERVING USED IN THE FIELD.

As is stated on page 49, the pendulums were standardized at the Washington station before and after a field season or between two seasons which were not long separated in time.

Usually the mean of the two values of the periods of a pendulum determined at the base station before and after a season's field work was used in the determination of the relative intensity of gravity at the field stations. An exception to this general rule occurred when it was found, after the season extending from June to December, 1909, that the periods of the pendulums had been affected between standardizations by a film of foreign substance, which had accumulated on the agate planes of the pendulums. Upon the removal of the film the pendulums resumed nearly their former Washington periods. (See p. 141.)

Beginning with the standardization of the pendulums in 1912, each of the pendulums had its period determined each time by swinging it continuously between consecutive determinations of the chronometer corrections. This plan has been followed since that time, both at the base station and in the field in establishing new stations. The previous custom had been to swing all of the pendulums of a set during the interval between two determinations of the chronometer corrections. It was only occasionally that more than two determinations of the chronometer corrections were made at a station.

Each of the pendulums of a set is now swung for at least 24 hours in three periods of 8 hours each, while previously each pendulum was swung for only 16 hours at a station in two periods of 8 hours each unless unfavorable weather prevented time observations on the stars at the end of the 48-hour period. In the earlier work the variation in the rate of the chronometers would occasionally make a large range in the values of the gravity at a station determined by the separate pendulums, but the mean of all the values was free from the effect of change in rate.

In the present method, where the period of a pendulum is obtained from separate time determinations, the result for any one pendulum is not affected by variation in the rate of the chronometers.

ABSTRACTS OF RESULTS.

In the table on pages 144–176 are given the pendulum observations and reductions for the stations in the United States which were determined in 1909 and later years. Similar data for the stations established before that year are given in other publications of the Survey,

which are indicated in the index on page 187. The number of a station is the same as was used in the various tables and the discussion in Part I of this volume. (See especially the table on pp. 50-52.)

The tables need little explanation. Under the heading "Total arc" are given the values of the arc through which the pendulum oscillates at the beginning and at the end of a period which is usually about 8 hours long. The period given has been corrected to reduce to an infinitesimally small arc.

The standard temperature is 15°C. , and a correction is applied to the period for any deviation of the observed from the standard temperature. The standard pressure of the air in the pendulum case is 60 mm. of mercury. A correction must also be applied for deviations of the pressure from the standard.

Finally there is the correction for flexure. This is necessary because the force of the pendulum in motion makes a sympathetic swinging of the pendulum case and its support, and this in turn reacts on the pendulum and affects its period. The flexure is determined by means of the interferometer, which is described in Appendix 6 of the Report for 1910. The flexure of the case and its support makes the period too long, and consequently the correction necessary to reduce the period to what it would have been in a rigid structure is negative.

It will be noticed that the period of a pendulum is determined by its comparison with each of two chronometers. This is done to avoid mistakes and to make the effect of accidental errors smaller.

The coincidence interval, as its name suggests, is the time which elapses between two consecutive coincidences between the beat of the chronometer and the swing of the pendulum.

The pendulums were swung in the direct position in all cases, both at the base stations and in the field. This fact is indicated in column 3 of the tables. The pendulums are designated as A4, A5, and A6 in one set and B4, B5, and B6 in the other. The pendulums used are indicated in the second column.

The tables do not state whether there were local time observations or comparisons of the chronometers with the noon signals sent out from the Naval Observatory over the commercial telegraph lines (The Western Union and Postal Telegraph Companies). It is evident, however, from the data in the columns of corrections for rate that there was such a determination between the two swings where a change in the rate corrections occurs. If the rate corrections at a station are the same for each swing, then there were only two determinations of the chronometer corrections at that station, one at the beginning and the other at the end of the entire set of observations, as it is quite unlikely that the computed rates during two intervals between three different time comparisons would come out exactly identical.

During the first season of 1909, the season of 1914, and the first season of 1915 pendulum B4 showed great changes in its period. Careful inspection of the pendulum failed to discover any cause for this. It was finally decided to strengthen by an additional rivet the connection between the stem and the bob; after this was done no further trouble occurred.

There is given below a summary of the periods at the base station of the six United States Coast and Geodetic Survey pendulums. These periods were used in computing the relative intensity of gravity at the field stations.

Summary of periods of pendulums resulting from standardizations at the base station, Coast and Geodetic Survey Office, Washington, D. C.

Date	Mean periods						Observer
	A4	A5	A6	B4	B5	B6	
January, 1909.....	0.5008393	0.5008615	0.5008240	0.5008091	0.5007230	0.5007031	W. H. Burger
June, 1909.....	.5008368	.5008612	.5008231	.5008229	.5007212	.5007036	Do.
November, 1909.....	.5008320	.5008601	.5008208				Do.
December, 1909.....	.5008362	.5008595	a. 5008248	.5008257	.5007220	.5007040	Do.
Do.....	.5008363	.5008592	a. 5008234				Do.
May, 1910.....	.5008353	.5008588	.5008233				Do.
October, 1910.....	.5008348	.5008602	.5008257	.5008246	.5007220	.5007016	H. D. King.
June, 1911.....	.5008374	.5008618	a. 5008265				T. L. Warner.
Do.....	.5008360	.5008622	a. 5008289				Do.
January, 1912.....	.5008392	.5008635	.5008286	.5008126	.5007232	.5007042	Do.
July, 1914.....	.5008377	.5008623	b. 5008247	.5008117	.5007225	b. 5007026	C. L. Garner and
Do.....	.5008385	.5008639	c. 5008272	.5008119	.5007228	c. 5007020	J. D. Powell.
January, 1915.....	.5008373	.5008629	.5008288	.5008178	.5007210	.5007023	Do.
July, 1915.....	.5008379	.5008629	.5008278	.5008289	.5007207	.5007013	Do.
January, 1916.....	.5008392	.5008639	.5008301	.5008292	.5007209	.5007014	Do.
Mean.....	.5008369	.5008613	.5008262		.5007219	.5007026	

a The mean was used.

b Rate corrections were determined from star observations.

c Rate corrections were determined from the noon signals sent by telegraph from the Naval Observatory at Washington, D. C.

During the second season of 1909, mentioned on page 139, in which the periods of the pendulums were affected by films of foreign substance on the agate planes on which the pendulums swing, W. H. Burger established the following stations in the order given. The table shows which stations were reoccupied, the name of the second observer, and the value of gravity adopted.

Number and name of station	Reoccupied in 1910 or 1911 by—	Adopted value of gravity	Number and name of station	Reoccupied in 1910 or 1911 by—	Adopted value of gravity
102. Cloudland, Tenn.....			88. Wilson, N. Y.....		
103. Hughes, Tenn.....	T. L. Warner.....	979.553	89. Alpena, Mich.....		
106. Fort Kent, Me.....			57. Iron River, Mich.....	H. D. King.....	980.633
85. North Hero, Vt.....	H. D. King.....	980.588	58. Ely, Minn.....		
86. Lake Placid, N. Y.....			59. Pembina, N. Dak.....		
87. Potsdam, N. Y.....			60. Mitchell, S. Dak.....		

In order to strengthen the field work, stations Hughes, North Hero, and Iron River were reoccupied as is indicated in the above table. The King and Warner values were adopted for North Hero and Hughes, respectively. The Burger value for Iron River when the November 4 to 10, 1909, Washington periods were used differed only 0.006 from King's value. The mean of the two determinations for that station was adopted. The November 4 to 10, 1909, Washington periods were also used in computing the value of gravity at Ely, Pembina, and Mitchell. (See p. 87 of Special Publication No. 10).

For Cloudland the Washington periods of November 4 to 10, 1909, and Warner's periods at station Hughes were used as standard values. North Hero and Iron River, with their adopted values of gravity, were used as the base stations for Lake Placid, Potsdam, Wilson, and Alpena. Hughes and North Hero, with their adopted values of gravity, were used as bases in determining the value of gravity at Fort Kent.

From July, 1914, until January, 1916, the chronometer corrections at the base stations and at field stations were obtained from comparisons with the noon signals sent over the lines of the Western Union and the Postal Telegraph companies from the Naval Observatory at Washington. At the beginning of each month the corrections to the time as sent out by the observatory were furnished for each day of the preceding month. These corrections were seldom greater than 0.10 second. Before the year 1914 the chronometer rates were determined by the gravity parties from local time observations on the stars with an astronomic transit.

The tests at the base station and at field stations showed that the time by telegraph gave as satisfactory results as the time determined by local astronomic observations. Of course there were errors in the absolute time as received at a field station over the telegraph wires due to the time of transmission, but this error was probably very nearly the same for each day at a station, and the effects on the rate determinations of the chronometers were not appreciable.

In the table on page 141 there are given the results of two standardizations in July, 1914, one with local time and the other with time from the observatory. The two results agree closely.

There are given below the values of the gravity at three stations at which both local and Naval Observatory time was used in rating the chronometers. The values indicate that the observatory time by telegraph is satisfactory.

Name of station	Observer	Date	Time used	Observed gravity
Wilmer, Ala.....	H. D. King.....	1911	Local time.....	979.346
	C. L. Garner.....	1914	Noon signals.....	979.345
Albany, N. Y.....	T. L. Warner.....	1911	Local time.....	980.343
	C. L. Garner.....	1914	Noon signals.....	980.344
Little Rock, Ark.....	G. R. Putnam.....	1896	Local time.....	979.720
	J. D. Powell.....	1914	Noon signals.....	979.728

The use of the observatory time materially lessens the work and the cost of establishing a gravity station.

There is given below a table which shows the chronometer rates at stations near and at others which are distant from Washington. These rates were determined from the comparisons with the Naval Observatory time received by telegraph. The range in the daily rates at the distant stations is about the same as the range for the near ones. As there are two chronometers, it can be seen whether the rates are due to errors in the time signals or to conditions not connected with those signals. For instance, when the rate for one day is considerably lower by both chronometers than for the other two days it is probable that this is due to the time signals. This might be the case for the first 24-hour period at station 194 (Huntley, Mont.). This is also the case for the first interval at station 202 (Moorcroft, Wyo.). Here the error was of such size that the observer swung his pendulums a fourth day. On the other hand, at station 192 (Poplar, Mont.) the third day gives a low rate for one chronometer and a normal rate for the other, and the cause of the variation of the first could not have been an error in the time signals.

The chronometers are subject to the temperature changes which occur in the pendulum room, which no doubt cause variations in the rates, but, as the pendulums are swung almost continuously for the interval between the determinations of the chronometer corrections, no appreciable errors enter into the mean period for a pendulum from the variation in rate.

Chronometer rates.

STATIONS NEAR WASHINGTON (MAXIMUM DISTANCE 800 KM.).

Number and name of station	Date, 1915	Daily rates		Number and name of station	Date, 1915	Daily rates	
		Chronometer No. 1823	Chronometer No. 1841			Chronometer No. 1823	Chronometer No. 1841
		<i>Seconds</i>	<i>Seconds</i>			<i>Seconds</i>	<i>Seconds</i>
146. Richmond, Va.....	Feb. 9-10.....	-3.89	-2.07	155. Knoxville, Tenn.....	May 10-12.....	-3.47	-3.23
	Feb. 10-11.....	-3.78	-2.07		May 12-13.....	-3.71	-3.40
	Feb. 11-12.....	-3.99	-2.27		May 13-14.....	-3.45	-3.36
147. Emporia, Va.....	Feb. 24-25.....	-2.87	-2.18	156. Bristol, Va.....	May 19-20.....	-3.92	-3.58
	Feb. 25-26.....	-2.28	-1.82		May 20-21.....	-3.80	-3.61
148. Greenville, N. C.....	Mar. 9-10.....	-3.85	-2.82		May 21-22.....	-3.56	-3.42
	Mar. 10-11.....	-2.97	-2.97	209. Laurel, Md.....	Nov. 18-19.....	-2.19	+3.08
	Mar. 11-12.....	-3.80	-2.86		Nov. 19-21.....	-2.24	+3.45
149. Wilmington, N. C.....	Mar. 16-17.....	-3.81	-2.88		Nov. 21-22.....	-2.34	+3.55
	Mar. 17-18.....	-3.56	-2.63	212. Rockville, Md.....	Nov. 27-28.....	-1.51	+2.55
	Mar. 18-19.....	-3.66	-2.63		Nov. 28-29.....	-1.68	+2.35
150. Cheraw, S. C.....	Mar. 25-26.....	-3.73	-2.80		Nov. 29-30.....	-2.20	+2.46
	Mar. 26-27.....	-3.84	-3.15	214. Fairfax, Va.....	Dec. 3-4.....	+0.27	+3.20
	Mar. 29-30.....	-3.46	-2.92		Dec. 4-5.....	+0.45	+3.34
151. Charlotte, N. C.....	Apr. 5-6.....	-2.65	-1.87		Dec. 5-6.....	+0.60	+3.40
	Apr. 6-7.....	-2.44	-2.05	213. Upper Marlboro, Md.....	Dec. 11-12.....	+2.26	+3.41
	Apr. 7-8.....	-2.26	-2.06		Dec. 12-13.....	+1.52	+3.72
154. Winston-Salem, N. C.....	Apr. 12-13.....	-3.38	-2.73		Dec. 13-14.....	+1.01	+3.86
	Apr. 13-14.....	-3.54	-3.10				
	Apr. 14-15.....	-3.55	-2.93	219. Hagerstown, Md.....	1916.		
152. Asheville, N. C.....	Apr. 22-23.....	-4.02	-3.21		Jan. 8-9.....	-1.92	+3.35
	Apr. 23-24.....	-4.14	-3.36		Jan. 9-10.....	-1.65	+3.38
	Apr. 24-25.....	-3.97	-3.32		Jan. 10-11.....	-2.09	+3.57
153. Cleveland, Tenn.....	Apr. 30-May 1.....	-3.88	-3.09				
	May 1-2.....	-3.80	-3.04				
	May 2-3.....	-3.75	-3.12				

STATIONS DISTANT FROM WASHINGTON (MAXIMUM DISTANCE 2700 KM.; MINIMUM DISTANCE 1400 KM.).

Number and name of station	Date, 1915	Daily rates		Number and name of station	Date, 1915	Daily rates	
		Chronometer No. 1828	Chronometer No. 1838			Chronometer No. 1828	Chronometer No. 1838
		<i>Seconds</i>	<i>Seconds</i>			<i>Seconds</i>	<i>Seconds</i>
186. Aberdeen, S. Dak.....	Aug. 5-6.....	-2.10	+8.14	195. Lander, Wyo.....	Sept. 29-30.....	-2.31	+2.17
	Aug. 6-7.....	-2.21	+8.26		Sept. 30-Oct. 1.....	-2.33	+2.18
	Aug. 7-8.....	-2.14	+8.34		Oct. 1-2.....	-2.17	+2.13
187. Faith, S. Dak.....	Aug. 12-13.....	-2.18	+6.62	198. Edgemont, S. Dak.....	Oct. 5-7.....	-1.74	+2.18
	Aug. 13-14.....	-2.24	+7.24		Oct. 7-8.....	-1.83	+2.67
	Aug. 14-15.....	-1.90	+7.48		Oct. 8-9.....	-2.01	+2.36
190. Towner, N. Dak.....	Aug. 20-21.....	-1.61	+7.87	202. Moorcroft, Wyo.....	Oct. 12-13.....	0.00	+4.12
	Aug. 21-23.....	-1.50	+7.63		Oct. 13-14.....	-1.40	+2.84
	Aug. 23-24.....	-1.91	+6.22		Oct. 14-15.....	-0.74	+3.31
190. Crosby, N. Dak.....	Aug. 27-28.....	-1.94	+3.61		Oct. 15-16.....	-1.01	+3.26
	Aug. 28-29.....	-1.62	+5.25	201. Wasta, S. Dak.....	Oct. 20-21.....	-1.00	+2.48
	Aug. 29-30.....	-1.86	+4.97		Oct. 21-22.....	-1.16	+2.25
192. Poplar, Mont.....	Sept. 2-3.....	-1.75	+5.74		Oct. 22-23.....	-1.19	+2.08
	Sept. 3-4.....	-1.37	+5.68	206. Valentine, Nebr.....	Oct. 26-27.....	-1.85	+3.36
	Sept. 4-5.....	-1.01	+5.78		Oct. 27-28.....	-1.88	+3.26
188. Marmarth, N. Dak.....	Sept. 10-12.....	-0.80	+4.25		Oct. 28-29.....	-1.91	+3.01
	Sept. 12-13.....	-1.10	+4.90	205. Randolph, Nebr.....	Nov. 2-3.....	-1.46	+2.13
	Sept. 13-14.....	-1.12	+5.26		Nov. 3-4.....	-1.62	+2.35
193. Miles City, Mont.....	Sept. 17-18.....	-1.01	+1.44		Nov. 4-5.....	-1.42	+2.31
	Sept. 18-19.....	-1.18	+1.63	208. Leon, Iowa.....	Nov. 10-11.....	-3.27	+3.56
	Sept. 19-20.....	-1.52	+1.29		Nov. 11-12.....	-3.38	+3.56
194. Huntley, Mont.....	Sept. 22-23.....	-0.13	+1.08		Nov. 12-13.....	-2.95	+3.22
	Sept. 23-24.....	-0.39	+1.36				
	Sept. 24-25.....	-0.66	+1.47				

Pendulum observations and reductions.

[Chronometer numbers are shown in boldfaced type, both in box headings and the body of the table.]

Station and observer	Swing No.	Pen- du- lum	Post- tion	Date	Coincidence In- terval		Total arc		Tem- pera- ture	Pres- sure	Period uncorrected		Corrections (seventh decimal place)				Period corrected		θ	Mean θ	
					Chro- no- meter No. 1823	Chro- no- meter No. 1841	Ini- tial	Final			Chro- no- meter No. 1823	Chro- no- meter No. 1841	Arc	Tem- pera- ture	Pres- sure	Rate		Chro- no- meter No. 1823			Chro- no- meter No. 1841
Washington, D. C., Coast and Geodetic Survey Office, Wil- lam H. Burger.	1	A4	D	1908-9	302.92	300.26	5.1	1.9	13.2	48	0.508294	0.508340	-10	+72	+	89	+	0.508307	0.508314		
	2	A4	D	Dec. 8	303.75	300.56	4.6	1.6	12.86	50	0.508211	0.508257	-11	+90	+	89	+	0.508218	0.508225		
	3	A4	D	Dec. 9	304.17	300.76	5.3	2.1	13.02	51	0.508235	0.508281	-11	+83	+	89	+	0.508242	0.508249		
	4	A4	D	Dec. 9	304.06	300.28	5.0	2.0	12.73	52	0.508255	0.508301	-10	+82	+	89	+	0.508262	0.508269		
	5	A4	D	Dec. 10	304.34	301.43	4.7	1.5	12.56	54	0.508228	0.508274	-8	+94	+	89	+	0.508235	0.508242		
	6	A4	D	Dec. 10	305.57	302.52	5.0	1.9	11.68	58	0.508194	0.508240	-9	+102	+	89	+	0.508201	0.508208		
	7	A4	D	Jan. 1	308.28	304.30	4.7	1.9	10.86	59	0.508123	0.508169	-9	+161	+	121	+	0.508130	0.508137		
	8	A4	D	Jan. 2	308.04	304.70	4.9	2.0	10.86	59	0.508129	0.508175	-10	+173	+	121	+	0.508136	0.508143		
	9	A4	D	Jan. 2	308.98	303.20	5.1	1.9	11.11	62	0.508160	0.508206	-8	+168	+	121	+	0.508167	0.508174		
	10	A4	D	Jan. 3	307.14	303.24	5.4	1.5	11.48	58	0.508153	0.508199	-13	+147	+	121	+	0.508160	0.508167		
	11	A4	D	Jan. 3	307.25	303.08	5.4	1.7	11.06	58	0.508150	0.508196	-13	+147	+	121	+	0.508157	0.508164		
	12	A4	D	Jan. 3	308.70	304.58	5.1	1.7	11.06	58	0.508152	0.508198	-13	+147	+	121	+	0.508159	0.508166		
	13	A5	D	Jan. 15	302.64	306.59	4.8	1.7	10.98	55	0.508352	0.508398	-8	+165	+	122	+	0.508359	0.508366		
	14	A5	D	Jan. 16	302.64	306.59	4.8	1.7	10.98	55	0.508352	0.508398	-8	+165	+	122	+	0.508359	0.508366		
	15	A5	D	Jan. 16	304.47	308.04	5.2	1.8	11.03	58	0.508346	0.508392	-10	+169	+	122	+	0.508353	0.508360		
	16	A5	D	Jan. 16	305.97	309.54	5.1	1.6	10.57	60	0.508339	0.508385	-10	+186	+	122	+	0.508346	0.508353		
	17	A5	D	Jan. 17	303.63	307.20	5.0	1.6	10.57	62	0.508345	0.508391	-8	+180	+	122	+	0.508352	0.508359		
	18	A5	D	Jan. 17	304.29	307.86	4.9	1.5	12.92	52	0.508345	0.508391	-8	+180	+	122	+	0.508352	0.508359		
	19	A6	D	Jan. 28-27	412.08	408.02	4.9	1.5	12.92	52	0.508345	0.508391	-8	+180	+	122	+	0.508352	0.508359		
	20	A6	D	Jan. 27	411.61	407.43	4.7	1.8	13.12	58	0.508345	0.508391	-8	+180	+	122	+	0.508352	0.508359		
	21	A6	D	Jan. 27	411.61	407.43	4.7	1.8	13.12	58	0.508345	0.508391	-8	+180	+	122	+	0.508352	0.508359		
	22	A6	D	Jan. 27-28	410.78	406.30	5.0	1.7	13.24	61	0.508345	0.508391	-8	+180	+	122	+	0.508352	0.508359		
	23	A6	D	Jan. 28	409.84	405.34	5.3	1.7	13.24	62	0.508345	0.508391	-8	+180	+	122	+	0.508352	0.508359		
	24	A6	D	Jan. 28	413.21	407.44	4.8	1.7	13.10	64	0.508338	0.508384	-7	+80	-	1	+	0.508345	0.508352		
Washington, D. C., Coast and Geodetic Survey Office, Wil- lam H. Burger.	1	B4	D	Dec. 8	313.41	310.64	4.7	1.6	13.97	55	0.507990	0.508036	-8	+44	+	89	+	0.508001	0.508008		
	2	B4	D	Dec. 8	314.30	310.52	4.7	1.6	13.64	55	0.507907	0.507953	-8	+57	+	89	+	0.507918	0.507925		
	3	B4	D	Dec. 9	311.62	308.03	5.3	1.8	13.90	59	0.508435	0.508481	-10	+46	+	89	+	0.508446	0.508453		
	4	B4	D	Dec. 9	311.97	308.00	5.0	1.3	13.96	62	0.508427	0.508473	-7	+48	+	89	+	0.508438	0.508445		
	5	B4	D	Dec. 10	314.12	311.00	4.8	1.4	13.48	64	0.507971	0.508017	-7	+64	+	89	+	0.507982	0.507989		
	6	B4	D	Dec. 10	315.75	312.48	5.1	1.4	13.24	56	0.507930	0.507976	-8	+74	+	89	+	0.507941	0.507948		
	7	B4	D	Jan. 1	319.48	315.14	4.8	1.9	11.95	50	0.507838	0.507884	-10	+128	+	121	+	0.507849	0.507856		
	8	B4	D	Jan. 2	319.38	315.42	4.9	2.0	11.63	52	0.507848	0.507894	-10	+141	+	121	+	0.507859	0.507866		
	9	B4	D	Jan. 2	319.33	315.03	4.9	1.9	11.63	54	0.507835	0.507881	-10	+140	+	121	+	0.507846	0.507853		
	10	B4	D	Jan. 2	319.33	315.03	4.9	1.9	11.63	54	0.507835	0.507881	-10	+140	+	121	+	0.507846	0.507853		
	11	B4	D	Jan. 3	318.51	314.36	4.8	1.8	11.82	58	0.507802	0.507848	-10	+133	+	121	+	0.507813	0.507820		
	12	B4	D	Jan. 3	319.11	314.75	5.5	1.7	11.70	60	0.507811	0.507857	-10	+138	+	121	+	0.507822	0.507829		
	13	B5	D	Jan. 15	357.10	352.42	4.7	1.9	11.79	54	0.507011	0.507057	-11	+134	+	122	+	0.507022	0.507029		
	14	B5	D	Jan. 16	357.76	353.07	5.2	1.7	11.76	55	0.506994	0.507040	-11	+136	+	122	+	0.507005	0.507012		
	15	B5	D	Jan. 17	358.92	353.20	4.8	1.8	11.67	56	0.506963	0.507009	-8	+140	+	122	+	0.506974	0.506981		
	16	B5	D	Jan. 17	358.55	353.06	4.9	1.6	11.34	58	0.506959	0.507005	-8	+153	+	122	+	0.506970	0.506977		
	17	B5	D	Jan. 17	359.74	352.70	4.9	2.3	11.28	61	0.506939	0.506985	-11	+156	+	122	+	0.506950	0.506957		
	18	B6	D	Jan. 17	359.00	352.88	5.0	2.3	11.27	61	0.506934	0.506980	-11	+156	+	122	+	0.506945	0.506952		
	19	B6	D	Jan. 28-27	363.68	360.04	5.2	1.7	13.48	58	0.506853	0.506899	-10	+64	+	89	+	0.506864	0.506871		
	20	B6	D	Jan. 27	362.96	359.61	5.3	1.9	13.48	58	0.506853	0.506899	-10	+64	+	89	+	0.506864	0.506871		
	21	B6	D	Jan. 27	363.20	360.40	4.8	1.9	13.54	61	0.506853	0.506899	-10	+64	+	89	+	0.506864	0.506871		
	22	B6	D	Jan. 27-28	362.90	359.23	5.2	1.9	13.58	61	0.506853	0.506899	-10	+64	+	89	+	0.506864	0.506871		
	23	B6	D	Jan. 28	361.94	359.07	4.7	1.7	13.67	62	0.506874	0.506920	-7	+50	+	89	+	0.506885	0.506892		
	24	B6	D	Jan. 28	364.16	359.63	5.1	1.7	13.66	64	0.506875	0.506921	-8	+56	+	89	+	0.506886	0.506893		

		No. 2, West Palm Beach, Fla., William H. Burger.		No. 3, Punta Gorda, Fla., William H. Burger.		No. 4, Apalachicola, Fla., William H. Burger.		No. 6, Rayville, La., William H. Burger.		No. 8, Point Isabel, Tex., William H. Burger.		No. 12, McAlester, Okla., William H. Burger.		No. 14, Columbia, Tenn., William H. Burger.		No. 16, McCormick, S. C., William H. Burger.		No. 18, Beaufort, N. C., William H. Burger.	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
1	B4	D	Feb. 13-14...	230.08	231.68	4.7	1.7	20.50	61	.5010890	.6010819	-9	-230	+3	-41	-2	9	.5010604	.5010772
2	B4	D	Feb. 14...	229.74	230.70	4.4	1.7	20.74	61	.5010896	.6010826	-9	-241	+3	-41	-2	9	.5010610	.5010778
3	B4	D	Feb. 14-15...	219.64	219.90	6.1	1.8	21.21	59	.5010934	.6010910	-9	-256	+5	-41	-2	9	.5010724	.5010892
4	B5	D	Feb. 14-15...	218.76	219.90	6.0	1.8	21.22	60	.5010970	.6010924	-9	-261	+4	-41	-2	9	.5010754	.5010922
5	B6	D	Feb. 15...	233.62	234.54	5.0	1.7	21.42	60	.5008777	.5008815	-9	-269	+3	-41	-2	9	.5008532	.5008570
6	B6	D	Feb. 15...	233.95	234.54	5.1	2.0	21.75	60	.5008964	.5008911	-10	-283	+4	-41	-2	9	.5008625	.5008663
1	B4	D	Feb. 26-27...	233.76	235.78	4.8	1.8	16.97	58	.5010718	.6010696	-9	-83	+6	9	52	-11	.5010612	.5010780
2	B4	D	Feb. 27...	231.62	235.88	6.3	2.1	16.36	58	.5010678	.6010621	-9	-57	+6	9	52	-11	.5010688	.5010856
3	B5	D	Feb. 27...	234.00	235.46	6.4	2.1	17.55	60	.5009892	.6009846	-11	-107	+4	9	52	-11	.5009728	.5009896
4	B5	D	Feb. 27-28...	232.65	234.81	6.1	1.7	18.07	60	.5009915	.6009861	-9	-129	+4	9	52	-11	.5009750	.5009918
5	B6	D	Feb. 28...	236.77	238.85	6.1	1.6	17.48	62	.5009580	.6009526	-8	-104	+2	9	52	-11	.5009420	.5009588
6	B6	D	Feb. 28...	236.38	238.26	5.9	2.0	17.91	63	.5009695	.6009642	-13	-122	+1	9	52	-11	.5009541	.5009709
1	B4	D	Mar. 13-14...	240.64	239.43	6.1	1.5	20.88	63	.5010410	.6010364	-8	-246	+1	+11	73	-19	.5010149	.5010317
2	B4	D	Mar. 14...	241.74	239.34	6.1	1.6	20.56	63	.5010393	.6010347	-8	-253	+1	+11	73	-19	.5010125	.5010293
3	B5	D	Mar. 14...	236.82	238.82	4.8	1.5	21.78	65	.5009855	.6009809	-8	-281	0	+11	73	-19	.5009695	.5009863
4	B5	D	Mar. 14-15...	236.07	238.94	6.0	1.7	18.56	63	.5009114	.6009068	-9	-149	+1	+11	73	-19	.5009211	.5009379
5	B6	D	Mar. 15...	277.10	274.48	5.0	1.8	14.68	61	.5009038	.6008992	-9	+13	+2	+11	73	-19	.5008874	.5008942
6	B6	D	Mar. 15...	279.90	276.41	5.3	2.2	13.69	61	.5008948	.6008902	-12	+55	+2	+11	73	-19	.5008785	.5008853
1	B4	D	Mar. 24-25...	255.00	254.14	4.7	1.6	20.18	59	.5009823	.6009777	-8	-277	+5	-23	102	-11	.5009469	.5009637
2	B4	D	Mar. 25...	257.02	255.14	4.7	1.5	18.93	59	.5009716	.6009670	-8	-165	+7	+16	83	-11	.5009562	.5009730
3	B5	D	Mar. 25...	252.97	250.92	6.1	1.6	18.34	65	.5009851	.6009805	-8	-110	+1	-23	102	-11	.5009698	.5009866
4	B5	D	Mar. 25-26...	252.48	250.94	5.2	1.8	18.09	68	.5009876	.6009830	-10	-129	-2	-23	102	-11	.5009812	.5009980
5	B6	D	Mar. 26...	250.92	250.92	4.5	1.6	16.98	60	.5009696	.6009650	-7	-83	+4	-23	102	-11	.5009818	.5009986
6	B6	D	Mar. 26...	231.81	237.88	4.9	1.9	17.18	62	.5008582	.6008536	-10	-91	+2	-23	102	-11	.5008419	.5008587
1	B5	D	Apr. 6-7...	242.08	239.42	4.9	1.7	26.61	58	.5010349	.6010303	-9	-496	+7	+16	83	-11	.5009984	.5010152
2	B5	D	Apr. 7...	242.04	239.47	5.1	1.7	26.27	58	.5010350	.6010304	-9	-472	+7	+16	83	-11	.5009985	.5010153
3	B6	D	Apr. 7...	246.88	244.20	4.9	1.7	26.32	65	.5010147	.6010101	-9	-478	0	+16	83	-11	.5009770	.5009938
4	B6	D	Apr. 7-8...	246.56	244.01	6.1	1.8	26.42	66	.5010153	.6010107	-9	-474	+0	+16	83	-11	.5009771	.5009939
5	B4	D	Apr. 8...	220.47	218.38	5.0	2.0	25.67	61	.5011366	.6011320	-5	-401	+3	+16	83	-11	.5010918	.5011086
6	B4	D	Apr. 8...	222.10	220.08	4.9	0.7	24.58	62	.5011292	.6011246	-5	-401	+3	+16	83	-11	.5010844	.5011012
7	B4	D	Apr. 8-9...	222.89	221.02	4.9	1.2	22.89	62	.5011337	.6011291	-6	-232	+3	+16	83	-11	.5010880	.5011048
8	B4	D	Apr. 9...	255.34	253.21	4.5	1.2	20.53	60	.5011149	.6011103	-6	-232	+3	+16	83	-11	.5010896	.5011064
9	B6	D	Apr. 9-10...	255.18	253.05	6.0	1.2	19.21	63	.5009817	.6009771	-7	-176	0	+16	83	-11	.5009661	.5009829
10	B6	D	Apr. 9-10...	255.98	253.85	6.3	1.2	17.87	61	.5009800	.6009754	-10	-120	0	+16	83	-11	.5009644	.5009812
11	B5	D	Apr. 10...	252.42	250.77	4.9	1.9	16.99	61	.5009829	.6009783	-6	-83	+3	+16	83	-11	.5009667	.5009835
12	B5	D	Apr. 10...	253.05	250.74	4.6	1.7	17.16	61	.5009899	.6009853	-6	-91	+3	+16	83	-11	.5009810	.5009978
13	B4	D	Apr. 10-11...	226.78	224.67	5.4	1.3	18.29	61	.5011048	.6011002	-8	-138	+3	+16	83	-11	.5010710	.5010878
14	B4	D	Apr. 11...	226.78	224.67	5.4	1.9	19.06	61	.5011048	.6011002	-8	-170	+2	+16	83	-11	.5010710	.5010878
15	B5	D	Apr. 11...	226.85	224.60	4.9	1.9	19.06	62	.5011053	.6011007	-10	-250	+2	+16	83	-11	.5009550	.5009718
1	A4	D	Apr. 21-22...	255.45	253.96	6.4	1.9	18.93	55	.5009946	.6009900	-11	-165	+9	-19	101	-12	.5009608	.5009776
2	A4	D	Apr. 22...	257.49	255.02	6.1	1.7	17.82	55	.5009728	.6009682	-9	-118	+8	-19	101	-12	.5009570	.5009738
3	A5	D	Apr. 22...	314.66	310.22	4.9	1.7	17.89	62	.5009958	.6009912	-9	-121	+2	-19	101	-12	.5009799	.5009967
4	A5	D	Apr. 22-23...	314.92	310.67	5.2	1.5	17.24	67	.5009751	.6009705	-9	-94	+2	-19	101	-12	.5009814	.5009982
5	A6	D	Apr. 23...	327.78	325.33	6.3	2.0	16.96	60	.5009739	.6009693	-11	-82	+4	-19	101	-12	.5009739	.5009907
6	A6	D	Apr. 23...	326.50	324.26	4.9	1.9	17.80	63	.5009770	.6009724	-10	-117	+1	-19	101	-12	.5009513	.5009681
1	A5	D	May 3-4...	332.14	329.50	6.1	1.3	15.18	59	.5007338	.6007292	-8	-8	+4	+21	68	-16	.5007331	.5007500
2	A5	D	May 4...	333.44	329.46	6.0	1.7	14.85	59	.5007349	.6007303	-9	+6	+1	+21	68	-16	.5007345	.5007513
3	A6	D	May 4...	318.28	313.34	4.8	1.7	16.20	63	.5007188	.6007142	-9	-50	+1	+21	68	-16	.5007184	.5007352
4	A6	D	May 4-5...	317.94	313.48	5.0	1.8	15.87	64	.5007196	.6007150	-9	-36	-1	+21	68	-16	.5007192	.5007360
5	A4	D	May 5...	269.04	266.80	5.1	1.8	15.57	64	.5009310	.6009264	-9	-24	-1	+21	68	-16	.5009306	.5009474
6	A4	D	May 5...	268.34	265.22	4.8	1.8	16.56	66	.5009334	.6009288	-9	-65	-2	+21	68	-16	.5009330	.5009498
1	A4	D	May 12-13...	253.18	253.02	5.2	1.8	19.88	63	.5009894	.6009848	-10	-205	0	-36	60	-21	.5009422	.5009590
2	A4	D	May 13...	254.70	254.09	5.4	1.7	19.09	70	.5009835	.6009789	-10	-171	0	-36	60	-21	.5009452	.5009620
3	A5	D	May 13...	307.03	306.53	4.8	1.8	20.35	56	.5008156	.6008110	-9	-224	+7	-36	60	-21	.5008152	.5008320
4	A5	D	May 13-14...	306.46	305.99	4.8	1.8	20.56	58	.5008171	.6008125	-9	-253	+6	-36	60	-21	.5008167	.5008335
5	A6	D	May 14...	321.78	320.21	4.8	1.7	19.99	59	.5007820	.6007774	-9	-209	+5	-36	60	-21	.5007816	.5007984
6	A6	D	May 14...	320.16	319.35	4.8	1.7	21.24	61	.5007821	.6007775	-9	-261	+3	-36	60	-21	.5007817	.5007985
1	A4	D	May 24-25...	266.48	262.12	4.7	2.0	16.96	56	.5009399	.6009353	-9	-82	+7	+27	126	-18	.5009324	.5009492
2	A4	D	May 25...	265.58	262.88	4.9	1.5	17.38	57	.5009431	.6009385	-8	-100	+5	+27	126	-18	.5009356	.5009524
3	A5	D	May 25...	325.50	318.81	6.0	1.8	18.12	69	.5007992	.6007946	-9	-131	+6	+27	126	-18	.5007918	.5008086
4	A5	D	May 25-26...	323.15	317.39	4.9	1.8	18.50	61	.5007448	.6007402	-9	-146	+4	+27	126	-18	.5007424	.5007592
5	A6	D	May 26...	336.83	330.98	4.9	1.4	19.05	69	.5007432	.6007386	-8	-170	+5	+27	126	-18	.5007408	.5007576
6	A6	D	May 26...	336.48	329.26	4.7	1.8	19.06	61	.5007441	.6007395	-9	-196	+3	+27	126	-18	.5007417	.5007585

No. 2, West Palm Beach, Fla., William H. Burger.

No. 3, Punta Gorda, Fla., William H. Burger.

No. 4, Apalachicola, Fla., William H. Burger.

No. 6, Rayville, La., William H. Burger.

No. 8, Point Isabel, Tex., William H. Burger.

No. 12, McAlester, Okla., William H. Burger.

No. 14, Columbia, Tenn., William H. Burger.

No. 16, McCormick, S. C., William H. Burger.

No. 18, Beaufort, N. C., William H. Burger.

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Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pen- dulum	Date	Coincidence interval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected			Corrections (seventh decimal place)					Period corrected		Mean θ	Dynes	
				Chro- no- meter No. 1823	Chro- no- meter No. 1841	Inf- lial	Final			Chro- no- meter No. 1823	Chro- no- meter No. 1841	Arc	Tem- pera- ture	Pres- sure	Rate		Chro- no- meter No. 1823	Chro- no- meter No. 1841	Flex- ure			
															Chro- no- meter No. 1823	Chro- no- meter No. 1841						
Washington, D. C., Coast and Geodetic Survey Office, Wil- liam H. Burger.	1	A4	June 6-7.....	240.71	240.08	5.0	1.6	20.53	61	0.5008315	0.5008355	-8	-232	+3	+8	-155	-17	0.5008309	0.5008316		Mean 978.364 ±0.006	Dynes 978.370
	2	A4	June 7.....	240.18	240.08	5.0	1.6	20.55	62	0.5008311	0.5008351	-8	-233	+2	+8	-155	-17	0.5008307	0.5008314			
	11	A4	June 10.....	241.60	240.66	4.9	1.9	19.91	58	0.5008366	0.5008377	-10	-207	+5	+8	-155	-17	0.5008367	0.5008372			
	12	A4	June 10.....	242.42	240.14	4.9	1.8	19.71	59	0.5008364	0.5008373	-10	-197	+5	+8	-155	-17	0.5008364	0.5008368			
	13	A4	June 10.....	241.73	240.31	4.9	1.6	19.69	60	0.5008354	0.5008377	-10	-197	+4	+8	-155	-17	0.5008366	0.5008366			
	3	A5	June 7-8.....	365.54	357.32	4.9	1.6	20.48	58	0.5008358	0.5007007	-8	-228	+4	+8	-155	-17	0.5008367	0.5008365			
	4	A5	June 7-8.....	365.22	357.32	4.9	1.8	20.45	60	0.5008355	0.5007007	-9	-217	+4	+8	-155	-17	0.5008367	0.5008365			
	9	A5	June 9.....	365.24	355.94	5.1	1.8	20.18	60	0.5008354	0.5007007	-8	-213	+4	+8	-155	-17	0.5008358	0.5008361			
Washington, D. C., Coast and Geodetic Survey Office, Wil- liam H. Burger.	1	B4	June 15-16.....	295.28	290.34	5.2	1.6	20.55	59	0.5008318	0.5008326	-8	-233	+5	+11	-152	-11	0.5008245	0.5008245		Mean 978.364 ±0.006	Dynes 978.370
	2	B4	June 16.....	294.78	290.97	5.0	1.8	20.58	59	0.5008316	0.5008337	-9	-230	+5	+11	-152	-11	0.5008245	0.5008245			
	9	B4	June 18.....	296.88	291.08	4.6	1.7	20.60	59	0.5008335	0.5008401	-8	-235	+5	+11	-152	-11	0.5008107	0.5008203			
	3	B5	June 16.....	336.81	329.03	4.9	1.7	20.41	60	0.5007363	0.5007289	-9	-226	+4	+11	-152	-11	0.5007202	0.5007194			
	4	B5	June 16-17.....	335.50	328.43	5.1	1.8	20.40	60	0.5007363	0.5007314	-9	-226	+4	+11	-152	-11	0.5007232	0.5007220			
	5	B6	June 17.....	344.00	335.98	5.1	1.7	20.53	60	0.5007278	0.5007452	-9	-233	+4	+11	-152	-11	0.5007066	0.5007033			
	6	B6	June 17.....	345.58	336.78	4.8	1.6	20.56	61	0.5007245	0.5007435	-9	-232	+3	+11	-152	-11	0.5007066	0.5007033			
	7	B6	June 17-18.....	344.00	335.96	5.0	1.8	20.53	62	0.5007245	0.5007453	-9	-232	+2	+11	-152	-11	0.5007066	0.5007033			
No. 102, Cloudland, Tenn., William H. Burger.	1	A4	July 2-3.....	215.22	220.66	4.7	1.1	14.46	59	0.5010216	0.5010154	-6	+14	+4	+53	-181	-17	0.5010264	0.5010268		Mean 979.882 ±0.006	Dynes 979.884
	2	A4	July 3.....	216.18	220.14	4.7	1.2	14.26	59	0.5010216	0.5010332	-7	+31	+4	+53	-181	-17	0.5010237	0.5010262			
	3	A5	July 3.....	246.33	238.53	4.8	1.6	14.65	60	0.5008451	0.5008485	-7	+49	+3	+53	-181	-17	0.5008197	0.5008197			
	4	A5	July 3-4.....	297.22	280.08	4.7	1.3	13.84	61	0.5008451	0.5008485	-7	+49	+2	+53	-181	-17	0.5008197	0.5008197			
	5	A6	July 4.....	319.78	310.74	4.7	1.3	10.59	57	0.5007830	0.5008078	-8	+185	+5	+53	-181	-17	0.5008061	0.5008042			
	6	A6	July 4.....	321.32	313.00	4.7	1.8	9.31	58	0.5007792	0.5008000	-9	+238	+4	+53	-181	-17	0.5008061	0.5008035			
No. 103, Hughes, Tenn., William H. Burger.	1	A4	July 10-11.....	230.46	244.34	5.1	1.9	20.03	55	0.5010002	0.5010252	-10	-211	+9	+9	-229	-22	0.5009764	0.5009780		Mean 979.556 ±0.003	Dynes 979.560
	2	A4	July 11.....	230.78	244.34	5.1	1.7	19.75	57	0.5009888	0.5010227	-9	-199	+8	+9	-229	-22	0.5009764	0.5009776			
	3	A6	July 11.....	317.13	308.74	4.7	1.5	19.75	59	0.5009888	0.5010227	-9	-199	+6	+9	-229	-22	0.5009764	0.5009776			
	4	A6	July 11-12.....	315.34	307.58	5.0	1.7	19.75	60	0.5009888	0.5010227	-9	-199	+4	+9	-229	-22	0.5009764	0.5009776			
	5	A5	July 12.....	302.39	294.60	5.0	1.9	19.78	61	0.5009888	0.5010227	-10	-200	+3	+9	-229	-22	0.5009764	0.5009776			
	6	A5	July 12.....	303.56	286.17	5.1	1.5	19.13	63	0.5009888	0.5010227	-8	-207	+1	+9	-229	-22	0.5009764	0.5009776			
No. 104, Fort Kent, Me., William H. Burger.	1	A4	July 21-22.....	378.96	376.06	5.2	1.6	15.02	55	0.5006811	0.5006765	-9	-1	+8	+49	-130	-14	0.5006644	0.5006619		Mean 980.764 ±0.001	Dynes 980.772
	2	A4	July 22.....	378.82	368.77	4.8	1.6	14.72	66	0.5006811	0.5006765	-9	-12	+7	+49	-130	-14	0.5006644	0.5006619			
	3	A5	July 22.....	415.98	409.04	5.2	1.8	15.20	68	0.5006811	0.5006765	-9	-8	+5	+49	-130	-14	0.5006644	0.5006619			
	4	A5	July 22-23.....	410.20	409.42	5.2	1.8	15.05	69	0.5006811	0.5006765	-10	-21	+4	+49	-130	-14	0.5006644	0.5006619			
	5	A6	July 23.....	434.08	432.06	5.2	1.8	14.95	67	0.5006811	0.5006765	-10	+2	+6	+49	-130	-14	0.5006644	0.5006619			
	6	A6	July 23.....	434.87	431.70	5.2	1.8	14.94	68	0.5006811	0.5006765	-10	+3	+5	+49	-130	-14	0.5006644	0.5006619			
No. 85, North Hero, Vt., William H. Bur- ger.	1	A4	July 31-Aug. 1.....	349.42	343.60	5.1	1.3	17.59	58	0.5007165	0.5007266	-8	-109	+6	+52	-98	-15	0.5007091	0.5007092		Mean 980.583 ±0.003	Dynes 980.597
	2	A4	Aug. 1.....	350.53	343.94	5.2	1.2	17.05	58	0.5007143	0.5007280	-8	-86	+6	+52	-98	-15	0.5007092	0.5007079			
	3	A5	Aug. 1.....	468.14	474.60	5.1	1.5	16.84	63	0.5005346	0.5005306	-9	-79	+1	+52	-98	-15	0.5005298	0.5005306			
	4	A5	Aug. 1-2.....	465.02	453.11	5.1	1.5	16.98	67	0.5005346	0.5005324	-8	-83	+6	+52	-98	-15	0.5005298	0.5005324			
	5	A6	Aug. 2.....	496.74	482.75	5.3	1.7	16.68	60	0.5005038	0.5005184	-10	-70	+4	+52	-98	-15	0.5004999	0.5004999			
	6	A6	Aug. 2.....	501.95	491.69	5.2	1.7	16.75	61	0.5004935	0.5005192	-10	-75	+3	+52	-98	-15	0.5004999	0.5004999			

No. 56. Lake Placid, N. Y., William H. Burger.										No. 57. Potsdam, N. Y., William H. Bur- ger.										No. 58. Wilton, N. Y., William H. Burger.										No. 59. Alpena, Mich., William H. Burger.										No. 57. Iron River, Mich., William H. Burger.										No. 58. Ely, Minn., William H. Burger.										No. 59. Pembina, N. Dak., William H. Burger.										No. 60. Mitchell, S. Dak., William H. Burger.									
1	A4	D	Aug. 11-12.....	332.64	324.83	5.1	1.2	18.77	56	5007527	5007708	-7	32	7	24	-164	-12	5007504	5007504	980.425	980.425	±0.001																																																									
2	A4	D	Aug. 12.....	332.98	325.00	5.2	1.4	18.54	56	5007528	5007709	-8	33	8	25	-165	-13	5007505	5007505	980.426	980.426	±0.001																																																									
3	A5	D	Aug. 12.....	420.20	420.20	5.3	1.6	18.72	61	5005700	5005957	-9	30	9	26	-164	-12	5007506	5007506	980.427	980.427	±0.001																																																									
4	A5	D	Aug. 12-13.....	431.04	417.45	5.4	1.7	16.08	61	5005807	5005958	-9	45	9	27	-164	-12	5007507	5007507	980.412	980.412	±0.001																																																									
5	A6	D	Aug. 13.....	457.04	441.11	5.4	1.7	16.40	60	5005476	5005959	-10	46	10	28	-164	-12	5007508	5007508	980.416	980.416	±0.001																																																									
6	A6	D	Aug. 13.....	458.15	440.82	5.3	1.4	16.65	61	5005462	5005978	-9	61	9	29	-164	-12	5007509	5007509	980.421	980.421	±0.001																																																									
1	A4	D	Aug. 19-20.....	345.02	337.43	5.1	1.0	18.60	59	5007257	5007420	-7	59	7	30	-155	-14	5007510	5007510	980.582	980.582	±0.001																																																									
2	A4	D	Aug. 20.....	345.12	338.65	5.3	1.2	18.82	60	5007258	5007421	-8	147	8	31	-155	-14	5007511	5007511	980.579	980.579	±0.001																																																									
3	A5	D	Aug. 20.....	452.54	438.82	4.8	1.4	18.55	61	5005531	5005706	-8	140	8	32	-155	-14	5007512	5007512	980.583	980.583	±0.001																																																									
4	A5	D	Aug. 20-21.....	453.00	439.88	5.2	1.6	18.33	60	5005325	5005707	-9	140	9	33	-155	-14	5007513	5007513	980.584	980.584	±0.001																																																									
5	A6	D	Aug. 21.....	481.68	466.38	5.0	1.6	18.09	58	5005168	5005566	-8	125	8	34	-155	-14	5005062	5005062	980.578	980.578	±0.001																																																									
6	A6	D	Aug. 21.....	484.23	470.65	5.3	1.9	17.99	58	5005168	50055318	-11	125	8	35	-155	-14	5005062	5005062	980.582	980.582	±0.001																																																									
1	A4	D	Aug. 30-31.....	333.12	325.31	5.1	1.0	16.56	53	5007510	5007597	-7	66	7	36	-131	-16	5007489	5007489	980.433	980.433	±0.001																																																									
2	A4	D	Aug. 31.....	334.12	326.54	4.9	1.0	16.82	54	5007494	5007668	-6	34	6	37	-131	-16	5007490	5007490	980.431	980.431	±0.001																																																									
3	A5	D	Aug. 31.....	433.34	422.56	5.2	1.2	15.85	58	5005749	50059523	-8	54	8	38	-131	-16	5005720	5005720	980.430	980.430	±0.001																																																									
4	A5	D	Aug. 31-Sept. 1.....	432.76	420.04	5.2	1.3	16.30	59	5005763	5005959	-8	54	8	39	-131	-16	5005752	5005752	980.418	980.418	±0.001																																																									
5	A6	D	Sept. 1.....	463.70	449.71	5.2	1.5	15.39	60	5005394	5005565	-9	16	9	40	-131	-16	5005396	5005396	980.427	980.427	±0.001																																																									
6	A6	D	Sept. 1.....	463.60	453.82	5.0	1.2	15.04	63	5005397	5005515	-7	2	7	41	-131	-16	5005399	5005399	980.438	980.438	±0.001																																																									
1	A4	D	Sept. 10-11.....	348.94	335.82	5.1	1.3	17.60	56	5007175	5007456	-8	109	7	42	-143	-14	5007189	5007189	980.551	980.551	±0.001																																																									
2	A4	D	Sept. 11.....	348.90	335.60	5.2	1.5	17.52	57	5007178	5007460	-9	101	8	43	-143	-14	5007179	5007179	980.549	980.549	±0.001																																																									
3	A5	D	Sept. 11.....	464.90	441.96	5.0	1.6	17.40	61	5005383	5005663	-8	106	9	44	-143	-14	5005385	5005385	980.559	980.559	±0.001																																																									
4	A5	D	Sept. 11-12.....	464.11	441.72	5.0	1.6	17.37	63	5005393	5005666	-9	101	11	45	-143	-14	5005396	5005396	980.556	980.556	±0.001																																																									
5	A6	D	Sept. 12.....	463.36	469.20	5.0	1.6	17.50	57	5005072	5005374	-8	95	10	46	-143	-14	5005070	5005070	980.554	980.554	±0.001																																																									
6	A6	D	Sept. 12.....	463.60	470.63	5.0	1.7	17.60	59	5005070	5005318	-9	109	12	47	-143	-14	5005068	5005068	980.557	980.557	±0.001																																																									
7	A6	D	Sept. 12-13.....	461.92	470.76	5.0	1.6	17.62	60	5005087	5005318	-8	110	14	48	-143	-14	5005085	5005085	980.549	980.549	±0.001																																																									
8	A6	D	Sept. 13.....	461.24	459.82	5.1	1.6	17.72	57	5005426	5005680	-8	114	13	49	-143	-14	5005419	5005419	980.558	980.558	±0.001																																																									
9	A4	D	Sept. 13.....	348.70	335.64	5.0	1.6	17.65	59	5007180	5007459	-8	112	15	50	-143	-14	5007170	5007170	980.556	980.556	±0.001																																																									
1	A4	D	Sept. 18-19.....	339.42	338.64	5.0	1.4	16.35	61	5006964	5007181	-8	57	2	108	-139	-9	5006970	5006970	980.633	980.633	±0.001																																																									
2	A4	D	Sept. 19.....	339.76	348.51	5.1	1.4	16.33	62	5006965	5007184	-7	56	3	108	-139	-9	5006966	5006966	980.633	980.633	±0.001																																																									
3	A5	D	Sept. 19.....	432.93	402.15	4.9	1.4	16.45	60	5005173	5005431	-8	61	4	108	-139	-9	5005174	5005174	980.638	980.638	±0.001																																																									
4	A5	D	Sept. 19-20.....	432.16	401.30	5.2	1.4	16.36	63	5005178	5005431	-8	61	4	108	-139	-9	5005174	5005174	980.638	980.638	±0.001																																																									
5	A6	D	Sept. 20.....	517.52	491.30	5.2	1.2	16.24	60	5004836	5005094	-8	64	4	108	-139	-9	5004837	5004837	980.630	980.630	±0.001																																																									
6	A6	D	Sept. 20.....	518.46	499.32	5.0	1.7	16.51	61	5004826	5005114	-8	63	2	103	-139	-9	5004833	5004833	980.633	980.633	±0.001																																																									
1	A4	D	Sept. 27-28.....	363.20	368.76	5.1	0.9	16.03	55	5006532	5006780	-7	43	8	119	-178	-9	5006500	5006500	980.791	980.791	±0.001																																																									
2	A4	D	Sept. 28.....	361.88	366.58	5.1	0.8	15.96	56	5006535	5006782	-7	40	6	119	-178	-9	5006528	5006528	980.778	980.778	±0.001																																																									
3	A5	D	Sept. 28.....	518.86	497.97	4.8	1.2	16.23	57	5004823	5005128	-7	52	6	119	-178	-9	5004830	5004830	980.704	980.704	±0.001																																																									
4	A5	D	Sept. 28-29.....	517.04	520.94	5.0	1.2	16.43	58	5004830	5005144	-7	60	4	119	-178	-9	5004835	5004835	980.761	980.761	±0.001																																																									
5	A6	D	Sept. 29.....	555.01	525.94	5.2	1.2	16.51	59	5004836	5004994	-8	63	4	119	-178	-9	5004832	5004832	980.760	980.760	±0.001																																																									
6	A6	D	Sept. 29.....	557.10	518.88	5.1	1.4	16.65	61	5004491	5004823	-8	69	3	119	-178	-9	5004537	5004537	980.763	980.763	±0.001																																																									
1	A4	D	Oct. 7.....	396.74	380.39	5.1	1.2	18.78	61	5006309	5006581	-7	153	3	131	-153	-19	5006259	5006259	980.926	980.926	±0.001																																																									
2	A4	D	Oct. 7.....	397.28	378.60	5.2	1.1	18.24	62	5006310	5006612	-7	136	3	131	-153	-19	5006272	5006272	980.906	980.906	±0.001																																																									
3	A5	D	Oct. 7.....	556.17	522.70	4.9	1.3	17.99	60	5004499	5004787	-7	125	4	131	-153	-19	5004487	5004487	980.920	980.920	±0.001																																																									
4	A5	D	Oct. 7-8.....	549.25	517.76	5.0	1.5	18.08	61	5004836	5004836	-8	129	4	131	-153	-19	5004530	5004530	980.902	980.902	±0.001																																																									
5	A6	D	Oct. 8.....	601.51	566.62	5.2	1.2	17.57	60	5004160	5004416	-7	108	4	131	-153	-19	5004161	5004161	980.918	980.918	±0.001																																																									
6	A6	D	Oct. 8.....	590.32	559.62	5.0	1.1	18.14	61	5004471	5004471	-7	132	4	131	-153	-19	5004163	5004163	980.914	980.914	±0.001																																																									
7	A6	D	Oct. 8-9.....	598.55	538.50	5.1	1.6	18.04	61	5004181	5004480	-8	127	4	131	-153	-19	5004176	5004176	980.910	980.910	±0.001																																																									
8	A5	D	Oct. 9.....	584.62	527.94	5.2	1.3	17.10	58	5004471	5004740	-8	88	3	131	-153	-19	5004478	5004478	980.920	980.920	±0.001																																																									
9	A4	D	Oct. 9.....	405.35	387.62	5.3	1.6	16.38	57	5006176	5006458	-9	58	6	131	-153	-19	5006226	5006226	980.930	980.930	±0.001																																																									
1	A4	D	Oct. 21-22.....	324.04	312.94	5.2	1.3	18.87	62	5007705	5008004	-8	145	2	110	-167	-17	5007652	5007652	980.372	980.372	±0.001																																																									
2	A4	D	Oct. 22.....	324.94	313.84	5.2	1.3	18.47	63	5007706	5008002	-8	162	2	110	-167	-17	5007653	5007653	980.373	980.373	±0.001																																																									
3	A5	D	Oct. 22.....	420.96	402.58	4.0	1.2	18.87	58	5005946	5006217	-7	167	6	110	-167	-17	5005978	5005978	980.378	980.378	±0.001																																																									
4	A5	D	Oct. 22-23.....	419.76	401.40	4.8	1.2	18.99	60	5005963	5006232	-7	167	4	110	-167	-17	5005986	5005986	980.373	980.373	±0.001																																																									
5	A6	D	Oct. 23.....	445.48	424.12	5.3	1.2	18.83	59	5005618	5005948	-7	150	5	110	-167	-17	5005545	5005545	980.368	980.368	±0.001																																																									
6	A6	D	Oct. 23.....	448.08	427.31	5.2	0.9	18.57	61	5005586	5005858	-7	150	5	110	-167	-17	5005525	5005525	980.380	980.380	±0.001																																																									

Pendulum observations and reductions—Continued.

Station and observer	Spring No.	Per- duc- tum	Post- tion	Date	Coincidence In- terval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected		Corrections (seventh decimal place)					Period corrected		Mean θ	Dynes	
					Chro- no- meter No. 1823	Chro- no- meter No. 1841	Ini- tial	Final			Chronom- eter No. 1823	Chronom- eter No. 1841	Arc	Tem- pera- ture	Pres- sure	Rate		Chronom- eter No. 1823	Chronom- eter No. 1841			Mean
																Chro- no- meter No. 1823	Chro- no- meter No. 1841					
Washington, D. C., Coast and Geodetic Survey Office, Wil- liam H. Burger.	1	A4	D	Nov. 4-5-1909	300.72	291.69	5.1	17.70	1.5	57	0.508322	0.508385	-8	-113	+7	+126	-130	0.508324	0.508325	0.508324		
	2	A4	D	Nov. 5-6-1909	301.36	292.33	5.3	17.40	1.3	57	0.508309	0.508366	-8	-101	+6	+126	-130	0.508316	0.508317	0.508316		
	3	A4	D	Nov. 5-6-1909	301.78	292.63	5.1	17.08	1.3	56	0.508298	0.508355	-8	-87	+6	+126	-130	0.508319	0.508320	0.508319		
	4	A5	D	Nov. 5-6-1909	382.60	368.99	5.1	17.11	1.2	56	0.508543	0.508784	-7	-88	+7	+131	-129	0.508570	0.508571	0.508570		
	5	A5	D	Nov. 6-7-1909	385.26	368.30	5.2	17.05	1.4	57	0.508543	0.508784	-8	-96	+6	+131	-129	0.508570	0.508571	0.508570		
	6	A5	D	Nov. 6-7-1909	384.28	368.61	4.9	16.80	1.3	58	0.508514	0.508752	-7	-75	+7	+131	-129	0.508543	0.508544	0.508543		
	7	A8	D	Nov. 6-7-1909	406.54	390.17	5.0	16.71	1.2	58	0.508157	0.508416	-7	-72	+7	+137	-134	0.508208	0.508209	0.508208		
	8	A8	D	Nov. 7-8-1909	406.38	389.58	5.3	16.55	1.1	58	0.508159	0.508418	-7	-65	+7	+137	-134	0.508213	0.508214	0.508213		
	9	A6	D	Nov. 7-8-1909	409.04	391.26	4.9	16.23	1.0	59	0.508119	0.508378	-6	-62	+4	+137	-134	0.508191	0.508192	0.508191		
	10	A6	D	Nov. 7-8-1909	408.94	391.07	5.2	16.07	1.2	62	0.508121	0.508380	-8	-45	+1	+137	-134	0.508207	0.508208	0.508207		
	11	A6	D	Nov. 8-9-1909	407.25	389.96	5.0	16.19	1.2	66	0.508146	0.508401	-7	-50	+3	+137	-134	0.508220	0.508221	0.508220		
	12	A6	D	Nov. 8-9-1909	406.66	389.47	5.2	16.43	1.5	56	0.508155	0.508419	-9	-71	+5	+137	-134	0.508220	0.508221	0.508220		
	13	A6	D	Nov. 8-9-1909	405.50	388.66	5.2	16.70	1.4	58	0.508162	0.508427	-9	-71	+5	+137	-134	0.508221	0.508222	0.508221		
	14	A6	D	Nov. 9-10-1909	405.24	388.30	5.0	16.53	1.2	59	0.508174	0.508447	-8	-77	+4	+137	-134	0.508221	0.508222	0.508221		
	15	A6	D	Nov. 9-10-1909	405.42	387.72	5.2	16.70	1.5	60	0.508177	0.508450	-9	-71	+3	+137	-134	0.508221	0.508222	0.508221		
	16	A6	D	Nov. 10-11-1909	405.18	387.23	5.2	16.70	1.5	61	0.508177	0.508450	-9	-71	+3	+137	-134	0.508221	0.508222	0.508221		
	17	A6	D	Nov. 10-11-1909	406.79	390.01	5.1	16.58	1.6	62	0.508153	0.508418	-7	-66	+1	+137	-134	0.508202	0.508203	0.508202		
	18	A6	D	Nov. 10-11-1909	406.79	390.01	5.1	16.58	1.6	62	0.508153	0.508418	-7	-66	+1	+137	-134	0.508202	0.508203	0.508202		
Washington, D. C., Coast and Geodetic Survey Office, Wil- liam H. Burger.	1	A4	D	Nov. 26-27-1909	303.71	292.22	4.3	14.70	1.4	61	0.508245	0.508454	-7	+13	+2	+117	-94	0.508358	0.508359	0.508357		
	2	A4	D	Nov. 27-28-1909	304.36	293.65	4.7	14.50	1.3	64	0.508227	0.508441	-7	+21	+1	+117	-94	0.508345	0.508346	0.508346		
	3	A5	D	Nov. 27-28-1909	388.11	375.62	4.9	14.39	1.4	61	0.508150	0.508395	-8	+26	+2	+117	-94	0.508375	0.508379	0.508377		
	4	A5	D	Nov. 27-28-1909	387.90	375.65	4.8	14.29	1.7	58	0.508453	0.508694	-9	+30	+1	+121	-104	0.508582	0.508580	0.508580		
	5	A6	D	Nov. 28-29-1909	411.01	396.95	5.0	14.25	1.6	58	0.508690	0.508931	-8	+40	+2	+121	-104	0.508827	0.508825	0.508827		
	6	A6	D	Nov. 28-29-1909	411.52	394.62	4.9	14.04	1.5	61	0.508678	0.508919	-8	+40	+2	+121	-104	0.508821	0.508822	0.508822		
Washington, D. C., Coast and Geodetic Survey Office, Wil- liam H. Burger.	1	A4	D	Dec. 2-3-1909	307.01	293.96	4.9	12.78	1.8	65	0.508157	0.508376	-9	+83	-3	+142	-76	0.508368	0.508369	0.508369		
	2	A4	D	Dec. 3-4-1909	307.38	294.33	4.9	12.80	1.5	59	0.508147	0.508365	-8	+92	+4	+142	-76	0.508365	0.508365	0.508365		
	3	A5	D	Dec. 3-4-1909	392.86	378.42	4.7	12.91	1.3	64	0.508372	0.508613	-7	+85	+1	+142	-76	0.508592	0.508592	0.508592		
	4	A5	D	Dec. 3-4-1909	392.37	378.58	4.7	12.92	1.7	60	0.508379	0.508620	-8	+87	+2	+158	-83	0.508607	0.508607	0.508607		
	5	A6	D	Dec. 4-5-1909	415.71	399.69	4.9	12.99	1.6	56	0.508921	0.509162	-8	+84	+2	+158	-83	0.509049	0.509049	0.509049		
	6	A6	D	Dec. 4-5-1909	418.65	399.00	5.1	12.95	1.8	61	0.508908	0.509149	-9	+86	+2	+158	-83	0.509033	0.509033	0.509033		
Washington, D. C., Coast and Geodetic Survey Office, Wil- liam H. Burger.	1	B4	D	Dec. 2-3-1909	311.58	303.28	4.9	12.58	1.9	59	0.508037	0.508257	-10	+101	+3	+142	-76	0.508259	0.508261	0.508260		
	2	B4	D	Dec. 3-4-1909	311.70	303.27	5.0	12.43	1.6	59	0.508033	0.508253	-8	+103	+3	+142	-76	0.508261	0.508264	0.508264		
	3	B5	D	Dec. 3-4-1909	358.64	346.66	5.0	12.51	1.3	58	0.508080	0.508300	-8	+104	+3	+142	-76	0.508261	0.508263	0.508263		
	4	B5	D	Dec. 3-4-1909	358.00	347.00	4.8	12.51	1.3	59	0.508083	0.508303	-10	+103	+3	+158	-83	0.508263	0.508263	0.508263		
	5	B6	D	Dec. 4-5-1909	368.23	355.58	5.0	12.67	1.6	60	0.508078	0.508298	-9	+98	+12	+158	-83	0.508263	0.508263	0.508263		
	6	B6	D	Dec. 4-5-1909	369.38	355.42	4.5	12.61	1.6	50	0.508077	0.508297	-7	+100	+12	+158	-83	0.508263	0.508263	0.508263		
Washington, D. C., Coast and Geodetic Survey Office, Wil- liam H. Burger.	1	A4	D	Dec. 8-9-1909	308.24	299.96	4.7	13.02	1.7	60	0.508124	0.508348	-8	+83	+3	+178	-59	0.508368	0.508365	0.508362		
	2	A4	D	Dec. 9-10-1909	308.42	300.61	4.8	12.80	1.6	64	0.508119	0.508337	-8	+82	+1	+178	-59	0.508368	0.508359	0.508359		
	3	A5	D	Dec. 9-10-1909	305.91	300.62	5.1	12.41	1.6	61	0.508323	0.508577	-8	+109	+1	+178	-59	0.508591	0.508591	0.508590		
	4	A5	D	Dec. 9-10-1909	307.30	303.18	5.1	11.89	1.7	64	0.508300	0.508552	-8	+130	+7	+167	-49	0.508576	0.508592	0.508584		
	5	A6	D	Dec. 10-11-1909	421.63	407.82	4.7	11.31	1.5	61	0.508306	0.508558	-8	+135	+7	+167	-49	0.508584	0.508592	0.508592		
	6	A6	D	Dec. 10-11-1909	423.22	407.80	5.1	11.00	2.7	61	0.508314	0.508566	-13	+168	+1	+167	-49	0.508592	0.508625	0.508623		

No. 61. Sweetwater, Tex., William H. Burger.		No. 62. Kerrville, Tex., William H. Burger.		No. 63. El Paso, Tex., William H. Burger.		No. 64. Nogales, Ariz., William H. Burger.		No. 65. Yuma, Ariz., William H. Burger.		No. 66. Compton, Cal., William H. Burger.		No. 67. Goldfield, Nev., William H. Burger.		No. 68. Yavapai, Ariz., William H. Burger.		No. 69. Grand Canyon, Ariz., William H. Burger.	
1	A4	1	A4	1	A4	1	A4	1	A4	1	A4	1	A4	1	A4	1	A4
2	A5	2	A5	2	A5	2	A5	2	A5	2	A5	2	A5	2	A5	2	A5
3	A6	3	A6	3	A6	3	A6	3	A6	3	A6	3	A6	3	A6	3	A6
4	A5	4	A5	4	A5	4	A5	4	A5	4	A5	4	A5	4	A5	4	A5
5	A6	5	A6	5	A6	5	A6	5	A6	5	A6	5	A6	5	A6	5	A6
6	A8	6	A8	6	A8	6	A8	6	A8	6	A8	6	A8	6	A8	6	A8
7	A8	7	A8	7	A8	7	A8	7	A8	7	A8	7	A8	7	A8	7	A8
8	A8	8	A8	8	A8	8	A8	8	A8	8	A8	8	A8	8	A8	8	A8
9	A8	9	A8	9	A8	9	A8	9	A8	9	A8	9	A8	9	A8	9	A8
10	A8	10	A8	10	A8	10	A8	10	A8	10	A8	10	A8	10	A8	10	A8
11	A8	11	A8	11	A8	11	A8	11	A8	11	A8	11	A8	11	A8	11	A8
12	A8	12	A8	12	A8	12	A8	12	A8	12	A8	12	A8	12	A8	12	A8
13	A8	13	A8	13	A8	13	A8	13	A8	13	A8	13	A8	13	A8	13	A8
14	A8	14	A8	14	A8	14	A8	14	A8	14	A8	14	A8	14	A8	14	A8
15	A8	15	A8	15	A8	15	A8	15	A8	15	A8	15	A8	15	A8	15	A8
16	A8	16	A8	16	A8	16	A8	16	A8	16	A8	16	A8	16	A8	16	A8
17	A8	17	A8	17	A8	17	A8	17	A8	17	A8	17	A8	17	A8	17	A8
18	A8	18	A8	18	A8	18	A8	18	A8	18	A8	18	A8	18	A8	18	A8
19	A8	19	A8	19	A8	19	A8	19	A8	19	A8	19	A8	19	A8	19	A8
20	A8	20	A8	20	A8	20	A8	20	A8	20	A8	20	A8	20	A8	20	A8
21	A8	21	A8	21	A8	21	A8	21	A8	21	A8	21	A8	21	A8	21	A8
22	A8	22	A8	22	A8	22	A8	22	A8	22	A8	22	A8	22	A8	22	A8
23	A8	23	A8	23	A8	23	A8	23	A8	23	A8	23	A8	23	A8	23	A8
24	A8	24	A8	24	A8	24	A8	24	A8	24	A8	24	A8	24	A8	24	A8
25	A8	25	A8	25	A8	25	A8	25	A8	25	A8	25	A8	25	A8	25	A8
26	A8	26	A8	26	A8	26	A8	26	A8	26	A8	26	A8	26	A8	26	A8
27	A8	27	A8	27	A8	27	A8	27	A8	27	A8	27	A8	27	A8	27	A8
28	A8	28	A8	28	A8	28	A8	28	A8	28	A8	28	A8	28	A8	28	A8
29	A8	29	A8	29	A8	29	A8	29	A8	29	A8	29	A8	29	A8	29	A8
30	A8	30	A8	30	A8	30	A8	30	A8	30	A8	30	A8	30	A8	30	A8
31	A8	31	A8	31	A8	31	A8	31	A8	31	A8	31	A8	31	A8	31	A8
32	A8	32	A8	32	A8	32	A8	32	A8	32	A8	32	A8	32	A8	32	A8
33	A8	33	A8	33	A8	33	A8	33	A8	33	A8	33	A8	33	A8	33	A8
34	A8	34	A8	34	A8	34	A8	34	A8	34	A8	34	A8	34	A8	34	A8
35	A8	35	A8	35	A8	35	A8	35	A8	35	A8	35	A8	35	A8	35	A8
36	A8	36	A8	36	A8	36	A8	36	A8	36	A8	36	A8	36	A8	36	A8
37	A8	37	A8	37	A8	37	A8	37	A8	37	A8	37	A8	37	A8	37	A8
38	A8	38	A8	38	A8	38	A8	38	A8	38	A8	38	A8	38	A8	38	A8
39	A8	39	A8	39	A8	39	A8	39	A8	39	A8	39	A8	39	A8	39	A8
40	A8	40	A8	40	A8	40	A8	40	A8	40	A8	40	A8	40	A8	40	A8
41	A8	41	A8	41	A8	41	A8	41	A8	41	A8	41	A8	41	A8	41	A8
42	A8	42	A8	42	A8	42	A8	42	A8	42	A8	42	A8	42	A8	42	A8
43	A8	43	A8	43	A8	43	A8	43	A8	43	A8	43	A8	43	A8	43	A8
44	A8	44	A8	44	A8	44	A8	44	A8	44	A8	44	A8	44	A8	44	A8
45	A8	45	A8	45	A8	45	A8	45	A8	45	A8	45	A8	45	A8	45	A8
46	A8	46	A8	46	A8	46	A8	46	A8	46	A8	46	A8	46	A8	46	A8
47	A8	47	A8	47	A8	47	A8	47	A8	47	A8	47	A8	47	A8	47	A8
48	A8	48	A8	48	A8	48	A8	48	A8	48	A8	48	A8	48	A8	48	A8
49	A8	49	A8	49	A8	49	A8	49	A8	49	A8	49	A8	49	A8	49	A8
50	A8	50	A8	50	A8	50	A8	50	A8	50	A8	50	A8	50	A8	50	A8
51	A8	51	A8	51	A8	51	A8	51	A8	51	A8	51	A8	51	A8	51	A8
52	A8	52	A8	52	A8	52	A8	52	A8	52	A8	52	A8	52	A8	52	A8
53	A8	53	A8	53	A8	53	A8	53	A8	53	A8	53	A8	53	A8	53	A8
54	A8	54	A8	54	A8	54	A8	54	A8	54	A8	54	A8	54	A8	54	A8
55	A8	55	A8	55	A8	55	A8	55	A8	55	A8	55	A8	55	A8	55	A8
56	A8	56	A8	56	A8	56	A8	56	A8	56	A8	56	A8	56	A8	56	A8
57	A8	57	A8	57	A8	57	A8	57	A8	57	A8	57	A8	57	A8	57	A8
58	A8	58	A8	58	A8	58	A8	58	A8	58	A8	58	A8	58	A8	58	A8
59	A8	59	A8	59	A8	59	A8	59	A8	59	A8	59	A8	59	A8	59	A8
60	A8	60	A8	60	A8	60	A8	60	A8	60	A8	60	A8	60	A8	60	A8
61	A8	61	A8	61	A8	61	A8	61	A8	61	A8	61	A8	61	A8	61	A8
62	A8	62	A8	62	A8	62	A8	62	A8	62	A8	62	A8	62	A8	62	A8
63	A8	63	A8	63	A8	63	A8	63	A8	63	A8	63	A8	63	A8	63	A8
64	A8	64	A8	64	A8	64	A8	64	A8	64	A8	64	A8	64	A8	64	A8
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66	A8	66	A8	66	A8	66	A8	66	A8	66	A8	66	A8	66	A8	66	A8
67	A8	67	A8	67	A8	67	A8	67	A8	67	A8	67	A8	67	A8	67	A8
68	A8	68	A8	68	A8	68	A8	68	A8	68	A8	68	A8	68	A8	68	A8
69	A8	69	A8	69	A8	69	A8	69	A8	69	A8	69	A8	69	A8	69	A8
70	A8	70	A8	70	A8	70	A8	70	A8	70	A8	70	A8	70	A8	70	A8
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72	A8	72	A8	72	A8	72	A8	72	A8	72	A8	72	A8	72	A8	72	A8
73	A8	73	A8	73	A8	73	A8	73	A8	73	A8	73	A8	73	A8	73	A8
74	A8	74	A8	74	A8	74	A8	74	A8	74	A8	74	A8	74	A8	74	A8
75	A8	75	A8	75	A8	75	A8	75	A8	75	A8	75	A8	75	A8	75	A8
76	A8	76	A8	76	A8	76	A8	76	A8	76	A8	76	A8	76	A8	76	A8
77	A8	77	A8	77	A8	77	A8	77	A8	77	A8	77	A8	77	A8	77	A8
78	A8	78	A8	78	A8	78	A8	78	A8	78	A8	78	A8	78	A8	78	A8
79	A8	79	A8	79	A8	79	A8	79	A8	79	A8	79	A8	79	A8	79	A8
80	A8	80	A8	80	A8	80	A8	80	A8	80	A8	80	A8	80	A8	80	A8
81	A8	81	A8	81	A8	81	A8	81	A8	81	A8	81	A8	81	A8	81	A8
82	A8	82	A8	82	A8	82	A8	82	A8	82	A8	82	A8	82	A8	82	A8
83	A8	83	A8	83	A8	83	A8	83	A8	83	A8	83	A8	83	A8	83	A8
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85	A8	85	A8	85	A8	85	A8	85	A8	85	A8	85	A8	85	A8	85	A8
86	A8	86	A8	86	A8	86	A8	86	A8	86	A8	86	A8	86	A8	86	A8
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88	A8	88	A8	88	A8	88	A8	88	A8	88	A8	88	A8	88	A8	88	A8
89	A8	89	A8	89	A8	89	A8	89	A8	89	A8	89	A8	89	A8	89	A8
90	A8	90	A8	90	A8	90	A8	90	A8	90	A8	90	A8	90	A8	90	A8
91	A8	91	A8	91	A8	91	A8	91	A8	91	A8	91	A8	91	A8	91	A8
92	A8	92	A8	92	A8	92	A8	92	A8	92	A8	92	A8	92	A8	92	A8
93	A8	93	A8	93	A8	93	A8	93	A8	93	A8	93	A8	93	A8	93	A8
94	A8	94	A8	94	A8	94	A8	94	A8	94	A8	94	A8	94	A8	94	A8
95	A8	95	A8	95	A8	95	A8	95	A8	95	A8	95	A8	95	A8	95	A8
96	A8	96	A8	96	A8	96	A8	96	A8	96	A8	96	A8	96	A8	96	A8
97	A8	97	A8	97	A8	97	A8	97	A8	97	A8	97	A8	97	A8	97	A8
98	A8	98	A8	98	A8	98	A8	98	A8	98	A8	98	A8	98	A8	98	A8
99	A8	99	A8	99	A8	99	A8	99	A8	99	A8	99	A8	99	A8	99	A8
100	A8	100	A8	100	A8	100	A8	100	A8	100	A8	100	A8	100	A8	100	A8

Simultaneous with B4, B5, B6.

Swings 1 and 2 were swings of 4-hour periods and the mean was used as a single swing.

First half swing only.

• First half swing only.

First ball swing only.

Simultaneous with B4, B6, B8.

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pendulum	Portion	Date	Coincidence Interval		Total arc		Temperature	Pressure	Period uncorrected		Corrections (seventh decimal place)						Period corrected		Mean θ
					Chronometer No. 1823	Chronometer No. 1841	Initial	Final			Chronometer No. 1823	Chronometer No. 1841	Arc	Temperature	Pressure	Rate		Flexure	Chronometer No. 1823	Chronometer No. 1841	
No. 70, Gallup, N. Mex., William H. Burger.	1	A4	D	1910	235.46	228.72	mm.	mm.	° C.	mm.	0.5010640	0.5010654	-8	+61	-	-	-	-	-	-	978.166
	2	A4	D	Apr. 1-2	236.62	229.70	4.9	1.5	13.54	65	0.5010640	0.5010654	-9	+110	-	-	-	-	-	-	978.170
	3	A5	D	Apr. 2	235.18	228.70	8.1	1.8	12.37	74	0.5010640	0.5010654	-9	+124	-	-	-	-	-	-	978.169
	4	A5	D	Apr. 2-3	234.60	227.60	8.0	1.7	12.05	54	0.5010640	0.5010654	-9	+127	-	-	-	-	-	-	978.165
	5	A6	D	Apr. 3	234.60	227.60	8.0	1.5	11.96	56	0.5010640	0.5010654	-8	+142	-	-	-	-	-	-	978.164
	6	A6	D	Apr. 3	234.82	228.54	8.1	2.0	11.61	58	0.5010640	0.5010654	-10	+156	-	-	-	-	-	-	978.163
	7	A6	D	Apr. 3-4	238.12	228.56	8.1	1.5	11.27	57	0.5010640	0.5010654	-9	+164	-	-	-	-	-	-	978.176
	8	A6	D	Apr. 4	238.06	227.30	8.2	1.8	11.09	61	0.5010640	0.5010654	-9	+164	-	-	-	-	-	-	978.180
	9	A5	D	Apr. 4	239.28	227.56	8.5	2.0	11.07	63	0.5010640	0.5010654	-11	+146	-	-	-	-	-	-	978.162
No. 71, Las Vegas, N. Mex., William H. Burger.	1	A4	D	1910	243.72	236.14	5.2	2.0	8.81	56	0.5010679	0.5010699	-11	+259	-	-	-	-	-	-	978.203
	2	A4	D	Apr. 12	244.35	236.02	5.2	1.8	8.64	56	0.5010679	0.5010699	-10	+266	-	-	-	-	-	-	978.203
	3	A5	D	Apr. 12	244.58	231.76	5.2	1.8	8.94	60	0.5010679	0.5010699	-10	+254	-	-	-	-	-	-	978.199
	4	A5	D	Apr. 12-13	263.74	230.92	5.3	1.7	9.22	59	0.5010679	0.5010699	-10	+245	-	-	-	-	-	-	978.193
	5	A6	D	Apr. 13	305.89	232.40	5.3	1.7	9.22	59	0.5010679	0.5010699	-10	+245	-	-	-	-	-	-	978.189
	6	A6	D	Apr. 13	307.91	233.78	5.4	1.8	8.73	62	0.5010679	0.5010699	-11	+264	-	-	-	-	-	-	978.205
	7	A6	D	Apr. 13-14	308.90	234.28	5.4	1.9	8.73	60	0.5010679	0.5010699	-11	+264	-	-	-	-	-	-	978.213
	8	A6	D	Apr. 14	309.88	235.36	5.2	1.5	8.38	60	0.5010679	0.5010699	-11	+279	-	-	-	-	-	-	978.213
	9	A5	D	Apr. 14	297.76	233.42	5.3	1.9	8.22	60	0.5010679	0.5010699	-11	+285	-	-	-	-	-	-	978.215
No. 72, Shamrock, Tex., William H. Burger.	1	A4	D	1910	259.38	251.36	5.2	2.1	15.96	63	0.5009657	0.5009685	-11	-40	-	-	-	-	-	-	978.572
	2	A4	D	Apr. 22-23	260.55	253.81	5.4	2.0	15.21	62	0.5009657	0.5009685	-11	-9	-	-	-	-	-	-	978.588
	3	A5	D	Apr. 23	318.04	265.50	5.2	1.7	15.79	65	0.5009657	0.5009685	-10	-34	-	-	-	-	-	-	978.574
	4	A5	D	Apr. 23-24	317.83	265.70	4.9	1.8	16.07	61	0.5009657	0.5009685	-8	+45	-	-	-	-	-	-	978.577
	5	A6	D	Apr. 24	336.08	322.84	4.9	1.5	14.51	70	0.5009657	0.5009685	-8	+21	-	-	-	-	-	-	978.585
	6	A6	D	Apr. 24	334.63	318.70	5.0	1.7	14.72	64	0.5009657	0.5009685	-9	+12	-	-	-	-	-	-	978.581
	1	A4	D	1910	255.13	246.98	5.2	2.1	19.24	57	0.5009680	0.5009740	-11	-178	-	-	-	-	-	-	978.566
	2	A4	D	Apr. 30	254.82	247.48	5.3	2.0	19.09	62	0.5009680	0.5009740	-11	-171	-	-	-	-	-	-	978.567
	3	A5	D	Apr. 30	308.74	295.63	5.2	1.8	19.72	61	0.5009680	0.5009740	-10	-198	-	-	-	-	-	-	978.584
No. 73, Denison, Tex., William H. Burger.	1	A4	D	1910	323.58	311.19	4.9	1.9	19.81	56	0.5008084	0.5008111	-10	-203	-	-	-	-	-	-	978.577
	2	A4	D	Apr. 30-May 1	323.11	311.75	4.7	1.7	20.32	58	0.5008084	0.5008111	-9	-224	-	-	-	-	-	-	978.581
	3	A5	D	May 1	296.70	287.45	5.1	2.3	19.83	54	0.5008084	0.5008111	-11	-202	-	-	-	-	-	-	978.566
	4	A4	D	May 23-24	295.65	286.46	4.8	1.7	20.01	56	0.5008084	0.5008111	-9	-210	-	-	-	-	-	-	978.567
	5	A4	D	May 24	296.35	286.41	4.8	1.7	19.75	63	0.5008084	0.5008111	-9	-199	-	-	-	-	-	-	978.584
	6	A4	D	May 27	297.14	287.14	5.0	2.0	19.49	60	0.5008084	0.5008111	-10	-188	-	-	-	-	-	-	978.577
	7	A5	D	May 24	374.00	358.36	4.8	1.6	20.40	61	0.5008084	0.5008111	-8	-235	-	-	-	-	-	-	978.585
	8	A5	D	May 24-25	372.14	357.48	4.8	1.6	20.54	58	0.5008084	0.5008111	-8	-235	-	-	-	-	-	-	978.581
	9	A5	D	May 26	374.11	359.10	4.8	1.7	20.36	64	0.5008084	0.5008111	-8	-235	-	-	-	-	-	-	978.572
Washington, D. C., Coast and Geodetic Survey Office, William H. Burger.	1	A4	D	1910	372.67	358.20	4.7	1.6	20.12	58	0.5008084	0.5008111	-8	-215	-	-	-	-	-	-	978.567
	2	A4	D	May 25	393.06	376.11	4.8	1.7	20.73	60	0.5008084	0.5008111	-9	-240	-	-	-	-	-	-	978.584
	3	A5	D	May 25	391.86	375.26	4.8	1.8	21.41	60	0.5008084	0.5008111	-9	-269	-	-	-	-	-	-	978.584
	4	A6	D	May 25-26	391.82	375.49	5.0	1.7	21.07	59	0.5008084	0.5008111	-9	-254	-	-	-	-	-	-	978.562
	5	A6	D	May 26	393.06	376.76	4.9	1.7	20.60	61	0.5008084	0.5008111	-8	-235	-	-	-	-	-	-	978.572
	6	A6	D	June 22-23	354.84	341.76	4.7	1.5	18.11	62	0.5008084	0.5008111	-8	-130	-	-	-	-	-	-	978.567
	7	A4	D	June 23	354.44	341.30	4.8	1.7	18.14	59	0.5008084	0.5008111	-8	-132	-	-	-	-	-	-	978.567
	8	A5	D	June 23	471.96	449.18	5.0	1.7	18.75	56	0.5008084	0.5008111	-9	-167	-	-	-	-	-	-	978.584
	9	A5	D	June 23-24	472.95	449.18	5.0	1.7	18.30	60	0.5008084	0.5008111	-9	-138	-	-	-	-	-	-	978.584
No. 57, Iron River, Mich., Harold D. King.	1	A4	D	1910	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	2	A4	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	3	A5	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	4	A5	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	5	A6	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	6	A6	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	7	A6	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	8	A6	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619
	9	A6	D	June 21	505.06	476.72	4.7	1.9	18.10	59	0.5009415	0.5009415	-9	-134	-	-	-	-	-	-	980.619

No. 74. Minneapolis, Minn., Harold D. King.	1	A4	D	July 2-3.....	334.36	324.50	5.5	2.0	25.91	54	5007488	5007716	12	-457	+	11	+	90	-149	-11	5007109	5007098	5007103	980,598 ±0.001
	2	A4	D	July 3.....	337.00	324.04	4.8	1.7	25.92	58	5007486	5007727	-	9	-457	+	90	-149	-11	5007116	5007098	5007112	980,598	
	3	A4	D	July 3.....	337.00	324.04	4.8	1.7	25.92	58	5007486	5007727	-	9	-457	+	90	-149	-11	5007116	5007098	5007112	980,598	
	4	A5	D	July 3-4.....	337.00	324.04	4.8	1.7	25.92	58	5007486	5007727	-	9	-457	+	90	-149	-11	5007116	5007098	5007112	980,598	
	5	A5	D	July 3-4.....	337.00	324.04	4.8	1.7	25.92	58	5007486	5007727	-	9	-457	+	90	-149	-11	5007116	5007098	5007112	980,598	
	6	A6	D	July 4.....	465.44	444.40	4.9	1.7	25.70	56	5005376	5005382	-	9	-448	+	90	-149	-11	5005007	5005024	5005016	980,592	
	1	A4	D	July 11-12.....	311.74	296.76	4.9	1.5	14.63	56	5008302	5008338	-	8	-14	+	7	+58	-261	-	5008197	5008183	5008190	980,173
No. 76. Lead, S. Dak., Harold D. King.	1	A4	D	July 11-12.....	311.74	296.76	4.9	1.5	14.63	56	5008302	5008338	-	8	-14	+	7	+58	-261	-	5008197	5008183	5008190	980,173
	2	A4	D	July 11-12.....	311.74	296.76	4.9	1.5	14.63	56	5008302	5008338	-	8	-14	+	7	+58	-261	-	5008197	5008183	5008190	980,173
	3	A5	D	July 12.....	396.90	372.58	4.8	1.6	14.91	59	5008307	5008349	-	8	-6	+	4	+158	-261	-	5008347	5008343	5008353	980,173
	4	A5	D	July 12-13.....	397.14	373.70	5.0	1.7	14.96	58	5008303	5008349	-	8	-6	+	4	+158	-261	-	5008347	5008343	5008353	980,173
	5	A5	D	July 12-13.....	397.14	373.70	5.0	1.7	14.96	58	5008303	5008349	-	8	-6	+	4	+158	-261	-	5008347	5008343	5008353	980,173
	6	A6	D	July 13.....	418.94	392.38	4.7	1.7	15.15	59	5008373	5008379	-	9	-7	+	7	+159	-261	-	5008683	5008683	5008683	980,167
	1	A4	D	July 19-20.....	346.98	331.80	4.9	1.5	22.60	61	5007215	5007348	-	8	-318	+	3	+135	-185	-	5007020	5007020	5007024	980,629
	2	A4	D	July 20.....	347.26	331.75	5.1	1.7	22.46	56	5007210	5007348	-	8	-318	+	3	+135	-185	-	5007020	5007020	5007024	980,629
	3	A5	D	July 20.....	435.61	430.32	5.3	1.7	22.91	62	5007192	5007348	-	8	-318	+	3	+135	-185	-	5007020	5007020	5007024	980,629
	4	A5	D	July 20-21.....	454.64	430.32	5.3	1.7	22.91	62	5007192	5007348	-	8	-318	+	3	+135	-185	-	5007020	5007020	5007024	980,629
	5	A6	D	July 21.....	481.84	457.58	5.0	1.6	22.89	60	5007192	5007348	-	8	-318	+	3	+135	-185	-	5007020	5007020	5007024	980,629
	6	A6	D	July 21.....	485.05	456.54	5.2	1.9	23.04	53	5005160	5005182	-	11	-337	+	11	+135	-185	-	5005952	5005952	5005952	980,619
	1	A6	D	July 27-28.....	534.06	496.44	5.3	1.7	18.41	65	5005886	5005914	-	10	-185	+	1	+173	-187	-	5005653	5005653	5005653	980,735
No. 77. Hinedale, Mont., Harold D. King.	1	A6	D	July 27-28.....	534.06	496.44	5.3	1.7	18.41	65	5005886	5005914	-	10	-185	+	1	+173	-187	-	5005653	5005653	5005653	980,735
	2	A6	D	July 28.....	538.96	490.83	4.8	1.7	18.71	62	5005912	5005940	-	10	-187	+	1	+173	-187	-	5005653	5005653	5005653	980,735
	3	A5	D	July 28.....	538.96	490.83	4.8	1.7	18.71	62	5005912	5005940	-	10	-187	+	1	+173	-187	-	5005653	5005653	5005653	980,735
	4	A5	D	July 28-29.....	500.78	467.56	5.1	1.8	18.79	60	5005897	5005925	-	10	-187	+	1	+173	-187	-	5005653	5005653	5005653	980,735
	5	A6	D	July 29.....	531.77	496.78	5.1	1.9	18.41	61	5005897	5005925	-	10	-187	+	1	+173	-187	-	5005653	5005653	5005653	980,735
	6	A4	D	July 29.....	532.74	496.78	5.1	1.9	18.41	61	5005897	5005925	-	10	-187	+	1	+173	-187	-	5005653	5005653	5005653	980,735
	1	A4	D	Aug. 3-4.....	365.34	351.76	5.0	1.7	16.28	71	5008582	5008717	-	9	-54	-	0	+130	-160	-	5008603	5008603	5008603	980,680
	2	A4	D	Aug. 4.....	365.34	351.76	5.0	1.7	16.28	71	5008582	5008717	-	9	-54	-	0	+130	-160	-	5008603	5008603	5008603	980,680
	3	A5	D	Aug. 4.....	492.46	461.16	5.0	1.9	16.34	68	5005081	5005392	-	8	-56	+	4	+130	-160	-	5005134	5005134	5005134	980,679
	4	A5	D	Aug. 4-5.....	492.46	461.16	5.0	1.9	16.34	68	5005081	5005392	-	8	-56	+	4	+130	-160	-	5005134	5005134	5005134	980,679
	5	A6	D	Aug. 5.....	527.16	497.59	5.1	1.9	18.61	71	5007547	5007029	-	9	-60	+	2	+130	-160	-	5007190	5007190	5007190	980,679
	6	A6	D	Aug. 5.....	528.74	496.78	4.9	1.9	16.35	62	5007533	5008037	-	8	-57	+	1	+130	-160	-	5007190	5007190	5007190	980,679
	1	A4	D	Aug. 10-11.....	307.73	297.61	5.1	1.8	15.82	63	5008137	5008144	-	9	-147	+	1	+130	-172	-	5008102	5008107	5008107	980,212
	2	A4	D	Aug. 11.....	307.73	297.61	5.1	1.8	15.82	63	5008137	5008144	-	9	-147	+	1	+130	-172	-	5008102	5008107	5008107	980,212
	3	A5	D	Aug. 11.....	307.73	297.61	5.1	1.8	15.82	63	5008137	5008144	-	9	-147	+	1	+130	-172	-	5008102	5008107	5008107	980,212
	4	A5	D	Aug. 11-12.....	391.96	373.38	5.1	1.7	18.61	76	5008386	5008397	-	9	-154	+	11	+130	-172	-	5008330	5008330	5008330	980,215
	5	A6	D	Aug. 12.....	413.44	390.12	4.8	1.8	18.76	75	5008325	5008331	-	9	-154	+	11	+130	-172	-	5008330	5008330	5008330	980,212
	6	A6	D	Aug. 12.....	413.44	390.12	4.8	1.8	18.76	75	5008325	5008331	-	9	-154	+	11	+130	-172	-	5008330	5008330	5008330	980,212
	1	B4	D	Aug. 18-19.....	284.00	260.82	5.3	1.9	25.38	61	5008185	5008436	-	11	-435	+	13	-79	+279	-	1589	1589	1589	980,099
No. 78. Washington, D. C., Bureau of Standards, William H. Burger.	1	B4	D	Aug. 18-19.....	284.00	260.82	5.3	1.9	25.38	61	5008185	5008436	-	11	-435	+	13	-79	+279	-	1589	1589	1589	980,099
	2	B4	D	Aug. 19.....	284.00	260.82	5.3	1.9	25.38	61	5008185	5008436	-	11	-435	+	13	-79	+279	-	1589	1589	1589	980,099
	3	B5	D	Aug. 19-20.....	321.69	316.67	4.9	1.7	25.20	52	5007783	5007427	-	9	-432	+	7	-84	+278	-	5007255	5007265	5007265	980,095
	4	B5	D	Aug. 19-20.....	321.69	316.67	4.9	1.7	25.20	52	5007783	5007427	-	9	-432	+	7	-84	+278	-	5007255	5007265	5007265	980,095
	5	B6	D	Aug. 20.....	329.43	345.14	5.4	2.0	25.02	53	5007000	5007354	-	10	-416	+	10	-88	+266	-	5007079	5007087	5007087	980,095
	6	B6	D	Aug. 20.....	329.43	345.14	5.4	2.0	25.02	53	5007000	5007354	-	10	-416	+	10	-88	+266	-	5007079	5007087	5007087	980,095
	1	A4	D	Aug. 17-18.....	372.25	360.98	5.3	1.7	16.09	60	5007225	5007335	-	10	-71	+	4	+163	-114	-	1823	1823	1823	980,770
	2	A4	D	Aug. 18.....	372.25	360.98	5.3	1.7	16.09	60	5007225	5007335	-	10	-71	+	4	+163	-114	-	1823	1823	1823	980,770
	3	A5	D	Aug. 18.....	508.48	482.28	6.1	1.7	16.28	62	5004924	5005189	-	9	-44	+	2	+163	-114	-	5005021	5005021	5005021	980,720
	4	A5	D	Aug. 18-19.....	508.48	482.28	6.1	1.7	16.28	62	5004924	5005189	-	9	-44	+	2	+163	-114	-	5005021	5005021	5005021	980,720
	5	A6	D	Aug. 19.....	546.75	516.49	5.0	1.9	16.05	58	5004577	5004845	-	10	-49	+	6	+163	-114	-	5004681	5004672	5004672	980,726
	6	A6	D	Aug. 19.....	546.75	516.49	5.0	1.9	16.05	58	5004577	5004845	-	10	-49	+	6	+163	-114	-	5004681	5004672	5004672	980,726
	7	A6	D	Aug. 19-20.....	549.89	513.88	5.3	1.8	15.72	59	5004551	5004806	-	10	-30	+	7	+163	-114	-	5004653	5004653	5004653	980,726
	8	A6	D	Aug. 19-20.....	549.89	513.88	5.3	1.8	15.72	59	5004551	5004806	-	10	-30	+	7	+163	-114	-	5004653	5004653	5004653	980,726
	9	A6	D	Aug. 20.....	511.47	480.20	4.9	1.6	15.56	56	5004582	5004832	-	8	-23	+	4	+163	-114	-	5004683	5004683	5004683	980,726
	10	A5	D	Aug. 20-21.....	511.47	480.20	4.9	1.6	15.56	56	5004582	5004832	-	8	-23	+	4	+163	-114	-	5004683	5004683	5004683	980,726
	11	A5	D	Aug. 21.....	375.35	360.68	4.8	1.7	15.69	58	5004689	5004941	-	9	-31	+	6	+163	-114	-	5005029	5005029	5005029	980,727
	12	A4	D	Aug. 21.....	375.35	360.68	4.8	1.7	15.69	58	5004689	5004941	-	9	-31	+	6	+163	-114	-	5005029	5005029	5005029	980,727
	13	A4	D	Aug. 21-22.....	370.42	361.26	4.9	1.7	15.62	56	5006351	5006330	-	9	-									

• Mean of the two rates.

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pen- du- lum	Date	Coincidence interval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected		Corrections (seventh decimal place)						Period corrected		Mean θ	Dyna
				Chro- no- meter No. 1923	Chro- no- meter No. 1841	Inti- tial	Final			Chrom- eter No. 1841	Chrom- eter No. 1823	Arc	Tem- pera- ture	Rate		Flex- ure	Chrom- eter No. 1823	Chrom- eter No. 1841	Mean		
														Chro- no- meter No. 1823	Chro- no- meter No. 1841						
No. 81. Sloan, Cal., Harold D. King.	1	A4	1910 Aug. 29-30....	292.38	290.38	4.9	1.5	14.80	78	0.5008565	0.5008563	-	8	5	-14	+192	-192	0.5008725	0.5008709	979.967	
	2	A4	Aug. 30....	294.64	292.05	4.8	1.7	14.23	50	0.5008599	0.5008598	-	9	32	+12	+192	-192	0.5008711	0.5008708	979.969	
	3	A5	Aug. 30....	369.51	349.86	4.9	1.7	15.02	60	0.5008775	0.5008775	-	9	1	+3	+192	-192	0.5008915	0.5008914	979.971	±0.001
	4	A5	Aug. 30-31....	368.92	349.38	4.9	1.7	15.13	60	0.5008786	0.5008786	-	9	6	+3	+192	-192	0.5008952	0.5008950	979.972	
	5	A6	Aug. 31....	392.60	369.02	4.9	1.7	14.26	60	0.5008776	0.5008784	-	9	31	+3	+192	-192	0.5008778	0.5008780	979.976	
	6	A6	Aug. 31....	388.76	366.76	4.7	1.7	15.07	61	0.5008439	0.5008526	-	8	3	+3	+192	-192	0.5008607	0.5008608	979.969	
No. 82. Rock Springs, Wyo., Harold D. King.	1	A6	Sept. 7-8....	350.00	331.23	5.0	1.7	16.72	64	0.5007153	0.5007559	-	9	72	0	+157	-272	0.5007218	0.5007165	979.735	
	2	A6	Sept. 8....	350.52	330.80	5.1	1.7	16.69	58	0.5007143	0.5007569	-	9	71	6	+157	-272	0.5007214	0.5007211	979.733	
	3	A5	Sept. 8....	356.40	317.10	5.2	1.9	16.70	61	0.5007465	0.5007906	-11	71	7	+3	+157	-272	0.5007532	0.5007534	979.743	
	4	A5	Sept. 8-9....	354.70	316.72	5.0	1.7	16.63	62	0.5007465	0.5007906	-	9	68	2	+157	-272	0.5007531	0.5007548	979.737	±0.001
	5	A4	Sept. 9....	271.48	259.35	5.0	1.6	16.39	64	0.5008236	0.5008936	8	68	1	+157	-272	0.5008305	0.5008286	979.741		
	6	A4	Sept. 9....	272.62	259.20	5.2	1.9	16.26	62	0.5008157	0.5009664	-11	63	1	+157	-272	0.5008318	0.5009294	979.741		
No. 83. Paxton, Nebr., Harold D. King.	1	A4	Sept. 14-15....	290.44	278.36	5.0	1.2	16.90	69	0.5008973	0.5008987	-	7	80	5	+149	-222	0.5008667	0.5008670	979.986	
	2	A4	Sept. 15....	289.46	278.06	5.0	1.9	17.17	60	0.5008552	0.5009007	-10	91	4	+149	-222	0.5008691	0.5008705	979.980		
	3	A5	Sept. 15....	362.28	343.18	5.1	1.7	17.76	58	0.5008011	0.5007395	-	9	118	7	+149	-222	0.5008929	0.5008942	979.978	
	4	A5	Sept. 15-16....	361.68	343.68	4.9	1.8	18.03	69	0.5008771	0.5007285	-	9	127	5	+149	-222	0.5008926	0.5008930	979.983	
	5	A6	Sept. 16....	380.64	360.89	5.0	1.9	17.87	60	0.5008577	0.5009337	-10	120	4	+149	-222	0.5008577	0.5008579	979.979	±0.001	
	6	A6	Sept. 16....	380.53	359.32	5.1	1.9	18.22	60	0.5008578	0.5008683	-10	135	4	+149	-222	0.5008573	0.5008582	979.979		
No. 85. North Hero, Vt., Harold D. King.	1	A6	Sept. 25-26....	515.18	492.90	4.9	1.7	14.85	56	0.5004557	0.5004832	-	9	6	7	+175	-136	0.5005024	0.5005038	980.581	
	2	A6	Sept. 26....	512.04	486.06	4.9	1.6	14.64	62	0.5004579	0.5004839	-	8	15	7	+175	-136	0.5005024	0.5005024	980.583	
	3	A5	Sept. 26....	460.65	452.51	4.9	1.6	14.59	71	0.5005306	0.5005306	-	8	17	8	+175	-136	0.5005377	0.5005377	980.588	
	4	A5	Sept. 26-27....	460.65	453.08	5.1	1.7	14.65	59	0.5005306	0.5005321	-	8	19	8	+175	-136	0.5005390	0.5005390	980.584	
	5	A4	Sept. 27....	359.38	344.81	5.0	1.7	14.47	60	0.5006946	0.5007261	-	9	22	4	+175	-136	0.5007130	0.5007138	980.581	
	6	A4	Sept. 27....	360.29	343.00	5.1	1.8	14.63	62	0.5006948	0.5007269	-	9	16	5	+175	-136	0.5007160	0.5007160	980.580	
	7	A4	Sept. 27-28....	358.34	343.24	5.2	2.3	14.89	62	0.5006946	0.5007294	-12	5	5	+175	-136	0.5007144	0.5007142	980.589		
Washington, D. C., Coast and Geodetic Survey Office, Har- old D. King-2	1	A4	Oct. 26-27....	301.93	290.16	5.1	2.0	16.88	56	0.5008931	0.5008931	-10	79	7	+149	-194	0.5009346	0.5009346	980.581		
	2	A4	Oct. 27....	301.82	290.02	5.0	1.8	16.76	62	0.5008935	0.5008935	-	9	74	7	+149	-194	0.5009351	0.5009351	980.583	
	3	A4	Oct. 27....	302.36	289.82	5.3	1.9	16.90	60	0.5008932	0.5008941	-10	80	7	+149	-194	0.5009352	0.5009352	980.588		
	4	A4	Oct. 27-28....	301.63	289.78	5.2	1.6	16.90	63	0.5008939	0.5008962	-10	85	7	+149	-194	0.5009355	0.5009360	980.584		
	5	A4	Oct. 28....	301.63	289.78	5.2	1.6	16.90	62	0.5008932	0.5008942	-	9	80	7	+149	-194	0.5009351	0.5009352	980.581	
	6	A4	Oct. 28....	302.60	291.24	5.0	1.7	16.53	58	0.5008935	0.5008969	-	9	69	6	+149	-194	0.5009350	0.5009350	980.580	
	7	A5	Oct. 28-29....	384.57	366.92	5.0	1.7	16.53	58	0.5008935	0.5008905	-	9	64	5	+149	-194	0.5009352	0.5009352	980.581	
	8	A5	Oct. 29....	384.94	367.58	5.1	1.9	16.17	61	0.5008932	0.5008929	-10	49	4	+149	-194	0.5009355	0.5009355	980.587		
	9	A5	Oct. 29....	387.48	366.59	5.2	1.9	15.87	61	0.5008932	0.5008939	-11	36	3	+149	-194	0.5009357	0.5009357	980.584		
	10	A6	Oct. 29....	412.50	392.70	5.1	1.7	14.23	61	0.5008934	0.5008934	-	9	32	2	+149	-194	0.5009355	0.5009355	980.587	
	11	A6	Oct. 29....	412.50	392.70	5.1	1.7	14.23	61	0.5008934	0.5008934	-	9	32	2	+149	-194	0.5009355	0.5009355	980.587	
	12	A6	Oct. 29....	413.69	398.32	5.2	1.7	14.31	62	0.5008935	0.5008930	-10	33	2	+149	-194	0.5009357	0.5009357	980.589		
Washington, D. C., Coast and Geodetic Survey Office, Har- old D. King.	1	B4	Oct. 26-27....	305.58	293.45	4.9	1.9	16.95	56	0.5008935	0.5008935	-	9	82	7	+149	-194	0.5009350	0.5009345	980.581	
	2	B4	Oct. 27....	305.44	293.26	4.9	1.8	17.30	58	0.5008935	0.5008935	-	9	88	7	+149	-194	0.5009354	0.5009344	980.583	
	3	B5	Oct. 27....	340.40	332.69	5.1	1.8	17.30	60	0.5007526	0.5007526	-	9	96	7	+149	-194	0.5007526	0.5007521	980.584	
	4	B5	Oct. 27-28....	348.30	332.06	5.3	1.8	17.32	61	0.5007526	0.5007540	-10	96	7	+149	-194	0.5007526	0.5007528	980.587		
	5	B6	Oct. 28....	358.08	341.50	5.0	1.7	17.32	59	0.5007526	0.5007531	-	9	97	6	+149	-194	0.5007526	0.5007529	980.589	
	6	B6	Oct. 28....	359.62	343.65	4.9	1.7	16.95	59	0.5008962	0.5007285	-	9	82	7	+149	-194	0.5009346	0.5009345	980.589	

No. 98. Vargate Beach, Va., Harold D. King.															No. 99. Durham, N. C., Harold D. King.															No. 100. Fernandina, Fla., Harold King.															No. 101. Wilmer, Ala., Harold D. King.															No. 102. Alceville, Ala., Harold D. King.															No. 103. New Madrid, Mo., Harold King.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1	A4	D	Jan. 10-11.....	292.10	292.45	292.80	5.1	1.8	6.57	76	509573	509548	509523	509498	509473	509448	509423	509398	509373	509348	509323	509298	509273	509248	509223	509198	509173	509148	509123	509098	509073	509048	509023	509000	508975	508950	508925	508900	508875	508850	508825	508800	508775	508750	508725	508700	508675	508650	508625	508600	508575	508550	508525	508500	508475	508450	508425	508400	508375	508350	508325	508300	508275	508250	508225	508200	508175	508150	508125	508100	508075	508050	508025	508000	507975	507950	507925	507900	507875	507850	507825	507800	507775	507750	507725	507700	507675	507650	507625	507600	507575	507550	507525	507500	507475	507450	507425	507400	507375	507350	507325	507300	507275	507250	507225	507200	507175	507150	507125	507100	507075	507050	507025	507000	506975	506950	506925	506900	506875	506850	506825	506800	506775	506750	506725	506700	506675	506650	506625	506600	506575	506550	506525	506500	506475	506450	506425	506400	506375	506350	506325	506300	506275	506250	506225	506200	506175	506150	506125	506100	506075	506050	506025	506000	505975	505950	505925	505900	505875	505850	505825	505800	505775	505750	505725	505700	505675	505650	505625	505600	505575	505550	505525	505500	505475	505450	505425	505400	505375	505350	505325	505300	505275	505250	505225	505200	505175	505150	505125	505100	505075	505050	505025	505000	504975	504950	504925	504900	504875	504850	504825	504800	504775	504750	504725	504700	504675	504650	504625	504600	504575	504550	504525	504500	504475	504450	504425	504400	504375	504350	504325	504300	504275	504250	504225	504200	504175	504150	504125	504100	504075	504050	504025	504000	503975	503950	503925	503900	503875	503850	503825	503800	503775	503750	503725	503700	503675	503650	503625	503600	503575	503550	503525	503500	503475	503450	503425	503400	503375	503350	503325	503300	503275	503250	503225	503200	503175	503150	503125	503100	503075	503050	503025	503000	502975	502950	502925	502900	502875	502850	502825	502800	502775	502750	502725	502700	502675	502650	502625	502600	502575	502550	502525	502500	502475	502450	502425	502400	502375	502350	502325	502300	502275	502250	502225	502200	502175	502150	502125	502100	502075	502050	502025	502000	501975	501950	501925	501900	501875	501850	501825	501800	501775	501750	501725	501700	501675	501650	501625	501600	501575	501550	501525	501500	501475	501450	501425	501400	501375	501350	501325	501300	501275	501250	501225	501200	501175	501150	501125	501100	501075	501050	501025	501000	500975	500950	500925	500900	500875	500850	500825	500800	500775	500750	500725	500700	500675	500650	500625	500600	500575	500550	500525	500500	500475	500450	500425	500400	500375	500350	500325	500300	500275	500250	500225	500200	500175	500150	500125	500100	500075	500050	500025	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	500000	5

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pendulum	Date	Coincidence interval		Total arc	Temperature	Pressure	Period uncorrected		Corrections (seventh decimal places)					Period corrected		Mean θ	
				Chronometer No. 1823	Chronometer No. 1841				Chronometer No. 1823	Chronometer No. 1841	Temperature	Pressure	Rate		Chronometer No. 1823	Chronometer No. 1841	Mean		
													Chronometer No. 1823	Chronometer No. 1841					
No. 96, Mens, Ark., Harold D. King.	1	A5	1911 Mar. 27-28	310.72	314.22	5.2	1.9	16.08	65	0.5008559	0.5007969	-11	-45	2	38	+126	-11	0.5008027	979.538
	2	A5	Mar. 28	310.42	313.12	5.6	2.1	16.12	61	0.5008097	0.5007967	-12	-47	2	38	+126	-11	0.5008046	979.530
	3	A4	Mar. 28	314.14	316.83	5.0	1.0	16.02	59	0.5008336	0.5007533	-10	-68	5	38	+126	-11	0.5008027	979.546
	4	A4	Mar. 28-29	324.52	326.81	5.1	1.8	16.33	64	0.5008841	0.5007532	-10	-60	1	38	+126	-11	0.5007967	979.548
	5	A6	Mar. 29	324.16	327.66	5.2	1.6	16.32	64	0.5007721	0.5007612	-9	-55	1	38	+126	-11	0.5007967	979.553
	6	A6	Mar. 29	322.03	326.31	5.1	2.0	16.78	59	0.5007761	0.5007672	-10	-74	5	38	+126	-11	0.5007708	979.547
No. 97, Nacogdoches, Tex., Harold D. King.	1	A6	Apr. 4-5	307.12	310.72	4.9	1.7	17.98	62	0.5008153	0.5008039	-9	-125	2	22	+118	-10	0.5008034	979.420
	2	A6	Apr. 5	308.13	311.62	5.2	1.9	17.96	62	0.5008127	0.5008035	-11	-124	2	22	+118	-10	0.5008006	979.430
	3	A5	Apr. 5	295.55	298.36	5.0	1.7	17.74	61	0.5008171	0.5008034	-9	-115	3	22	+118	-10	0.5008081	979.422
	4	A5	Apr. 5-6	294.46	298.00	5.1	1.9	18.08	59	0.5008301	0.5008035	-10	-129	6	22	+118	-10	0.5008372	979.421
	5	A4	Apr. 6	244.50	247.21	5.2	1.8	18.06	64	0.5010216	0.5010131	-10	-128	0	22	+118	-10	0.5010104	979.421
	6	A4	Apr. 6	244.77	246.77	5.3	2.0	17.90	57	0.5010234	0.5010151	-11	-122	5	22	+118	-10	0.5010118	979.420
No. 98, Alpine, Tex., Harold D. King.	1	A6	Apr. 10-11	270.85	272.36	4.8	1.5	17.02	61	0.5009218	0.5009196	-8	-85	3	9	+20	-8	0.5009118	979.991
	2	A6	Apr. 11	271.37	272.10	5.0	2.0	16.68	57	0.5009229	0.5009195	-10	-70	2	9	+20	-8	0.5009138	979.983
	3	A5	Apr. 11	261.08	262.70	4.5	1.8	16.96	66	0.5009594	0.5009535	-8	-82	4	9	+20	-8	0.5009585	979.983
	4	A5	Apr. 11-12	261.10	261.92	5.1	2.0	17.03	60	0.5009591	0.5009573	-10	-85	4	9	+20	-8	0.5009581	979.988
	5	A4	Apr. 12	221.20	221.72	5.0	1.8	17.06	65	0.5011328	0.5011301	-9	-86	0	9	+20	-8	0.5011216	979.993
	6	A4	Apr. 12	220.72	221.44	5.3	2.0	17.17	61	0.5011352	0.5011315	-11	-91	3	9	+20	-8	0.5011228	979.987
No. 99, Farwell, Tex., Harold D. King.	1	A6	Apr. 15-16	303.77	305.02	5.0	1.8	12.72	67	0.5008214	0.5008210	-9	+96	4	24	+60	-8	0.5008314	979.299
	2	A6	Apr. 16	303.58	305.01	4.8	1.8	12.70	61	0.5008219	0.5008210	-9	+96	4	24	+60	-8	0.5008312	979.296
	3	A5	Apr. 16	240.44	241.80	5.0	1.9	12.96	70	0.5008231	0.5008232	-10	+85	2	24	+60	-8	0.5008314	979.293
	4	A5	Apr. 16-17	240.66	241.98	4.8	1.9	13.11	65	0.5008616	0.5008577	-10	+79	2	24	+60	-8	0.5008606	979.295
	5	A4	Apr. 17	211.30	212.12	5.0	1.9	13.15	65	0.5010382	0.5010317	-10	+78	2	24	+60	-8	0.5010161	979.287
	6	A4	Apr. 17	211.04	211.57	4.9	1.7	13.30	60	0.5010393	0.5010371	-9	+71	3	24	+60	-8	0.5010474	979.281
No. 100, Guymon, Okla., Harold D. King.	1	A4	Apr. 21-22	251.40	254.04	5.0	1.7	19.01	62	0.5009944	0.5009890	-9	-169	2	17	+48	-10	0.5009722	979.573
	2	A4	Apr. 22	252.32	254.26	5.2	1.9	19.08	62	0.5009927	0.5009852	-11	-171	2	17	+48	-10	0.5009710	979.580
	3	A5	Apr. 22	301.80	307.24	5.2	1.7	19.55	65	0.5008216	0.5008150	-10	-191	1	17	+48	-10	0.5007866	979.573
	4	A5	Apr. 22-23	301.43	307.10	5.4	1.7	19.67	63	0.5008225	0.5008151	-10	-196	1	17	+48	-10	0.5007866	979.572
	5	A6	Apr. 23	318.62	321.26	4.9	1.8	19.59	66	0.5007859	0.5007794	-9	-192	1	17	+48	-10	0.5007630	979.570
	6	A6	Apr. 23	318.72	321.14	5.3	1.8	19.24	61	0.5007836	0.5007797	-9	-177	3	17	+48	-10	0.5007617	979.571
	7	A6	Apr. 23-24	318.78	321.64	5.1	1.7	18.92	60	0.5007835	0.5007785	-9	-171	4	17	+48	-10	0.5007617	979.570
	8	A6	Apr. 24	319.66	322.00	5.1	1.7	18.92	55	0.5007833	0.5007776	-9	-173	5	17	+48	-10	0.5007617	979.571
	9	A5	Apr. 24	301.89	306.96	5.1	1.8	19.21	63	0.5008217	0.5008138	-9	-173	5	17	+48	-10	0.5008010	979.564
	10	A5	Apr. 24-25	301.75	306.77	5.1	1.8	19.14	59	0.5009917	0.5009818	-9	-173	5	17	+48	-10	0.5008010	979.563
	11	A4	Apr. 25	251.83	253.85	4.8	1.8	19.21	64	0.5009917	0.5009819	-9	-173	5	17	+48	-10	0.5007732	979.574
	12	A4	Apr. 25	251.39	252.56	4.7	1.8	19.20	61	0.5009664	0.5009619	-9	-180	4	17	+48	-10	0.500758	979.562
	13	A4	Apr. 25-26	251.25	252.81	5.3	1.5	19.30	61	0.5009370	0.5009307	-9	-180	4	17	+48	-10	0.500758	979.564
	14	A4	Apr. 26	251.56	252.59	4.9	1.9	19.13	62	0.5009558	0.5009517	-9	-186	5	17	+48	-10	0.500758	979.566
	15	A4	Apr. 26	250.90	252.40	4.9	1.8	19.99	58	0.5009596	0.5009525	-9	-209	6	17	+48	-10	0.500751	979.565
No. 101, Helenwood, Tenn., T. L. Warner.	1	A6	May 10-11	345.12	349.36	5.0	1.4	19.69	56	0.5007255	0.5007166	-8	-197	3	19	+94	-11	0.5007059	979.801
	2	A6	May 11	317.54	320.28	4.8	1.5	18.67	61	0.5007201	0.5007117	-8	-185	3	19	+94	-11	0.5007052	979.800
	3	A5	May 11	327.26	330.09	4.9	1.6	19.86	63	0.5007371	0.5007371	-8	-203	3	19	+94	-11	0.5007444	979.785
	4	A5	May 11-12	327.82	331.46	5.0	1.6	19.66	59	0.5007338	0.5007354	-8	-185	3	19	+94	-11	0.5007444	979.785
	5	A4	May 12	266.81	268.66	5.0	1.8	19.12	61	0.5007323	0.5007323	-8	-173	3	19	+94	-11	0.5007223	979.772
	6	A4	May 12	265.26	267.26	4.9	1.6	19.95	60	0.5009443	0.5009372	-8	-207	4	19	+94	-11	0.5009240	979.765

No. 108, Hughes, Tenn., T. L. Warner.	1	A6	D	May 17-18.....	317.16	322.41	4.9	1.6	19.22	62	5007895	5007896	8	177	2	9	122	13	5007690	5007691	5007692	5007693	5007694	5007695	5007696	5007697	5007698	5007699	979.554 ±0.009
	2	A6	D	May 18.....	318.98	323.30	5.1	1.8	18.87	58	5007840	5007841	9	162	3	9	122	13	5007691	5007692	5007693	5007694	5007695	5007696	5007697	5007698	5007699	979.559	
	3	A6	D	May 18.....	305.00	310.36	5.1	1.6	19.34	56	5008210	5008211	8	162	4	9	122	13	5008011	5008012	5008013	5008014	5008015	5008016	5008017	5008018	5008019	5008020	979.569
	4	A5	D	May 18-19.....	305.38	311.48	5.1	1.5	19.00	56	5008200	5008201	8	167	5	9	122	13	5008011	5008012	5008013	5008014	5008015	5008016	5008017	5008018	5008019	5008020	979.548
	5	A4	D	May 19.....	250.66	253.98	5.3	1.8	19.41	56	5008815	5008816	11	169	6	9	122	13	5008811	5008812	5008813	5008814	5008815	5008816	5008817	5008818	5008819	5008820	979.542
	6	A4	D	May 19.....	250.01	253.14	5.3	1.8	19.41	56	5010020	5010021	9	163	7	9	122	13	5008811	5008812	5008813	5008814	5008815	5008816	5008817	5008818	5008819	5008820	979.540
	7	A4	D	May 19-20.....	219.52	252.98	5.1	1.8	19.61	58	5008815	5008816	11	169	8	9	122	13	5008811	5008812	5008813	5008814	5008815	5008816	5008817	5008818	5008819	5008820	979.545
	8	A4	D	May 20.....	219.95	253.08	5.1	2.0	19.66	58	5010022	5010023	10	165	9	9	122	13	5008811	5008812	5008813	5008814	5008815	5008816	5008817	5008818	5008819	5008820	979.545
	9	A5	D	May 20.....	301.24	306.08	5.0	1.5	20.29	58	5008313	5008314	8	222	10	9	122	13	5008807	5008808	5008809	5008810	5008811	5008812	5008813	5008814	5008815	5008816	5008817
No. 104, Charleston, W. Va., T. L. Warner.	1	A6	D	May 26-27.....	357.27	362.48	5.4	1.9	21.64	62	5007008	5007009	11	276	2	8	112	12	5006717	5006718	5006719	5006720	5006721	5006722	5006723	5006724	5006725	5006726	979.934
	2	A6	D	May 27.....	357.60	363.14	5.4	1.9	21.64	60	5007008	5007009	11	270	3	8	112	12	5006717	5006718	5006719	5006720	5006721	5006722	5006723	5006724	5006725	5006726	979.934
	3	A5	D	May 27.....	310.30	315.30	4.9	1.8	21.70	66	5007357	5007358	9	281	4	20	104	12	5007012	5007013	5007014	5007015	5007016	5007017	5007018	5007019	5007020	5007021	979.935
	4	A5	D	May 27-28.....	311.52	316.02	5.0	2.0	21.57	61	5007325	5007326	10	275	5	20	104	12	5007012	5007013	5007014	5007015	5007016	5007017	5007018	5007019	5007020	5007021	979.940
	5	A4	D	May 28.....	276.00	278.31	5.0	1.9	21.59	56	5009074	5009075	10	276	6	20	104	12	5008811	5008812	5008813	5008814	5008815	5008816	5008817	5008818	5008819	5008820	979.935
	6	A4	D	May 28.....	275.84	278.46	5.2	1.7	21.46	56	5009074	5009075	10	271	7	20	104	12	5008811	5008812	5008813	5008814	5008815	5008816	5008817	5008818	5008819	5008820	979.933
No. 105, State College, Pa., T. L. Warner.	1	A6	D	June 8-9.....	382.87	390.01	4.8	1.8	21.29	59	5006538	5006539	9	284	8	8	93	16	5006216	5006217	5006218	5006219	5006220	5006221	5006222	5006223	5006224	5006225	980.123
	2	A6	D	June 9.....	383.92	390.78	5.0	1.9	21.15	57	5006538	5006539	10	278	9	8	93	16	5006216	5006217	5006218	5006219	5006220	5006221	5006222	5006223	5006224	5006225	980.123
	3	A5	D	June 9.....	362.28	367.96	5.4	1.9	21.65	70	5006510	5006511	11	279	10	8	93	16	5006510	5006511	5006512	5006513	5006514	5006515	5006516	5006517	5006518	5006519	980.120
	4	A5	D	June 9-10.....	373.05	378.13	4.9	1.8	21.80	54	5006506	5006507	9	283	11	8	93	16	5006506	5006507	5006508	5006509	5006510	5006511	5006512	5006513	5006514	5006515	980.121
	5	A4	D	June 10.....	290.48	293.12	4.9	1.7	21.76	60	5008322	5008323	9	284	12	8	93	16	5008322	5008323	5008324	5008325	5008326	5008327	5008328	5008329	5008330	5008331	980.126
	6	A4	D	June 10.....	289.55	292.82	5.2	1.9	21.90	60	5008319	5008320	11	286	13	8	93	16	5008319	5008320	5008321	5008322	5008323	5008324	5008325	5008326	5008327	5008328	5008329
Washington, D. C., Coast and Geodetic Survey Office, T. L. Warner.	5	A4	D	June 16.....	289.58	292.38	5.2	1.7	21.57	59	5008448	5008449	10	275	14	14	108	12	5008370	5008371	5008372	5008373	5008374	5008375	5008376	5008377	5008378	5008379	5008380
	6	A4	D	June 16.....	289.08	292.92	5.5	1.9	21.52	59	5008448	5008449	12	273	15	14	108	12	5008370	5008371	5008372	5008373	5008374	5008375	5008376	5008377	5008378	5008379	5008380
	7	A4	D	June 16-17.....	289.52	292.78	5.4	2.3	21.56	57	5008504	5008505	12	275	16	14	108	12	5008504	5008505	5008506	5008507	5008508	5008509	5008510	5008511	5008512	5008513	5008514
	8	A4	D	June 16.....	262.15	266.83	5.0	1.9	21.71	64	5008313	5008314	10	281	17	0	14	108	12	5008313	5008314	5008315	5008316	5008317	5008318	5008319	5008320	5008321	5008322
	9	A5	D	June 15-16.....	263.46	268.48	5.0	1.8	21.60	59	5008358	5008359	9	277	18	5	14	108	12	5008358	5008359	5008360	5008361	5008362	5008363	5008364	5008365	5008366	5008367
	10	A6	D	June 14-15.....	381.61	387.10	5.2	1.9	22.12	58	5006560	5006561	11	298	19	6	14	108	12	5006560	5006561	5006562	5006563	5006564	5006565	5006566	5006567	5006568	5006569
Washington, D. C., Coast and Geodetic Survey Office, T. L. Warner.	1	A6	D	June 15.....	381.68	387.07	5.0	1.8	21.90	57	5006558	5006559	9	289	20	7	14	108	12	5006558	5006559	5006560	5006561	5006562	5006563	5006564	5006565	5006566	5006567
	2	A6	D	June 27-28.....	286.76	290.84	5.2	1.9	23.87	63	5008773	5008774	11	372	21	18	132	12	5008773	5008774	5008775	5008776	5008777	5008778	5008779	5008780	5008781	5008782	5008783
	3	A4	D	June 28.....	286.52	290.50	5.2	1.9	23.88	60	5008773	5008774	11	372	22	18	132	12	5008773	5008774	5008775	5008776	5008777	5008778	5008779	5008780	5008781	5008782	5008783
	4	A5	D	June 28.....	358.72	363.44	4.8	1.8	23.98	67	5009796	5009797	9	376	23	18	132	12	5009796	5009797	5009798	5009799	5009800	5009801	5009802	5009803	5009804	5009805	5009806
	5	A6	D	June 28-29.....	377.16	382.66	5.0	1.9	23.98	62	5009797	5009798	10	376	24	18	132	12	5009797	5009798	5009799	5009800	5009801	5009802	5009803	5009804	5009805	5009806	5009807
	6	A6	D	June 29.....	376.31	381.27	4.9	1.6	23.92	68	5006552	5006553	8	374	25	3	132	12	5006552	5006553	5006554	5006555	5006556	5006557	5006558	5006559	5006560	5006561	5006562
No. 107, Prentice, W. Va., T. L. Warner.	1	A6	D	July 12-13.....	472.70	479.20	4.8	1.8	18.30	56	5005235	5005236	9	178	26	20	54	12	5005124	5005125	5005126	5005127	5005128	5005129	5005130	5005131	5005132	5005133	980.544
	2	A6	D	July 13.....	472.72	479.68	4.9	1.9	18.09	55	5005234	5005235	10	178	27	20	54	12	5005124	5005125	5005126	5005127	5005128	5005129	5005130	5005131	5005132	5005133	980.542
	3	A5	D	July 13.....	443.98	449.92	5.0	2.0	18.00	58	5005237	5005238	10	178	28	20	54	12	5005124	5005125	5005126	5005127	5005128	5005129	5005130	5005131	5005132	5005133	980.542
	4	A5	D	July 13-14.....	445.18	450.45	4.8	1.9	17.90	58	5005237	5005238	10	178	29	20	54	12	5005124	5005125	5005126	5005127	5005128	5005129	5005130	5005131	50051		

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pendulum	Post-position	Date	Coincidence interval		Total arc		Temperature	Period uncorrected		Corrections (seventh decimal place)					Period corrected		θ	Mean θ
					Chronometer No. 1823	Chronometer No. 1841	Initial	Final		Chronometer No. 1823	Chronometer No. 1841	Arc	Temperature	Rate		Chronometer No. 1823	Chronometer No. 1841			
														Chronometer No. 1823	Chronometer No. 1841					
No. 110. Boulder, Mont., T. L. Warner.	1	A6	D	Aug. 7-8	421.90	422.73	5.2	1.8	14.89	0.505937	0.505921	-10	+5	+12	-16	-4	0.505916	0.505912	Dynes	980.255
	2	A6	D	Aug. 8	420.51	421.22	5.1	1.8	14.79	0.505952	0.505942	-10	+5	+12	-16	-4	0.505926	0.505922	980.251	±0.001
	3	A5	D	Aug. 8	395.83	397.08	5.0	1.9	15.11	0.506124	0.506104	-10	+5	+12	-16	-4	0.506092	0.506088	980.249	
	4	A5	D	Aug. 8-9	397.03	398.06	5.0	1.8	15.15	0.506105	0.506085	-10	+5	+12	-16	-4	0.506073	0.506069	980.253	
	5	A5	D	Aug. 9	396.74	399.34	5.2	1.8	14.77	0.506109	0.506089	-10	+5	+12	-16	-4	0.506073	0.506069	980.252	
	6	A4	D	Aug. 9	310.33	310.33	5.4	1.9	15.09	0.506053	0.506033	-11	+4	+3	-16	-4	0.506028	0.506024	980.249	
	7	A4	D	Aug. 9	310.40	310.97	5.2	1.7	15.01	0.506053	0.506033	-11	+4	+3	-16	-4	0.506028	0.506024	980.249	
	8	A4	D	Aug. 9-10	311.64	311.87	5.0	1.9	14.92	0.506053	0.506033	-11	+4	+3	-16	-4	0.506028	0.506024	980.255	
No. 111. Skykomish, Wash., T. L. Warner.	1	A6	D	Aug. 15-16	524.66	532.72	4.9	1.9	14.78	0.506769	0.506767	-10	+9	+3	+6	+81	0.506749	0.506752	980.711	
	2	A6	D	Aug. 16	528.15	536.04	4.9	1.9	14.13	0.506758	0.506748	-10	+9	+3	+6	+81	0.506750	0.506752	980.711	
	3	A5	D	Aug. 16	484.63	493.04	5.0	1.9	15.21	0.506764	0.506766	-10	+9	+3	+6	+81	0.506750	0.506752	980.709	±0.001
	4	A5	D	Aug. 16-17	485.16	492.23	5.0	2.0	15.21	0.506764	0.506766	-10	+9	+3	+6	+81	0.506750	0.506752	980.705	
	5	A4	D	Aug. 17	363.12	366.59	5.2	1.9	15.31	0.506764	0.506766	-11	+13	+6	+6	+81	0.506750	0.506752	980.706	
	6	A4	D	Aug. 17	361.40	365.90	4.9	1.9	15.38	0.506767	0.506767	-11	+24	+1	+6	+81	0.506750	0.506752	980.701	
	1	A6	D	Aug. 21-22	554.84	566.34	5.0	1.4	15.89	0.506767	0.506767	-8	+37	+4	+5	+87	0.506743	0.506743	980.872	
	2	A6	D	Aug. 22	557.97	567.50	5.2	1.4	15.49	0.506767	0.506767	-8	+37	+4	+5	+87	0.506743	0.506743	980.828	
No. 112. Olympia, Wash., T. L. Warner.	1	A6	D	Aug. 22-23	513.66	523.96	5.0	1.9	15.60	0.506767	0.506767	-8	+37	+4	+5	+87	0.506743	0.506743	980.821	
	2	A6	D	Aug. 23	378.36	383.44	5.1	1.7	15.62	0.506767	0.506767	-8	+37	+4	+5	+87	0.506743	0.506743	980.827	
	3	A5	D	Aug. 23	377.43	382.72	5.2	1.9	15.63	0.506767	0.506767	-11	+27	+5	+3	+89	0.506743	0.506743	980.819	
	4	A4	D	Aug. 23	377.43	382.72	5.2	1.9	15.63	0.506767	0.506767	-11	+27	+5	+3	+89	0.506743	0.506743	980.815	
	1	A6	D	Aug. 27-28	444.74	451.22	4.9	1.7	18.52	0.506767	0.506767	-9	+147	+5	-21	+49	0.506743	0.506743	980.436	
	2	A6	D	Aug. 28	445.42	451.22	5.0	1.7	18.52	0.506767	0.506767	-9	+147	+5	-21	+49	0.506743	0.506743	980.436	±0.001
	3	A5	D	Aug. 28	417.28	422.91	4.9	1.9	18.57	0.506767	0.506767	-11	+150	+6	-21	+49	0.506743	0.506743	980.437	
	4	A5	D	Aug. 28-29	418.28	422.91	4.9	1.8	18.01	0.506767	0.506767	-11	+163	+6	-15	+53	0.506743	0.506743	980.431	
No. 113. Happonet, Oreg., T. L. Warner.	1	A6	D	Aug. 29	323.40	327.24	5.0	1.9	18.72	0.506767	0.506767	-10	+151	+10	-15	+53	0.506743	0.506743	980.435	
	2	A6	D	Aug. 29	323.40	327.24	5.0	1.9	18.72	0.506767	0.506767	-10	+151	+10	-15	+53	0.506743	0.506743	980.435	
	1	A6	D	Sept. 6-7	333.10	340.64	5.0	1.7	12.03	0.506767	0.506767	-9	+124	+1	0	+149	0.506743	0.506743	979.592	
	2	A6	D	Sept. 7	334.46	340.64	5.1	1.8	11.55	0.506767	0.506767	-9	+145	+8	0	+149	0.506743	0.506743	979.587	
	3	A5	D	Sept. 7	317.42	324.00	4.9	1.9	12.07	0.506767	0.506767	-10	+123	+4	0	+149	0.506743	0.506743	979.579	
	4	A5	D	Sept. 7-8	318.04	324.00	4.8	1.8	12.15	0.506767	0.506767	-9	+119	+4	0	+149	0.506743	0.506743	979.586	
	5	A4	D	Sept. 8	260.36	263.98	5.3	1.8	11.89	0.506767	0.506767	-10	+130	+4	0	+149	0.506743	0.506743	979.590	
	6	A4	D	Sept. 8	260.36	263.98	5.3	1.8	11.89	0.506767	0.506767	-10	+130	+4	0	+149	0.506743	0.506743	979.587	
No. 114. Truckee, Cal., T. L. Warner.	1	A6	D	Sept. 12-13	354.51	363.92	5.0	1.6	16.01	0.506767	0.506767	-8	+42	+6	-41	+135	0.506743	0.506743	979.846	
	2	A6	D	Sept. 13	356.88	365.58	5.3	1.8	14.91	0.506767	0.506767	-10	+4	+8	-41	+135	0.506743	0.506743	979.846	±0.002
	3	A5	D	Sept. 13	337.24	345.52	5.4	1.8	15.49	0.506767	0.506767	-10	+21	+3	-41	+135	0.506743	0.506743	979.843	
	4	A5	D	Sept. 13-14	339.74	348.53	5.2	1.8	14.99	0.506767	0.506767	-10	+0	+8	-41	+135	0.506743	0.506743	979.846	
	5	A4	D	Sept. 14	276.87	281.72	5.3	2.0	13.44	0.506767	0.506767	-11	+65	+7	-41	+135	0.506743	0.506743	979.846	±0.001
	6	A4	D	Sept. 14	276.87	281.72	5.3	2.0	13.44	0.506767	0.506767	-11	+65	+7	-41	+135	0.506743	0.506743	979.846	
	7	A4	D	Sept. 14	276.87	281.72	5.3	2.0	13.44	0.506767	0.506767	-11	+65	+7	-41	+135	0.506743	0.506743	979.846	
	8	A4	D	Sept. 14	276.87	281.72	5.3	2.0	13.44	0.506767	0.506767	-11	+65	+7	-41	+135	0.506743	0.506743	979.846	
No. 115. Winnemucca, Nev., T. L. Warner.	1	A6	D	Sept. 18-19	316.96	323.90	5.0	1.7	14.99	0.506767	0.506767	-9	+0	+3	-51	+106	0.506743	0.506743	979.507	
	2	A6	D	Sept. 19	316.74	323.90	5.1	1.8	14.97	0.506767	0.506767	-9	+1	+2	-51	+106	0.506743	0.506743	979.504	
	3	A5	D	Sept. 19	301.48	307.48	5.4	2.0	15.63	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.492	±0.002
	4	A5	D	Sept. 19-20	302.50	308.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	
	5	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	
	6	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	±0.002
	7	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	
	8	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	
No. 116. Ely, Nev., T. L. Warner.	1	A6	D	Sept. 18-19	316.96	323.90	5.0	1.7	14.99	0.506767	0.506767	-9	+0	+3	-51	+106	0.506743	0.506743	979.507	
	2	A6	D	Sept. 19	316.74	323.90	5.1	1.8	14.97	0.506767	0.506767	-9	+1	+2	-51	+106	0.506743	0.506743	979.504	
	3	A5	D	Sept. 19	301.48	307.48	5.4	2.0	15.63	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.492	±0.002
	4	A5	D	Sept. 19-20	302.50	308.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	
	5	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	
	6	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	±0.002
	7	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	
	8	A4	D	Sept. 20	249.78	253.32	5.2	1.9	15.62	0.506767	0.506767	-11	+26	+8	-51	+106	0.506743	0.506743	979.503	

No. 117. Guernsey, Wyo., T. L. Warner.	No. 118. Pierre, S. Dak., T. L. Warner.	No. 119. Fort Dodge, Iowa, T. L. Warner.	No. 120. Keithsburg, Ill., T. L. Warner.	No. 121. Grand Rap- ids, Mich., T. L. Warner.	No. 122. Angola, Ind., T. L. Warner.	No. 123. Albany, N. Y., T. L. Warner.	No. 124. Port Jervis, N. Y., T. L. Warner.
1 A6	1 A6	1 A6	1 B4	1 B4	1 B4	1 B4	1 B4
2 A6	2 A6	2 A6	2 B4	2 B4	2 B4	2 B4	2 B4
3 A6	3 A6	3 A6	3 B5	3 B5	3 B5	3 B5	3 B5
4 A6	4 A6	4 A6	4 B6	4 B6	4 B6	4 B6	4 B6
5 A4	5 A4	5 A4	5 B6	5 B6	5 B6	5 B6	5 B6
6 A4	6 A4	6 A4	6 B6	6 B6	6 B6	6 B6	6 B6
7 A4	7 A4	7 A4	7 B6	7 B6	7 B6	7 B6	7 B6
8 A4	8 A4	8 A4	8 B6	8 B6	8 B6	8 B6	8 B6
9 A4	9 A4	9 A4	9 B6	9 B6	9 B6	9 B6	9 B6
10 A4	10 A4	10 A4	10 B6	10 B6	10 B6	10 B6	10 B6
11 A4	11 A4	11 A4	11 B6	11 B6	11 B6	11 B6	11 B6
12 A4	12 A4	12 A4	12 B6	12 B6	12 B6	12 B6	12 B6
13 A4	13 A4	13 A4	13 B6	13 B6	13 B6	13 B6	13 B6
14 A4	14 A4	14 A4	14 B6	14 B6	14 B6	14 B6	14 B6
15 A4	15 A4	15 A4	15 B6	15 B6	15 B6	15 B6	15 B6
16 A4	16 A4	16 A4	16 B6	16 B6	16 B6	16 B6	16 B6
17 A4	17 A4	17 A4	17 B6	17 B6	17 B6	17 B6	17 B6
18 A4	18 A4	18 A4	18 B6	18 B6	18 B6	18 B6	18 B6
19 A4	19 A4	19 A4	19 B6	19 B6	19 B6	19 B6	19 B6
20 A4	20 A4	20 A4	20 B6	20 B6	20 B6	20 B6	20 B6
21 A4	21 A4	21 A4	21 B6	21 B6	21 B6	21 B6	21 B6
22 A4	22 A4	22 A4	22 B6	22 B6	22 B6	22 B6	22 B6
23 A4	23 A4	23 A4	23 B6	23 B6	23 B6	23 B6	23 B6
24 A4	24 A4	24 A4	24 B6	24 B6	24 B6	24 B6	24 B6
25 A4	25 A4	25 A4	25 B6	25 B6	25 B6	25 B6	25 B6
26 A4	26 A4	26 A4	26 B6	26 B6	26 B6	26 B6	26 B6
27 A4	27 A4	27 A4	27 B6	27 B6	27 B6	27 B6	27 B6
28 A4	28 A4	28 A4	28 B6	28 B6	28 B6	28 B6	28 B6
29 A4	29 A4	29 A4	29 B6	29 B6	29 B6	29 B6	29 B6
30 A4	30 A4	30 A4	30 B6	30 B6	30 B6	30 B6	30 B6
31 A4	31 A4	31 A4	31 B6	31 B6	31 B6	31 B6	31 B6
32 A4	32 A4	32 A4	32 B6	32 B6	32 B6	32 B6	32 B6
33 A4	33 A4	33 A4	33 B6	33 B6	33 B6	33 B6	33 B6
34 A4	34 A4	34 A4	34 B6	34 B6	34 B6	34 B6	34 B6
35 A4	35 A4	35 A4	35 B6	35 B6	35 B6	35 B6	35 B6
36 A4	36 A4	36 A4	36 B6	36 B6	36 B6	36 B6	36 B6
37 A4	37 A4	37 A4	37 B6	37 B6	37 B6	37 B6	37 B6
38 A4	38 A4	38 A4	38 B6	38 B6	38 B6	38 B6	38 B6
39 A4	39 A4	39 A4	39 B6	39 B6	39 B6	39 B6	39 B6
40 A4	40 A4	40 A4	40 B6	40 B6	40 B6	40 B6	40 B6
41 A4	41 A4	41 A4	41 B6	41 B6	41 B6	41 B6	41 B6
42 A4	42 A4	42 A4	42 B6	42 B6	42 B6	42 B6	42 B6
43 A4	43 A4	43 A4	43 B6	43 B6	43 B6	43 B6	43 B6
44 A4	44 A4	44 A4	44 B6	44 B6	44 B6	44 B6	44 B6
45 A4	45 A4	45 A4	45 B6	45 B6	45 B6	45 B6	45 B6
46 A4	46 A4	46 A4	46 B6	46 B6	46 B6	46 B6	46 B6
47 A4	47 A4	47 A4	47 B6	47 B6	47 B6	47 B6	47 B6
48 A4	48 A4	48 A4	48 B6	48 B6	48 B6	48 B6	48 B6
49 A4	49 A4	49 A4	49 B6	49 B6	49 B6	49 B6	49 B6
50 A4	50 A4	50 A4	50 B6	50 B6	50 B6	50 B6	50 B6
51 A4	51 A4	51 A4	51 B6	51 B6	51 B6	51 B6	51 B6
52 A4	52 A4	52 A4	52 B6	52 B6	52 B6	52 B6	52 B6
53 A4	53 A4	53 A4	53 B6	53 B6	53 B6	53 B6	53 B6
54 A4	54 A4	54 A4	54 B6	54 B6	54 B6	54 B6	54 B6
55 A4	55 A4	55 A4	55 B6	55 B6	55 B6	55 B6	55 B6
56 A4	56 A4	56 A4	56 B6	56 B6	56 B6	56 B6	56 B6
57 A4	57 A4	57 A4	57 B6	57 B6	57 B6	57 B6	57 B6
58 A4	58 A4	58 A4	58 B6	58 B6	58 B6	58 B6	58 B6
59 A4	59 A4	59 A4	59 B6	59 B6	59 B6	59 B6	59 B6
60 A4	60 A4	60 A4	60 B6	60 B6	60 B6	60 B6	60 B6
61 A4	61 A4	61 A4	61 B6	61 B6	61 B6	61 B6	61 B6
62 A4	62 A4	62 A4	62 B6	62 B6	62 B6	62 B6	62 B6
63 A4	63 A4	63 A4	63 B6	63 B6	63 B6	63 B6	63 B6
64 A4	64 A4	64 A4	64 B6	64 B6	64 B6	64 B6	64 B6
65 A4	65 A4	65 A4	65 B6	65 B6	65 B6	65 B6	65 B6
66 A4	66 A4	66 A4	66 B6	66 B6	66 B6	66 B6	66 B6
67 A4	67 A4	67 A4	67 B6	67 B6	67 B6	67 B6	67 B6
68 A4	68 A4	68 A4	68 B6	68 B6	68 B6	68 B6	68 B6
69 A4	69 A4	69 A4	69 B6	69 B6	69 B6	69 B6	69 B6
70 A4	70 A4	70 A4	70 B6	70 B6	70 B6	70 B6	70 B6
71 A4	71 A4	71 A4	71 B6	71 B6	71 B6	71 B6	71 B6
72 A4	72 A4	72 A4	72 B6	72 B6	72 B6	72 B6	72 B6
73 A4	73 A4	73 A4	73 B6	73 B6	73 B6	73 B6	73 B6
74 A4	74 A4	74 A4	74 B6	74 B6	74 B6	74 B6	74 B6
75 A4	75 A4	75 A4	75 B6	75 B6	75 B6	75 B6	75 B6
76 A4	76 A4	76 A4	76 B6	76 B6	76 B6	76 B6	76 B6
77 A4	77 A4	77 A4	77 B6	77 B6	77 B6	77 B6	77 B6
78 A4	78 A4	78 A4	78 B6	78 B6	78 B6	78 B6	78 B6
79 A4	79 A4	79 A4	79 B6	79 B6	79 B6	79 B6	79 B6
80 A4	80 A4	80 A4	80 B6	80 B6	80 B6	80 B6	80 B6
81 A4	81 A4	81 A4	81 B6	81 B6	81 B6	81 B6	81 B6
82 A4	82 A4	82 A4	82 B6	82 B6	82 B6	82 B6	82 B6
83 A4	83 A4	83 A4	83 B6	83 B6	83 B6	83 B6	83 B6
84 A4	84 A4	84 A4	84 B6	84 B6	84 B6	84 B6	84 B6
85 A4	85 A4	85 A4	85 B6	85 B6	85 B6	85 B6	85 B6
86 A4	86 A4	86 A4	86 B6	86 B6	86 B6	86 B6	86 B6
87 A4	87 A4	87 A4	87 B6	87 B6	87 B6	87 B6	87 B6
88 A4	88 A4	88 A4	88 B6	88 B6	88 B6	88 B6	88 B6
89 A4	89 A4	89 A4	89 B6	89 B6	89 B6	89 B6	89 B6
90 A4	90 A4	90 A4	90 B6	90 B6	90 B6	90 B6	90 B6
91 A4	91 A4	91 A4	91 B6	91 B6	91 B6	91 B6	91 B6
92 A4	92 A4	92 A4	92 B6	92 B6	92 B6	92 B6	92 B6
93 A4	93 A4	93 A4	93 B6	93 B6	93 B6	93 B6	93 B6
94 A4	94 A4	94 A4	94 B6	94 B6	94 B6	94 B6	94 B6
95 A4	95 A4	95 A4	95 B6	95 B6	95 B6	95 B6	95 B6
96 A4	96 A4	96 A4	96 B6	96 B6	96 B6	96 B6	96 B6
97 A4	97 A4	97 A4	97 B6	97 B6	97 B6	97 B6	97 B6
98 A4	98 A4	98 A4	98 B6	98 B6	98 B6	98 B6	98 B6
99 A4	99 A4	99 A4	99 B6	99 B6	99 B6	99 B6	99 B6
100 A4	100 A4	100 A4	100 B6	100 B6	100 B6	100 B6	100 B6

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pen-Post-lum	Date	Coincidence interval		Total arc		Temperature ° C.	Period uncorrected		Corrections (seventh decimal place)					Period corrected		Mean θ	Dynes
				Chronometer No. 1823	Chronometer No. 1841	Initial	Final		Chronometer No. 1823	Chronometer No. 1841	Arc	Temperature	Rate		Flexure	Chronometer No. 1823	Chronometer No. 1841		
													Chronometer No. 1823	Chronometer No. 1841					
Washington, D. C., Coast and Geodetic Survey Office, T. L. Warner.	1 A6	D	1912 Jan. 13-14	440.82	461.92	mm. 3.2	mm. 1.7	3.70	0.5005678	0.5005430	-10	+475	+148	+400	8	0.5006285	0.5006289	5006289	
	2 A6	D	Jan. 14	445.72	466.35	3.5	1.8	2.45	0.5005678	0.5005430	-9	+526	+148	+400	8	0.5006273	0.5006277	5006278	
	3 A6	D	Jan. 14	445.74	466.38	4.0	1.8	1.94	0.5005678	0.5005430	-9	+547	+148	+400	8	0.5006297	0.5006278	5006298	
	4 A6	D	Jan. 14-15	447.28	468.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+537	+148	+400	8	0.5006283	0.5006282	5006282	
	5 A6	D	Jan. 15	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+504	+148	+400	8	0.5006321	0.5006308	5006310	
	6 A6	D	Jan. 15	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+504	+148	+400	8	0.5006321	0.5006308	5006310	
	7 A6	D	Jan. 15-16	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	8 A6	D	Jan. 16	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	9 A6	D	Jan. 16	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	10 A6	D	Jan. 16-17	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	11 A6	D	Jan. 17	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	12 A6	D	Jan. 17	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	13 A6	D	Jan. 17-18	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	14 A6	D	Jan. 18	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
	15 A6	D	Jan. 18	448.28	469.68	4.0	1.9	2.19	0.5005678	0.5005430	-9	+475	+148	+400	8	0.5006321	0.5006308	5006310	
Washington, D. C., Coast and Geodetic Survey Office, T. L. Warner.	1 B4	D	1912 Jan. 13-14	331.35	342.55	5.1	1.5	4.52	0.5007556	0.5007300	-8	+439	+148	+400	8	0.5008122	0.5008127	5008124	
	2 B4	D	Jan. 14	331.35	342.55	5.1	1.5	4.52	0.5007556	0.5007300	-8	+439	+148	+400	8	0.5008122	0.5008127	5008124	
	3 B4	D	Jan. 14	331.35	342.55	5.1	1.5	4.52	0.5007556	0.5007300	-8	+439	+148	+400	8	0.5008122	0.5008127	5008124	
	4 B4	D	Jan. 14-15	335.38	346.58	5.0	1.7	3.10	0.5007556	0.5007300	-9	+508	+148	+400	8	0.5008141	0.5008141	5008141	
	5 B4	D	Jan. 15	335.38	346.58	5.0	1.7	3.10	0.5007556	0.5007300	-9	+508	+148	+400	8	0.5008141	0.5008141	5008141	
	6 B4	D	Jan. 15	335.38	346.58	5.0	1.7	3.10	0.5007556	0.5007300	-9	+508	+148	+400	8	0.5008141	0.5008141	5008141	
	7 B4	D	Jan. 15-16	331.01	343.01	5.2	1.7	3.73	0.5007556	0.5007300	-9	+438	+148	+400	8	0.5008118	0.5008118	5008118	
	8 B4	D	Jan. 16	331.01	343.01	5.2	1.7	3.73	0.5007556	0.5007300	-9	+438	+148	+400	8	0.5008118	0.5008118	5008118	
	9 B4	D	Jan. 16	331.01	343.01	5.2	1.7	3.73	0.5007556	0.5007300	-9	+438	+148	+400	8	0.5008118	0.5008118	5008118	
	10 B4	D	Jan. 16	331.01	343.01	5.2	1.7	3.73	0.5007556	0.5007300	-9	+438	+148	+400	8	0.5008118	0.5008118	5008118	
	11 B4	D	Jan. 16-17	335.55	347.55	5.2	1.9	4.46	0.5007556	0.5007300	-11	+442	+148	+400	8	0.5008163	0.5008163	5008163	
	12 B4	D	Jan. 17	335.55	347.55	5.2	1.9	4.46	0.5007556	0.5007300	-11	+442	+148	+400	8	0.5008163	0.5008163	5008163	
	13 B4	D	Jan. 17	335.55	347.55	5.2	1.9	4.46	0.5007556	0.5007300	-11	+442	+148	+400	8	0.5008163	0.5008163	5008163	
	14 B4	D	Jan. 17-18	335.55	347.55	5.2	1.9	4.46	0.5007556	0.5007300	-11	+442	+148	+400	8	0.5008163	0.5008163	5008163	
	15 B4	D	Jan. 18	335.55	347.55	5.2	1.9	4.46	0.5007556	0.5007300	-11	+442	+148	+400	8	0.5008163	0.5008163	5008163	
Washington, D. C., Coast and Geodetic Survey Office, John D. Powell.	1 B4	D	1914 July 8-9	1838	3477	4.4	1.7	22.02	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	2 B4	D	July 9	1838	3477	4.4	1.7	22.02	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	3 B4	D	July 9	1838	3477	4.4	1.7	22.02	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	4 B4	D	July 9-10	316.34	326.34	4.8	1.9	22.12	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	5 B4	D	July 10	316.34	326.34	4.8	1.9	22.12	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	6 B4	D	July 10	316.34	326.34	4.8	1.9	22.12	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	7 B4	D	July 10-11	335.13	345.13	4.9	2.0	22.42	0.5007900	0.5007644	-10	+312	+148	+400	11	0.5008144	0.5008144	5008144	
	8 B4	D	July 11	335.13	345.13	4.9	2.0	22.42	0.5007900	0.5007644	-10	+312	+148	+400	11	0.5008144	0.5008144	5008144	
	9 B4	D	July 11	335.13	345.13	4.9	2.0	22.42	0.5007900	0.5007644	-10	+312	+148	+400	11	0.5008144	0.5008144	5008144	
Washington, D. C., Coast and Geodetic Survey Office, John D. Powell.	1 B4	D	1914 July 21	1838	3477	4.4	1.7	22.02	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	2 B4	D	July 21	1838	3477	4.4	1.7	22.02	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	3 B4	D	July 21-22	316.34	326.34	4.8	1.9	22.12	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	4 B4	D	July 22	316.34	326.34	4.8	1.9	22.12	0.5007900	0.5007644	-8	+294	+148	+400	11	0.5008144	0.5008144	5008144	
	5 B4	D	July 22-23	335.13	345.13	4.9	2.0	22.42	0.5007900	0.5007644	-10	+312	+148	+400	11	0.5008144	0.5008144	5008144	
	6 B4	D	July 23	335.13	345.13	4.9	2.0	22.42	0.5007900	0.5007644	-10	+312	+148	+400	11	0.5008144	0.5008144	5008144	
	7 B4	D	July 23	335.13	345.13	4.9	2.0	22.42	0.5007900	0.5007644	-10	+312	+148	+400	11	0.5008144	0.5008144	5008144	

- Chronometer rates were determined by star observations.
- Chronometer 3477 failed to break for the last day's observations.
- Chronometer rates were determined from Western Union noon signals.

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pen- dulum	Post- tion	Date	Coincidence interval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected		Corrections (seventh decimal place)						Period corrected		Mean g	
					Chro- no- meter No. 1823	Chro- no- meter No. 1841	Initial	Final			Chromom- eter No. 1823	Chromom- eter No. 1841	Arc	Tem- pera- ture	Pres- sure	Rate		Chromom- eter No. 1823	Chromom- eter No. 1841	Flex- ure		Chronom- eter No. 1841
No. 143, Hot Springs, Ark., John D. Pow- ell.	1	B6	D	Nov. 4, 1914	283.84	296.42	4.8	1.6	17.32	62	0.500523	0.500448	— 8	— 97	2	— 209	— 142	— 7	0.500520	0.500508	799.651	
	2	B6	D	Nov. 4, 1914	283.54	296.02	4.8	1.5	17.35	79	0.500531	0.500456	— 8	— 98	2	— 209	— 142	— 7	0.500519	0.500507	799.654	
	3	B6	D	Nov. 5, 1914	285.08	297.10	4.9	1.7	17.25	62	0.500537	0.500459	— 9	— 94	2	— 209	— 142	— 7	0.500517	0.500510	799.661	
	4	B5	D	Nov. 5, 1914	287.56	290.74	5.0	2.0	17.48	55	0.500530	0.500454	— 10	— 104	5	— 216	— 136	— 7	0.500530	0.500515	799.661	
	5	B5	D	Nov. 5, 1914	287.42	290.10	4.4	1.4	17.48	69	0.500533	0.500453	— 7	— 104	5	— 216	— 136	— 7	0.500534	0.500517	799.660	
	6	B5	D	Nov. 6, 1914	288.75	290.77	5.2	1.9	17.35	59	0.500573	0.500493	— 11	— 98	5	— 216	— 136	— 7	0.500546	0.500516	799.667	
No. 142, Texarkana, Ark., John D. Pow- ell.	1	B6	D	Nov. 11, 1914	277.68	290.74	5.2	2.2	24.75	40	0.500620	0.500502	— 12	— 409	22	— 220	— 136	— 5	0.500581	0.500581	799.579	
	2	B6	D	Nov. 11, 1914	278.23	291.74	5.1	1.8	24.60	46	0.500601	0.500529	— 9	— 402	22	— 220	— 136	— 5	0.500572	0.500564	799.587	
	3	B6	D	Nov. 12, 1914	277.72	279.82	5.5	2.0	25.15	53	0.500618	0.500550	— 12	— 425	22	— 220	— 136	— 5	0.500584	0.500571	799.584	
	4	B5	D	Nov. 12, 1914	271.56	273.95	5.4	2.0	25.52	54	0.500623	0.500542	— 11	— 441	22	— 220	— 145	— 5	0.500581	0.500551	799.589	
	5	B5	D	Nov. 12, 1914	271.26	273.22	5.7	1.7	25.68	65	0.500633	0.500559	— 12	— 417	22	— 220	— 145	— 5	0.500559	0.500536	799.589	
	6	B5	D	Nov. 13, 1914	271.08	272.91	5.3	1.7	25.85	75	0.500640	0.500577	— 10	— 455	9	— 216	— 145	— 5	0.500545	0.500533	799.592	
No. 144, Alexandria, La., John D. Powell.	1	B6	D	Nov. 18, 1914	270.02	272.46	4.9	1.9	21.75	53	0.500675	0.500593	— 10	— 283	11	— 212	— 138	— 6	0.500677	0.500707	799.428	
	2	B6	D	Nov. 18, 1914	269.83	271.90	4.9	1.6	21.90	63	0.500682	0.500602	— 8	— 259	11	— 212	— 138	— 6	0.500670	0.500710	799.428	
	3	B6	D	Nov. 19, 1914	269.96	271.88	4.4	1.5	21.90	71	0.500678	0.500598	— 7	— 259	6	— 212	— 138	— 6	0.500678	0.500706	799.429	
	4	B5	D	Nov. 19, 1914	263.69	266.74	5.1	1.8	22.05	57	0.500699	0.500619	— 9	— 245	7	— 220	— 122	— 6	0.500676	0.500707	799.427	
	5	B5	D	Nov. 19, 1914	263.26	266.20	5.2	1.5	22.25	50	0.500615	0.500535	— 9	— 204	0	— 220	— 122	— 6	0.500592	0.500702	799.432	
	6	B5	D	Nov. 20, 1914	264.01	268.11	5.5	1.9	22.12	60	0.500637	0.500557	— 11	— 228	0	— 220	— 122	— 6	0.500632	0.500705	799.429	
No. 145, Laurel, Miss., John D. Powell.	1	B6	D	Nov. 24, 1914	278.80	281.80	5.8	1.9	16.20	49	0.500683	0.500603	— 12	— 50	14	— 218	— 134	— 5	0.500672	0.500710	799.453	
	2	B6	D	Nov. 24, 1914	279.56	282.21	5.3	1.8	16.48	54	0.500659	0.500579	— 10	— 62	9	— 218	— 134	— 5	0.500673	0.500707	799.456	
	3	B6	D	Nov. 25, 1914	281.06	284.12	5.0	2.0	16.15	59	0.500611	0.500531	— 10	— 48	4	— 218	— 134	— 5	0.500634	0.500702	799.478	
	4	B5	D	Nov. 25, 1914	272.24	274.90	5.0	1.9	17.12	49	0.500600	0.500520	— 10	— 80	4	— 207	— 127	— 5	0.500594	0.500704	799.455	
	5	B5	D	Nov. 25, 1914	273.30	275.68	5.3	1.8	16.92	53	0.500604	0.500524	— 10	— 80	4	— 207	— 127	— 5	0.500572	0.500704	799.465	
	6	B5	D	Nov. 26, 1914	275.29	277.32	5.1	1.8	16.00	58	0.500608	0.500528	— 9	— 42	5	— 207	— 127	— 5	0.500580	0.500705	799.475	
Washington, D. C., Coast and Geodetic Survey Office, John D. Powell.	1	B4	D	Jan. 7, 1915	299.61	302.02	4.8	1.4	14.22	66	0.500658	0.500578	— 8	— 33	3	— 177	— 122	— 8	0.500613	0.500701	799.854	
	2	B4	D	Jan. 7, 1915	301.76	304.00	4.7	1.7	13.32	53	0.500628	0.500548	— 8	— 70	7	— 177	— 122	— 8	0.500618	0.500701	799.859	
	3	B4	D	Jan. 8, 1915	303.52	305.86	4.6	2.0	12.70	55	0.500630	0.500550	— 9	— 96	7	— 177	— 122	— 8	0.500618	0.500701	799.859	
	10	B4	D	Jan. 12, 1915	305.98	307.80	5.1	2.0	11.42	52	0.500619	0.500539	— 10	— 102	10	— 161	— 115	— 8	0.500618	0.500701	799.859	
	11	B4	D	Jan. 12, 1915	301.90	304.30	5.3	1.9	11.48	60	0.500623	0.500543	— 11	— 117	6	— 161	— 115	— 8	0.500617	0.500701	799.859	
	12	B4	D	Jan. 13, 1915	304.63	307.00	5.2	1.8	11.40	63	0.500620	0.500540	— 10	— 131	6	— 161	— 115	— 8	0.500617	0.500701	799.859	
	4	B5	D	Jan. 8, 1915	342.60	345.70	5.5	1.9	12.60	58	0.500608	0.500528	— 12	— 101	5	— 166	— 118	— 8	0.500628	0.500719	799.859	
	5	B5	D	Jan. 9, 1915	341.01	344.11	5.5	2.0	12.28	58	0.500624	0.500544	— 12	— 114	4	— 166	— 118	— 8	0.500620	0.500721	799.859	
	6	B5	D	Jan. 9, 1915	343.74	346.84	4.8	2.0	11.75	61	0.500621	0.500541	— 10	— 128	4	— 166	— 118	— 8	0.500618	0.500721	799.859	
	7	B6	D	Jan. 11, 1915	337.04	339.76	5.0	1.8	10.75	54	0.500702	0.500622	— 9	— 178	3	— 145	— 107	— 8	0.500702	0.500729	799.859	
	8	B6	D	Jan. 11, 1915	336.95	339.12	5.4	1.6	10.68	76	0.500701	0.500621	— 9	— 181	3	— 145	— 107	— 8	0.500701	0.500729	799.859	
	9	B6	D	Jan. 12, 1915	337.91	339.26	5.4	2.1	10.62	59	0.500695	0.500615	— 11	— 184	3	— 145	— 107	— 8	0.500702	0.500729	799.859	
No. 146, Richmond, Va., John D. Powell.	4	B5	D	Feb. 10, 1915	310.56	315.06	4.7	1.7	20.35	48	0.500693	0.500613	— 8	— 224	15	— 218	— 120	— 7	0.500704	0.500762	799.854	
	5	B5	D	Feb. 10, 1915	310.99	315.19	5.6	2.1	20.35	49	0.500690	0.500610	— 12	— 224	14	— 218	— 120	— 7	0.500705	0.500762	799.859	
	6	B5	D	Feb. 11, 1915	311.84	316.04	5.5	2.4	20.35	48	0.500690	0.500610	— 14	— 224	14	— 218	— 120	— 7	0.500700	0.500762	799.859	
	7	B6	D	Feb. 11, 1915	317.69	322.41	5.8	2.2	20.42	48	0.500781	0.500701	— 13	— 228	15	— 231	— 131	— 7	0.500703	0.500762	799.859	
	8	B6	D	Feb. 11, 1915	318.46	322.74	3.7	1.4	20.45	49	0.500783	0.500703	— 6	— 228	14	— 231	— 131	— 7	0.500705	0.500762	799.859	
	9	B6	D	Feb. 12, 1915	319.24	322.22	3.9	1.8	20.48	49	0.500783	0.500703	— 7	— 230	14	— 231	— 131	— 7	0.500710	0.500762	799.854	

No. 147. Emporia, Va., John D. Powell.										979.808 ± 0.001											
1	B5	D	Feb. 24	315.32	317.47	4.2	1.5	14.85	52	5007941	5007887	7	+ 29	+ 11	- 166	- 126	7	5007778	5007761	5007771	979.801
2	B5	D	Feb. 24-25	315.95	317.71	5.7	1.6	14.30	67	5007925	5007881	7	+ 32	+ 4	- 166	- 124	7	5007761	5007763	5007765	979.802
3	B5	D	Feb. 25	318.48	319.62	5.6	2.3	13.75	65	5007834	5007806	7	+ 31	+ 2	- 166	- 126	7	5007755	5007757	5007759	979.803
4	B6	D	Feb. 25	327.98	329.62	5.9	1.9	12.82	65	5007834	5007806	7	+ 32	+ 2	- 166	- 126	7	5007755	5007757	5007759	979.802
5	B6	D	Feb. 25-26	329.72	331.00	4.9	1.2	11.88	77	5007904	5007861	7	+ 31	+ 14	- 132	- 105	7	5007762	5007764	5007766	979.804
6	B6	D	Feb. 26	333.08	333.44	5.8	2.2	10.75	66	5007917	5007869	7	+ 178	- 4	- 132	- 105	7	5007758	5007760	5007762	979.805
No. 148. Greenville, N. C., John D. Pow- ell.										979.787 ± 0.001											
1	B5	D	Mar. 9	298.19	300.95	5.7	1.9	17.76	56	5008308	5008221	12	- 115	+ 7	- 222	- 163	8	5008300	5008302	5008304	979.787
2	B5	D	Mar. 9-10	298.30	300.76	5.7	1.9	17.90	57	5008326	5008239	12	- 121	+ 6	- 222	- 163	8	5008311	5008313	5008315	979.788
3	B5	D	Mar. 10	298.32	300.78	6.2	2.0	17.90	58	5008341	5008254	12	- 121	+ 6	- 222	- 163	8	5008326	5008328	5008330	979.789
4	B6	D	Mar. 10	301.27	306.54	5.0	1.9	18.02	58	5008250	5008163	10	- 126	+ 3	- 222	- 172	8	5008254	5008256	5008258	979.790
5	B6	D	Mar. 10-11	301.38	306.54	4.9	1.6	18.08	58	5008250	5008163	10	- 126	+ 3	- 222	- 172	8	5008254	5008256	5008258	979.790
6	B6	D	Mar. 11	301.81	306.12	4.6	1.8	18.45	59	5008216	5008129	8	- 137	+ 5	- 225	- 172	8	5008216	5008218	5008220	979.791
7	B6	D	Mar. 11	301.81	306.12	4.6	1.7	18.45	59	5008216	5008129	8	- 137	+ 5	- 225	- 172	8	5008216	5008218	5008220	979.791
8	B6	D	Mar. 11-12	301.77	306.79	4.7	1.7	18.40	60	5008162	5008075	8	- 142	+ 3	- 225	- 165	8	5008162	5008164	5008166	979.792
9	B6	D	Mar. 12	301.10	306.58	4.8	1.8	18.40	61	5008254	5008167	9	- 112	+ 3	- 225	- 165	8	5008254	5008256	5008258	979.793
No. 149. Wilmington, N. C., John D. Pow- ell.										979.663 ± 0.001											
1	B6	D	Mar. 16	296.80	299.40	6.0	2.3	15.30	55	5008437	5008350	13	- 13	+ 8	- 221	- 167	8	5008437	5008439	5008441	979.657
2	B6	D	Mar. 16-17	297.60	299.58	4.7	1.7	15.40	55	5008415	5008328	13	- 13	+ 8	- 221	- 167	8	5008415	5008417	5008419	979.658
3	B6	D	Mar. 17	299.82	300.95	5.0	2.0	14.70	56	5008332	5008245	8	- 13	+ 7	- 221	- 167	8	5008332	5008334	5008336	979.659
4	B5	D	Mar. 17	293.22	295.60	4.7	1.7	14.18	49	5008310	5008223	8	- 13	+ 13	- 206	- 152	8	5008310	5008312	5008314	979.660
5	B5	D	Mar. 17-18	293.72	295.68	5.8	2.0	13.80	49	5008310	5008223	8	- 13	+ 13	- 206	- 152	8	5008310	5008312	5008314	979.661
6	B5	D	Mar. 18	296.25	297.35	5.8	2.4	12.90	50	5008310	5008223	8	- 13	+ 13	- 206	- 152	8	5008310	5008312	5008314	979.662
7	B5	D	Mar. 18	294.70	297.55	4.5	1.7	12.80	51	5008308	5008223	8	- 13	+ 13	- 206	- 152	8	5008308	5008310	5008312	979.663
8	B5	D	Mar. 18-19	294.10	296.28	4.8	1.7	13.32	52	5008315	5008228	8	- 13	+ 13	- 212	- 152	8	5008315	5008317	5008319	979.664
9	B5	D	Mar. 19	296.11	296.34	5.3	1.8	13.45	53	5008315	5008228	8	- 13	+ 13	- 212	- 152	8	5008315	5008317	5008319	979.665
No. 150. Cheraw, S. C., John D. Powell.										979.711 ± 0.001											
1	B5	D	Mar. 25	300.75	303.08	4.3	1.5	11.70	57	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.708
2	B5	D	Mar. 25-26	299.50	301.26	4.7	1.6	12.35	58	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.709
3	B5	D	Mar. 26	299.82	300.47	6.5	2.0	12.90	60	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.710
4	B6	D	Mar. 26	303.82	306.06	4.3	1.5	13.05	54	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.711
5	B6	D	Mar. 26-27	303.05	304.72	4.3	1.4	14.42	56	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.712
6	B6	D	Mar. 27	303.91	304.60	4.0	1.6	14.58	57	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.713
7	B6	D	Mar. 28	306.42	308.36	5.1	1.8	12.90	62	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.714
8	B6	D	Mar. 28-30	306.50	306.57	5.3	1.8	13.25	63	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.715
9	B6	D	Mar. 30	306.10	306.60	4.2	1.6	13.50	64	5008308	5008221	7	+ 138	+ 3	- 216	- 167	11	5008308	5008310	5008312	979.716
No. 151. Charlotte, N. C., John D. Pow- ell.										979.727 ± 0.001											
1	B6	D	Apr. 5	316.43	318.90	5.7	2.2	8.38	65	5007904	5007852	13	+ 277	- 3	- 153	- 108	10	5008011	5008003	5008003	979.727
2	B6	D	Apr. 5-6	317.10	318.71	4.0	1.2	8.45	67	5007904	5007852	13	+ 277	- 3	- 153	- 108	10	5008011	5008005	5008005	979.727
3	B6	D	Apr. 6	317.10	318.03	5.3	2.2	8.90	69	5007904	5007852	13	+ 277	- 3	- 153	- 108	10	5007902	5007904	5007904	979.731
4	B5	D	Apr. 6	308.46	309.34	5.0	1.9	9.18	64	5008118	5008031	12	+ 255	+ 2	- 153	- 119	10	5008157	5008156	5008156	979.729
5	B5	D	Apr. 6-7	308.38	309.78	6.0	2.3	9.38	68	5008118	5008031	12	+ 255	+ 2	- 153	- 119	10	5008157	5008159	5008159	979.729
6	B5	D	Apr. 7	308.50	309.08	6.7	2.3	9.38	68	5008117	5008102	12	+ 255	+ 2	- 153	- 119	10	5008157	5008159	5008159	979.731
7	B5	D	Apr. 7	307.32	308.48	6.2	1.9	9.62	73	5008148	5008118	11	+ 225	+ 11	- 131	- 119	10	5008192	5008192	5008192	979.723
8	B5	D	Apr. 7-8	307.60	307.88	5.4	1.4	9.88	72	5008141	5008133	9	+ 211	+ 15	- 131	- 119	10	5008190	5008194	5008192	979.727
9	B5	D	Apr. 8	307.30	307.24	5.0	1.6	10.15	81	5008149	5008130	8	+ 203	+ 18	- 131	- 119	10	5008185	5008186	5008186	979.726
No. 154. Winston-Sa- lem, N. C., John D. Powell.										979.718 ± 0.001											
1	B5	D	Apr. 12	293.08	295.11	4.8	1.5	17.40	53	5008545	5008458	8	- 101	+ 10	- 195	- 158	7	5008244	5008222	5008223	979.711
2	B5	D	Apr. 12-13	293.68	295.36	4.9	1.8	17.15	58	5008528	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.713
3	B5	D	Apr. 13	295.46	296.10	6.3	2.4	16.42	58	5008528	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.718
4	B6	D	Apr. 13	302.48	303.92	3.8	1.5	15.05	54	5008528	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.718
5	B6	D	Apr. 13-14	302.00	303.09	6.0	2.1	15.08	56	5008529	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.718
6	B6	D	Apr. 14	303.56	303.64	4.5	1.9	15.95	57	5008529	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.718
7	B6	D	Apr. 14	301.52	303.26	5.4	1.9	16.15	58	5008529	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.716
8	B6	D	Apr. 14-15	302.10	303.64	5.0	1.7	15.90	59	5008529	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.716
9	B6	D	Apr. 15	304.78	305.30	4.9	2.1	15.05	60	5008529	5008441	9	- 90	+ 7	- 195	- 158	7	5008244	5008222	5008228	979.728
No. 152. Asheville, N. C., John D. Pow- ell.										979.603 ± 0.001											
1	B6	D	Apr. 22	285.39	287.23	4.6	1.3	20.22	49	5008775	5008719	7	- 219	+ 14	- 232	- 186	7	5008324	5008314	5008319	979.603
2	B6	D	Apr. 22-23	285.81	287.65	5.1	1.3	20.40	50	5008775	5008719	7	- 219	+ 14	- 232	- 186	7	5008324	5008314	5008319	979.603
3	B6	D	Apr. 23	285.60	286.38	5.1	1.5	20.45	51	5008769	5008745	1									

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pen- du- lum	Date	Coincidence in- terval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected		Corrections (seventh decimal place)				Period corrected		Mean g	Dynes	
				Chro- no- meter No. 1823	Chro- no- meter No. 1841	Ini- tial mm.	Final mm.			Chronom- eter No. 1823	Chronom- eter No. 1841	Arc	Tem- pera- ture	Pres- sure	Rate		Chronom- eter No. 1823			Mean
															Chronom- eter No. 1823	Chronom- eter No. 1841				
No. 153. Cleveland, Tenn., John D. Powell.	1	B5	1915 Apr. 30.....	281.59	283.41	4.3	1.1	21.00	66	0.500804	0.500837	5	251	2	-225	-179	8	0.5008103	0.5008392	979.646
	2	B5	Apr. 30-May 1	281.59	283.20	6.4	1.6	20.52	82	0.500804	0.500843	12	231	16	-225	-179	8	0.5008102	0.5008392	979.645
	3	B5	May 1.....	282.56	283.33	5.2	2.3	20.40	77	0.500803	0.500839	12	216	11	-223	-179	8	0.5008101	0.5008392	979.649
	4	B6	May 1.....	287.86	289.67	4.1	1.1	20.92	63	0.500800	0.500845	5	218	11	-223	-179	8	0.5008101	0.5008392	979.645
	5	B6	May 1-2.....	287.01	288.97	4.5	1.3	21.32	74	0.500824	0.500866	7	265	9	-223	-176	8	0.5008102	0.5008392	979.648
	6	B6	May 2.....	287.61	288.24	6.0	2.5	21.40	82	0.500808	0.500858	15	268	16	-223	-176	8	0.5008101	0.5008392	979.653
	7	B6	May 2.....	287.72	289.25	4.1	1.1	21.48	63	0.500804	0.500858	5	271	11	-217	-181	8	0.5008105	0.5008392	979.650
	8	B6	May 2-3.....	286.94	288.36	5.0	1.2	21.70	76	0.500828	0.500885	7	281	11	-217	-181	8	0.5008104	0.5008392	979.650
	9	B6	May 3.....	287.20	287.65	5.2	2.3	21.85	88	0.500820	0.500870	12	287	21	-217	-181	8	0.5008175	0.5008392	979.655
No. 155. Knoxville, Tenn., John D. Powell.	1	B6	May 10.....	297.30	297.98	4.5	1.1	18.98	68	0.500823	0.500804	6	163	4	-201	-187	10	0.5008039	0.5008336	979.714
	2	B6	May 10-11.....	296.12	297.02	6.4	1.9	18.90	92	0.500856	0.500813	15	163	26	-201	-187	10	0.5008011	0.5008336	979.714
	3	B6	May 11.....	297.01	297.01	6.4	2.7	18.95	79	0.500832	0.500831	18	164	7	-201	-187	10	0.5008030	0.5008336	979.714
	10	B6	May 13.....	295.13	295.52	6.8	2.5	20.42	49	0.500825	0.500874	18	227	21	-199	-194	10	0.5008032	0.5008416	979.709
	11	B6	May 13-14.....	291.80	293.08	4.7	1.1	20.45	61	0.500805	0.500816	6	228	4	-199	-194	10	0.5008018	0.5008417	979.711
	12	B6	May 14.....	294.40	294.08	4.9	1.8	20.52	91	0.500806	0.500820	9	231	25	-199	-194	10	0.5008012	0.5008417	979.712
	4	B5	May 11.....	290.70	290.49	6.4	1.9	19.28	58	0.500831	0.500821	14	179	6	-201	-187	10	0.5008016	0.5008337	979.712
	5	B5	May 11-12.....	289.02	289.58	6.0	1.8	19.70	74	0.500830	0.500870	12	197	13	-201	-187	10	0.5008015	0.5008337	979.712
	6	B5	May 12.....	289.20	289.86	7.0	2.9	19.88	67	0.500830	0.500853	20	205	9	-201	-187	10	0.5008029	0.5008337	979.713
No. 156. Bristol, Va., John D. Powell	7	B5	May 12-13.....	288.20	289.00	5.8	1.7	20.63	67	0.500830	0.500853	12	219	2	-215	-196	10	0.5008242	0.5008331	979.712
	8	B5	May 12-13.....	288.36	288.10	5.0	2.1	20.32	66	0.500835	0.500863	12	219	2	-215	-196	10	0.5008242	0.5008331	979.712
	9	B5	May 13.....	288.36	288.10	5.0	2.1	20.32	58	0.500835	0.500863	10	223	19	-215	-196	10	0.5008248	0.5008335	979.715
	1	R6	May 19.....	295.70	296.68	5.2	1.5	19.19	68	0.500849	0.500841	9	175	4	-227	-207	12	0.5008012	0.5008034	979.713
	2	B6	May 19-20.....	295.19	296.21	6.0	1.7	19.32	80	0.500844	0.500854	12	181	15	-227	-207	12	0.5008012	0.5008037	979.716
	3	B6	May 20.....	296.12	296.06	5.3	2.3	19.38	72	0.500846	0.500858	12	183	7	-227	-207	12	0.5008015	0.5008037	979.716
	4	B5	May 20.....	288.71	289.69	5.2	1.8	19.58	64	0.500847	0.500866	10	192	0	-220	-209	12	0.5008010	0.5008233	979.718
	5	B5	May 20-21.....	288.94	289.54	5.0	1.8	19.90	55	0.500847	0.500869	9	205	9	-220	-209	12	0.5008010	0.5008233	979.713
	6	B5	May 21.....	289.14	288.57	5.6	2.3	19.95	94	0.500861	0.500879	13	207	0	-220	-209	12	0.5008010	0.5008233	979.713
Washington, D. C., Coast and Geodetic Survey Office, John D. Powell.	7	B5	May 21.....	287.82	288.54	6.8	2.4	20.18	64	0.500801	0.500840	17	217	0	-206	-198	12	0.5008019	0.5008236	979.714
	8	B5	May 21-22.....	287.40	288.18	5.6	1.0	20.45	76	0.500831	0.500891	8	228	11	-206	-198	12	0.5008016	0.5008236	979.707
	9	B5	May 22.....	288.20	287.83	4.5	2.1	20.65	70	0.500860	0.500801	9	237	5	-206	-198	12	0.5008221	0.5008230	979.712
	1	B4	June 18.....	282.43	284.10	5.1	2.0	23.05	48	0.500857	0.500815	10	337	16	-215	-180	11	0.5008013	0.5008293	979.712
	2	B4	June 18-19.....	283.74	284.98	4.7	1.8	22.55	52	0.500826	0.500818	9	316	12	-215	-180	11	0.5008017	0.5008293	979.716
	3	B4	June 19.....	284.58	284.94	4.8	1.7	22.22	54	0.500801	0.500829	9	302	12	-215	-180	11	0.5008017	0.5008293	979.711
	10	B4	July 1.....	284.02	286.14	5.9	2.3	21.52	67	0.500817	0.500873	14	273	2	-215	-165	11	0.5008012	0.5008288	979.715
	11	B4	July 1-2.....	284.49	286.20	4.7	1.3	21.75	65	0.500803	0.500871	7	283	0	-215	-165	11	0.5008012	0.5008285	979.713
	12	B4	July 2.....	284.58	285.50	5.5	2.0	21.88	99	0.500801	0.500872	12	288	4	-215	-165	11	0.5008012	0.5008285	979.714

No. 177, Traverse City, Mich., John D. Pow- ell.	1	B4	D	July 14	329.72	332.20	5.9	2.0	10.42	51	5007594	5007337	-	12	-	155	+	12	-	168	-	7	5007191	5007177	980.545	±0.001		
	2	B4	D	July 15	329.81	331.32	3.2	1.3	13.45	64	5007391	5007314	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.550	±0.001	
	3	B4	D	July 16	329.91	331.78	3.4	1.3	13.45	71	5007401	5007346	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.554	±0.001	
	4	B5	D	July 17	329.95	331.85	3.8	2.0	18.68	73	5007425	5007410	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.558	±0.001	
	5	B5	D	July 18	329.98	331.90	3.8	2.0	18.68	76	5007435	5007420	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.562	±0.001	
	6	B5	D	July 19	329.99	331.92	3.8	2.1	18.70	81	5007445	5007430	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.566	±0.001	
	7	B6	D	July 20	329.99	331.92	3.8	2.1	18.70	81	5007445	5007430	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.570	±0.001	
	8	B6	D	July 21	329.99	331.92	3.8	2.1	18.70	81	5007445	5007430	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.574	±0.001	
	9	B6	D	July 22	329.99	331.92	3.8	2.1	18.70	81	5007445	5007430	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.578	±0.001	
	10	B6	D	July 23	329.99	331.92	3.8	2.1	18.70	81	5007445	5007430	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.582	±0.001	
	11	B6	D	July 24	329.99	331.92	3.8	2.1	18.70	81	5007445	5007430	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.586	±0.001	
	12	B6	D	July 25	329.99	331.92	3.8	2.1	18.70	81	5007445	5007430	-	18	-	185	+	0	211	-	168	-	7	5007177	5007177	980.590	±0.001	
No. 178, Sency Mich., John D. Powell.	1	B5	D	July 21	408.82	411.71	5.4	2.1	18.92	41	5008123	5008079	-	11	-	184	+	22	-	217	-	181	-	6	5007747	5007738	980.685	±0.001
	2	B5	D	July 22	408.84	411.73	5.6	2.1	18.92	41	5008127	5008089	-	12	-	184	+	22	-	217	-	181	-	6	5007747	5007738	980.689	±0.001
	3	B5	D	July 23	408.85	411.74	5.6	2.1	18.92	41	5008131	5008093	-	12	-	184	+	22	-	217	-	181	-	6	5007747	5007738	980.693	±0.001
	4	B5	D	July 24	408.86	411.75	5.6	2.1	18.92	41	5008135	5008097	-	12	-	184	+	22	-	217	-	181	-	6	5007747	5007738	980.697	±0.001
	5	B6	D	July 25	421.70	423.90	6.4	2.0	18.68	56	5008385	5008369	-	14	-	163	+	7	217	-	181	-	6	5007747	5007738	980.694	±0.001	
	6	B6	D	July 26	421.70	423.90	6.4	2.0	18.68	56	5008385	5008369	-	14	-	163	+	7	217	-	181	-	6	5007747	5007738	980.698	±0.001	
	7	B6	D	July 27	421.70	423.90	6.4	2.0	18.68	57	5008385	5008369	-	14	-	163	+	7	217	-	181	-	6	5007747	5007738	980.702	±0.001	
	8	B6	D	July 28	421.70	423.90	6.4	2.0	18.68	57	5008385	5008369	-	14	-	163	+	7	217	-	181	-	6	5007747	5007738	980.706	±0.001	
	9	B6	D	July 29	421.70	423.90	6.4	2.0	18.68	57	5008385	5008369	-	14	-	163	+	7	217	-	181	-	6	5007747	5007738	980.710	±0.001	
	10	B6	D	July 30	421.70	423.90	6.4	2.0	18.68	57	5008385	5008369	-	14	-	163	+	7	217	-	181	-	6	5007747	5007738	980.714	±0.001	
	11	B6	D	July 31	421.70	423.90	6.4	2.0	18.68	57	5008385	5008369	-	14	-	163	+	7	217	-	181	-	6	5007747	5007738	980.718	±0.001	
	12	B6	D	July 31-Aug.	421.70	423.90	6.4	2.0	18.68	56	5008386	5008370	-	13	-	159	+	7	201	-	158	-	6	5005368	5005358	980.678	±0.001	
No. 179, Oconto, Wis., John D. Powell.	1	B4	D	July 28	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.533	±0.001		
	2	B4	D	July 29	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.537	±0.001		
	3	B4	D	July 30	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.541	±0.001		
	4	B5	D	July 31	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.545	±0.001		
	5	B5	D	July 31-Aug.	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.549	±0.001		
	6	B5	D	Aug. 1	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.553	±0.001		
	7	B6	D	Aug. 2	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.557	±0.001		
	8	B6	D	Aug. 3	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.561	±0.001		
	9	B6	D	Aug. 4	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.565	±0.001		
	10	B6	D	Aug. 5	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.569	±0.001		
	11	B6	D	Aug. 6	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.573	±0.001		
	12	B6	D	Aug. 7	331.56	334.67	5.1	1.9	17.40	42	5007552	5007477	-	10	-	101	+	21	-	163	-	13	5007218	5007211	980.577	±0.001		
No. 182, Baldwin, Wis., John D. Powell.	1	B4	D	Aug. 26	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.468	±0.001		
	2	B4	D	Aug. 27	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.472	±0.001		
	3	B4	D	Aug. 28	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.476	±0.001		
	4	B5	D	Aug. 29	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.480	±0.001		
	5	B5	D	Aug. 30	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.484	±0.001		
	6	B5	D	Aug. 31	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.488	±0.001		
	7	B6	D	Aug. 31-Aug.	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.492	±0.001		
	8	B6	D	Aug. 31-Aug.	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.496	±0.001		
	9	B6	D	Aug. 31-Aug.	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.500	±0.001		
	10	B6	D	Aug. 31-Aug.	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.504	±0.001		
	11	B6	D	Aug. 31-Aug.	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.508	±0.001		
	12	B6	D	Aug. 31-Aug.	328.92	331.60	5.0	1.7	16.30	48	5007659	5007585	-	9	-	54	+	15	-	127	-	9	5007383	5007369	980.512	±0.001		
No. 183, Cumberland, Wis., John D. Powell.	1	B4	D	Sep. 1-2	333.90	337.25	5.2	1.7	15.32	53	5007503	5007402	-	10	-	15	+	10	-	209	-	12	5007280	5007248	980.516	±0.001		
	2	B4	D	Sep. 2	333.90	337.25	5.2	1.7	15.32	53	5007503	5007402	-	10	-	15	+	10	-	209	-	12	5007280	5007248	980.520	±0.001		
	3	B4	D	Sep. 3	333.90	337.25	5.2	1.7	15.32	53	5007503	5007402	-	10	-	15	+	10	-	209	-	12	5007280	5007248	980.524	±0.001		
	4	B5	D	Sep. 4	333.90	337.25	5.2	1.7	15.32	53	5007503	5007402	-	10	-	15	+	10	-	209	-	12	5007280	5007248	980.528	±0.001		
	5	B5	D	Sep. 5	333.90	337.25	5.2	1.7	15.32	53	5007503	5007402	-	10	-	15	+	10	-	209	-	12	5007280	5007248	980.532	±0.001		
	6	B5	D	Sep. 6	333.90	337.25	5.2	1.7	15.32	53	5007503	5007402	-	10	-	15	+	10	-	209	-	12	5007280	5007248	980.536	±0.001		
	7	B6	D	Sep. 7	333.90	337.25	5.2	1.7	15.32	53	5007503	5007402	-	10	-	15	+	10	-	209	-	12	5007280	5007248	980.540	±0.001		
	8	B6	D	Sep. 8	333.90	337.25	5.2	1.7	15.32	53	5007503																	

Pendulum observations and reductions—Continued.

Station and observer	Spring No.	Pen- du- lum	Date	Coincidence In- terval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected				Corrections (seventh decimal place)				Period corrected		θ	Mean θ
				Chro- no- meter No. 1823	Chro- no- meter No. 1841	Ini- tial	Final			Chro- no- meter No. 1823	Chro- no- meter No. 1841	Arc	Tem- pera- ture 1823	Pres- sure 1841	Chro- no- meter 1823	Flex- ure 1841	Chro- no- meter No. 1823	Chro- no- meter No. 1841			
No. 181. Winona, Minn., John D. Powell.	1	B4	1915 Aug. 11	319.09	321.48	6.0	1.9	20.90	65	0.5007847	0.5007789	13	-247	1	-228	15	0.5007343	0.5007338	Dynes	980.454	
	2	B4	Aug. 11-12	319.04	321.40	5.9	1.9	21.08	66	0.5007848	0.5007796	12	-235	2	-228	15	0.5007336	0.5007334		980.480	
	3	B4	Aug. 12	319.19	320.41	5.9	3.1	21.28	66	0.5007844	0.5007715	17	-263	2	-228	15	0.5007319	0.5007329		980.488	
	4	B5	Aug. 12	368.70	371.83	5.3	1.7	21.35	77	0.5007791	0.5007631	10	-263	10	-223	19	0.5007319	0.5007326		980.480	
	5	B5	Aug. 12-13	368.72	372.15	5.7	1.7	21.35	77	0.5007788	0.5007636	11	-267	12	-223	18	0.5007319	0.5007323		980.484	
	6	B5	Aug. 13	369.72	372.15	5.6	2.0	21.35	77	0.5007771	0.5007627	12	-266	13	-223	18	0.5007319	0.5007323		980.487	
	7	B6	Aug. 13	379.58	383.35	5.9	2.0	21.35	55	0.5006588	0.5006521	12	-266	9	-240	15	0.5006558	0.5006566		980.482	
	8	B6	Aug. 13-14	379.98	383.92	5.5	1.8	21.30	56	0.5006588	0.5006521	11	-261	8	-240	15	0.5006558	0.5006562		980.484	
	9	B6	Aug. 14	380.94	383.54	5.8	2.3	21.20	57	0.5006571	0.5006527	13	-260	7	-240	15	0.5006558	0.5006566		980.486	
No. 184. Cambridge, Minn., John D. Powell.	1	B4	Aug. 19	330.44	333.73	5.7	1.7	19.10	61	0.5007577	0.5007502	11	-172	3	-240	17	0.5007147	0.5007144		980.580	
	2	B4	Aug. 19-20	329.41	332.60	6.3	1.7	19.38	63	0.5007601	0.5007528	8	-184	1	-240	17	0.5007160	0.5007158		980.555	
	3	B4	Aug. 20	330.51	332.71	4.1	1.5	19.30	64	0.5007578	0.5007511	8	-181	0	-240	17	0.5007159	0.5007156		980.559	
	4	B5	Aug. 20	384.34	386.66	5.0	1.5	19.38	67	0.5007513	0.5007441	10	-196	14	-224	16	0.5007159	0.5007156		980.554	
	5	B5	Aug. 20-21	383.34	386.82	5.6	1.5	19.63	68	0.5007510	0.5007441	11	-196	14	-224	16	0.5007159	0.5007156		980.554	
	6	B5	Aug. 21	384.24	386.38	5.4	2.0	19.63	85	0.5007513	0.5007441	11	-196	14	-224	16	0.5007159	0.5007156		980.553	
	7	B6	Aug. 21	396.80	400.58	5.4	1.9	19.72	50	0.5008324	0.5008248	9	-216	10	-225	16	0.5008353	0.5008379		980.530	
	8	B6	Aug. 21-22	396.08	399.30	5.3	1.6	20.15	53	0.5008326	0.5008269	10	-225	10	-225	16	0.5008356	0.5008381		980.554	
	9	B6	Aug. 22	396.87	398.15	5.0	1.9	20.35	54	0.5008323	0.5008267	9	-225	10	-225	16	0.5008353	0.5008380		980.557	
No. 185. Brainerd, Minn., John D. Pow- ell.	1	B4	Sept. 15	338.42	342.24	5.7	1.7	20.98	54	0.5007308	0.5007315	11	-251	10	-222	14	0.5006916	0.5006911		980.650	
	2	B4	Sept. 15-16	338.21	342.40	5.9	2.3	20.92	55	0.5007312	0.5007312	8	-248	8	-222	14	0.5006920	0.5006914		980.650	
	3	B4	Sept. 16	339.22	341.92	4.5	1.7	21.00	56	0.5007312	0.5007312	8	-251	8	-222	14	0.5006916	0.5006910		980.652	
	4	B5	Sept. 16	394.30	399.90	5.3	1.8	21.38	57	0.5007312	0.5007312	10	-257	8	-221	13	0.5006916	0.5006914		980.644	
	5	B5	Sept. 16-17	393.93	399.02	5.5	1.8	21.48	59	0.5007312	0.5007312	11	-272	7	-221	13	0.5006916	0.5006914		980.645	
	6	B5	Sept. 17	395.24	399.71	5.7	2.2	21.32	60	0.5007312	0.5007312	13	-273	8	-221	13	0.5006916	0.5006914		980.652	
	7	B6	Sept. 17	406.13	411.58	4.4	1.4	21.97	54	0.5007312	0.5007312	7	-282	4	-218	14	0.5006916	0.5006914		980.646	
	8	B6	Sept. 17-18	405.80	411.58	5.1	1.0	22.08	56	0.5007312	0.5007312	8	-287	8	-218	14	0.5006916	0.5006914		980.650	
	9	B6	Sept. 18	407.38	410.56	4.8	2.1	21.98	56	0.5007312	0.5007312	10	-282	8	-218	14	0.5006916	0.5006914		980.651	
No. 196. Faribault, Minn., John D. Pow- ell.	1	B4	Sept. 22	328.58	333.74	4.9	1.9	16.12	50	0.5007820	0.5007502	10	-47	13	-245	11	0.5007309	0.5007300		980.499	
	2	B4	Sept. 22-23	328.96	333.71	4.5	1.8	16.45	50	0.5007820	0.5007502	8	-61	13	-245	11	0.5007309	0.5007300		980.505	
	3	B4	Sept. 23	330.40	333.46	5.0	1.7	16.42	50	0.5007820	0.5007502	9	-60	13	-245	11	0.5007309	0.5007300		980.511	
	4	B5	Sept. 23	382.64	388.19	5.4	1.6	16.45	51	0.5007820	0.5007502	11	-73	12	-244	11	0.5007309	0.5007300		980.507	
	5	B5	Sept. 23-24	382.40	387.28	4.5	1.9	17.42	51	0.5007820	0.5007502	7	-100	10	-244	11	0.5007309	0.5007300		980.504	
	6	B5	Sept. 24	382.62	387.52	4.8	1.8	17.42	50	0.5007820	0.5007502	9	-101	10	-244	11	0.5007309	0.5007300		980.507	
	7	B6	Sept. 24	382.62	387.52	4.6	1.8	17.42	50	0.5007820	0.5007502	9	-101	10	-244	11	0.5007309	0.5007300		980.505	
	8	B6	Sept. 24-25	382.13	387.40	4.5	1.8	18.00	50	0.5007820	0.5007502	6	-142	13	-244	11	0.5007309	0.5007300		980.503	
	9	B6	Sept. 25	392.44	393.74	4.7	2.2	18.38	50	0.5007820	0.5007502	10	-142	13	-244	11	0.5007309	0.5007300		980.505	
No. 197. St. James, Minn., John D. Pow- ell.	1	B4	Sept. 29	317.90	321.68	5.0	1.7	18.88	54	0.5007579	0.5007502	9	-163	13	-243	13	0.5007171	0.5007168		980.433	
	2	B4	Sept. 29-30	318.10	322.10	5.3	2.4	18.62	55	0.5007579	0.5007502	10	-152	9	-243	13	0.5007171	0.5007168		980.436	
	3	B4	Sept. 30	320.18	322.26	4.9	2.4	18.00	55	0.5007579	0.5007502	15	-126	8	-243	13	0.5007171	0.5007168		980.444	
	4	B5	Sept. 30	370.18	375.28	4.8	1.7	17.88	59	0.5007579	0.5007502	9	-124	3	-240	13	0.5007171	0.5007168		980.435	
	5	B5	Sept. 30-Oct. 1	370.37	375.40	5.1	1.9	17.96	61	0.5007579	0.5007502	10	-124	3	-240	13	0.5007171	0.5007168		980.435	
	6	B5	Oct. 1	372.48	375.70	5.4	1.9	17.92	62	0.5007579	0.5007502	11	-110	3	-240	13	0.5007171	0.5007168		980.432	
	7	B6	Oct. 1	380.44	386.10	4.7	1.8	17.92	62	0.5007579	0.5007502	9	-122	2	-241	13	0.5007171	0.5007168		980.432	
	8	B6	Oct. 1-2	373.05	385.08	4.6	1.5	18.42	63	0.5007579	0.5007502	7	-143	1	-241	13	0.5007171	0.5007168		980.435	
	9	B6	Oct. 2	381.16	384.81	4.7	1.9	18.45	64	0.5007579	0.5007502	9	-145	0	-241	13	0.5007171	0.5007168		980.440	

No. 199. Dawson, Minn., John D. Pow- ell.			1	B4	D	Oct. 8	338.06	342.15	4.6	1.7	14.38	51	5007406	5007317	- 8	+ 26	+ 11	- 214	- 139	- 11	5007210	5007196	5007203	980.537 ± 0.001
2	B4	D	Oct. 8-9	337.93	341.60	4.7	1.6	14.38	5.5	1.9	18.95	52	5007407	5007318	- 9	+ 26	+ 11	- 214	- 139	- 11	5007200	5007186	5007193	980.534
3	B4	D	Oct. 9	337.93	341.60	4.7	1.6	14.38	5.5	1.9	18.95	53	5007408	5007319	- 9	+ 26	+ 11	- 214	- 139	- 11	5007190	5007176	5007183	980.535
4	B5	D	Oct. 9-10	338.20	341.90	4.8	1.8	14.38	5.6	2.0	19.00	54	5007409	5007320	- 9	+ 26	+ 11	- 214	- 139	- 11	5007180	5007166	5007173	980.532
5	B5	D	Oct. 10	338.20	341.90	4.8	1.8	14.38	5.6	2.0	19.00	55	5007410	5007321	- 9	+ 26	+ 11	- 214	- 139	- 11	5007170	5007156	5007163	980.533
6	B5	D	Oct. 10-11	338.20	341.90	4.8	1.8	14.38	5.6	2.0	19.00	56	5007411	5007322	- 9	+ 26	+ 11	- 214	- 139	- 11	5007160	5007146	5007153	980.532
7	B6	D	Oct. 11	338.20	341.90	4.8	1.8	14.38	5.6	2.0	19.00	57	5007412	5007323	- 9	+ 26	+ 11	- 214	- 139	- 11	5007150	5007136	5007143	980.531
8	B6	D	Oct. 11-12	338.20	341.90	4.8	1.8	14.38	5.6	2.0	19.00	58	5007413	5007324	- 9	+ 26	+ 11	- 214	- 139	- 11	5007140	5007126	5007133	980.530
9	B6	D	Oct. 12	338.20	341.90	4.8	1.8	14.38	5.6	2.0	19.00	59	5007414	5007325	- 9	+ 26	+ 11	- 214	- 139	- 11	5007130	5007116	5007123	980.529
1	B4	D	Oct. 15	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	66	5007612	5007508	- 12	- 106	+ 2	- 215	- 132	- 7	5007100	5007086	5007093	980.545
2	B4	D	Oct. 15-16	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	67	5007613	5007509	- 12	- 106	+ 2	- 215	- 132	- 7	5007090	5007076	5007083	980.542
3	B4	D	Oct. 16	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	68	5007614	5007510	- 12	- 106	+ 2	- 215	- 132	- 7	5007080	5007066	5007073	980.541
4	B5	D	Oct. 16-17	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	69	5007615	5007511	- 12	- 106	+ 2	- 215	- 132	- 7	5007070	5007056	5007063	980.540
5	B5	D	Oct. 17	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	70	5007616	5007512	- 12	- 106	+ 2	- 215	- 132	- 7	5007060	5007046	5007053	980.539
6	B5	D	Oct. 17-18	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	71	5007617	5007513	- 12	- 106	+ 2	- 215	- 132	- 7	5007050	5007036	5007043	980.538
7	B5	D	Oct. 18	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	72	5007618	5007514	- 12	- 106	+ 2	- 215	- 132	- 7	5007040	5007026	5007033	980.537
8	B5	D	Oct. 18-19	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	73	5007619	5007515	- 12	- 106	+ 2	- 215	- 132	- 7	5007030	5007016	5007023	980.536
9	B6	D	Oct. 19	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	74	5007620	5007516	- 12	- 106	+ 2	- 215	- 132	- 7	5007020	5007006	5007013	980.535
10	B6	D	Oct. 19-20	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	75	5007621	5007517	- 12	- 106	+ 2	- 215	- 132	- 7	5007010	5006996	5007003	980.534
11	B6	D	Oct. 20	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	76	5007622	5007518	- 12	- 106	+ 2	- 215	- 132	- 7	5007000	5006986	5006993	980.533
12	B6	D	Oct. 20-21	338.04	342.90	4.6	1.6	14.38	5.5	1.9	18.95	77	5007623	5007519	- 12	- 106	+ 2	- 215	- 132	- 7	5006990	5006976	5006983	980.532
1	B4	D	Oct. 22	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	74	5007704	5007610	- 7	- 189	+ 1	- 225	- 140	- 7	5006980	5006966	5006973	980.548
2	B4	D	Oct. 22-23	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	75	5007705	5007611	- 7	- 189	+ 1	- 225	- 140	- 7	5006970	5006956	5006963	980.547
3	B4	D	Oct. 23	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	76	5007706	5007612	- 7	- 189	+ 1	- 225	- 140	- 7	5006960	5006946	5006953	980.546
4	B5	D	Oct. 23	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	77	5007707	5007613	- 7	- 189	+ 1	- 225	- 140	- 7	5006950	5006936	5006943	980.545
5	B5	D	Oct. 23-24	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	78	5007708	5007614	- 7	- 189	+ 1	- 225	- 140	- 7	5006940	5006926	5006933	980.544
6	B5	D	Oct. 24	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	79	5007709	5007615	- 7	- 189	+ 1	- 225	- 140	- 7	5006930	5006916	5006923	980.543
7	B6	D	Oct. 24	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	80	5007710	5007616	- 7	- 189	+ 1	- 225	- 140	- 7	5006920	5006906	5006913	980.542
8	B6	D	Oct. 25	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	81	5007711	5007617	- 7	- 189	+ 1	- 225	- 140	- 7	5006910	5006896	5006903	980.541
9	B6	D	Oct. 26	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	82	5007712	5007618	- 7	- 189	+ 1	- 225	- 140	- 7	5006900	5006886	5006893	980.540
1	B4	D	Oct. 27	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	83	5007713	5007619	- 7	- 189	+ 1	- 225	- 140	- 7	5006890	5006876	5006883	980.539
2	B4	D	Oct. 27-28	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	84	5007714	5007620	- 7	- 189	+ 1	- 225	- 140	- 7	5006880	5006866	5006873	980.538
3	B4	D	Oct. 28	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	85	5007715	5007621	- 7	- 189	+ 1	- 225	- 140	- 7	5006870	5006856	5006863	980.537
4	B5	D	Oct. 28	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	86	5007716	5007622	- 7	- 189	+ 1	- 225	- 140	- 7	5006860	5006846	5006853	980.536
5	B5	D	Oct. 28-29	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	87	5007717	5007623	- 7	- 189	+ 1	- 225	- 140	- 7	5006850	5006836	5006843	980.535
6	B5	D	Oct. 29	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	88	5007718	5007624	- 7	- 189	+ 1	- 225	- 140	- 7	5006840	5006826	5006833	980.534
7	B6	D	Oct. 29	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	89	5007719	5007625	- 7	- 189	+ 1	- 225	- 140	- 7	5006830	5006816	5006823	980.533
8	B6	D	Oct. 30	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	90	5007720	5007626	- 7	- 189	+ 1	- 225	- 140	- 7	5006820	5006806	5006813	980.532
9	B6	D	Oct. 30-31	342.79	347.26	4.3	1.4	26.42	4.3	1.4	26.42	91	5007721	5007627	- 7	- 189	+ 1	- 225	- 140	- 7	5006810	5006796	5006803	980.531
1	B4	D	Nov. 1	353.37	360.00	5.4	1.4	19.85	5.4	1.4	19.85	63	5008148	5008049	- 10	- 191	+ 1	- 202	- 106	- 12	5007734	5007722	5007728	980.332
2	B4	D	Nov. 1-2	353.37	360.00	5.4	1.4	19.85	5.4	1.4	19.85	64	5008149	5008050	- 10	- 191	+ 1	- 202	- 106	- 12	5007724	5007712	5007718	980.331
3	B4	D	Nov. 2	353.37	360.00	5.4	1.4	19.85	5.4	1.4	19.85	65	5008150	5008051	- 10	- 191	+ 1	- 202	- 106	- 12	5007714	5007702	5007708	980.330
4	B5	D	Nov. 2-3	353.37	360.00	5.4	1.4	19.85	5.4	1.4	19.85	66	5008151	5008052	- 10	- 191	+ 1	- 202	- 106	- 12	5007704	5007692	5007698	980.329
5	B5	D	Nov. 3	353.37	360.00	5.4	1.4	19.85	5.4	1.4	19.85	67	5008152	5008053	- 10	- 191	+ 1	- 202	- 106	- 12	5007694	5007682	5007688	980.328
6	B5	D	Nov. 3-4	353.37	360.00	5.4	1.4	19.85	5.4	1.4	19.85	68	5008153	5008054	- 10	- 191	+ 1	- 202	- 106	- 12	5007684	5007672	5007678	980.327
7	B6	D	Nov. 4	353.37	360.00	5.4	1.4	19.85	5.4	1.4	19.85	69	500											

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pendulum	Position	Date	Coincidence interval		Total arc		Temperature	Pressure	Period uncorrected				Corrections (seventh decimal place)				Period corrected		θ	Mean g
					Chronometer No. 1823	Chronometer No. 1841	Initial	Final			Chronometer No. 1823	Chronometer No. 1841	Arc	Temperature	Pressure	Rate		Chronometer No. 1823	Chronometer No. 1841	Flexure		
																Chronometer No. 1823	Chronometer No. 1841					
No. 216, Fredericksburg, Va., John D. Powell.	1	B4	D	1916	278.86	282.95	4.8	1.7	20.30	51	0.508081	0.508312	9	-222	+12	8	0.508315	0.508315	0.508315	980.023	980.027 ± 0.001	
	2	B4	D	Jan. 12-13	278.94	283.43	4.5	1.7	20.42	52	0.508097	0.508326	8	-227	+11	8	0.508308	0.508308	0.508308	980.029		
	3	B4	D	Jan. 13	279.30	282.81	4.7	2.1	20.50	53	0.508097	0.508326	8	-227	+11	8	0.508308	0.508308	0.508308	980.029		
	4	B5	D	Jan. 13	316.62	322.14	4.4	1.5	20.68	60	0.507908	0.507773	6	-238	+4	8	0.507133	0.507133	0.507133	980.027		
	5	B5	D	Jan. 13-14	316.87	322.55	4.6	1.2	20.55	60	0.507908	0.507773	6	-238	+4	8	0.507133	0.507133	0.507133	980.028		
	6	B5	D	Jan. 14	317.56	322.66	4.7	2.1	20.42	60	0.507908	0.507773	6	-238	+4	8	0.507133	0.507133	0.507133	980.028		
	7	B6	D	Jan. 14	325.01	330.88	5.2	1.8	20.45	52	0.507704	0.507597	10	-227	+11	8	0.507239	0.507239	0.507239	980.024		
	8	B6	D	Jan. 14-15	325.46	331.62	5.0	1.0	20.42	54	0.507693	0.507550	13	-227	+10	8	0.507231	0.507231	0.507231	980.028		
	9	B6	D	Jan. 15	326.02	330.73	4.9	2.8	20.35	53	0.507680	0.507570	13	-224	+11	8	0.507216	0.507216	0.507216	980.027		
No. 217, Dover, Del., John D. Powell.	1	B4	D	Dec. 1	261.40	264.38	5.4	1.7	16.28	61	0.508594	0.508307	10	-54	+2	9	0.508329	0.508329	0.508329	980.009		
	2	B4	D	Dec. 1-2	291.62	293.89	4.6	1.0	16.25	63	0.508587	0.508321	9	-52	+2	9	0.508326	0.508326	0.508326	980.006		
	3	B4	D	Dec. 2	292.22	294.36	4.4	2.0	16.28	65	0.508570	0.508307	9	-54	+2	9	0.508326	0.508326	0.508326	980.005		
	4	B5	D	Dec. 2-3	330.15	333.56	5.2	1.6	17.40	61	0.507584	0.507506	8	-101	+3	9	0.507275	0.507275	0.507275	980.088		
	5	B5	D	Dec. 3	330.94	333.70	5.0	1.5	17.72	63	0.507568	0.507543	8	-114	+3	9	0.507244	0.507244	0.507244	980.105		
	6	B5	D	Dec. 3	333.10	334.94	5.2	2.3	17.48	65	0.507516	0.507475	12	-91	+1	192	0.507233	0.507233	0.507233	980.087		
	7	B6	D	Dec. 3	339.51	342.84	5.4	1.5	17.48	65	0.507375	0.507303	9	-104	+3	9	0.507095	0.507095	0.507095	980.106		
	8	B6	D	Dec. 3-4	340.58	343.57	5.0	1.4	17.40	61	0.507351	0.507287	8	-101	+2	9	0.507044	0.507044	0.507044	980.092		
	9	B6	D	Dec. 4	342.44	344.87	4.5	2.4	16.90	62	0.507311	0.507260	11	-80	+2	9	0.507021	0.507021	0.507021	980.100		
No. 215, Crisfield, Md., John D. Powell.	1	B4	D	Dec. 8	287.49	290.19	5.2	1.4	12.15	74	0.508711	0.508430	9	+119	-11	196	0.508907	0.508907	0.508907	979.989		
	2	B4	D	Dec. 8-9	286.16	288.66	5.6	1.2	12.60	91	0.508752	0.508476	16	+90	-15	196	0.508614	0.508614	0.508614	979.985		
	3	B4	D	Dec. 9	286.28	288.40	5.5	1.7	12.85	78	0.508748	0.508476	16	+90	-15	196	0.508614	0.508614	0.508614	979.987		
	4	B5	D	Dec. 9-10	321.74	328.10	4.9	1.0	13.40	69	0.507710	0.507631	11	+67	-6	199	0.507554	0.507554	0.507554	979.976		
	5	B5	D	Dec. 10	327.33	330.48	4.6	2.2	13.10	70	0.507649	0.507576	10	+87	-6	199	0.507506	0.507506	0.507506	979.982		
	6	B5	D	Dec. 10	334.65	339.15	5.5	1.5	12.92	68	0.507482	0.507392	10	+80	-7	189	0.507358	0.507358	0.507358	979.983		
	7	B6	D	Dec. 10-11	335.23	339.06	4.9	0.9	12.72	86	0.507384	0.507344	6	+96	-22	189	0.507340	0.507340	0.507340	979.980		
	8	B6	D	Dec. 11	337.22	340.18	5.2	2.4	12.25	81	0.507311	0.507260	13	+115	-18	189	0.507313	0.507313	0.507313	979.983		
	9	B6	D	Dec. 11	337.22	340.18	5.2	2.4	12.25	81	0.507311	0.507260	13	+115	-18	189	0.507313	0.507313	0.507313	979.990		
Washington, D. C., Coast and Geodetic Survey Office, John D. Powell.	1	B4	D	Jan. 20	1828	306.66	316.14	4.3	1.4	8.98	63	0.508166	0.507920	7	+232	-1	120	0.508253	0.508253	0.508253	980.013	
	2	B4	D	Jan. 20-21	305.41	315.25	5.5	1.9	9.42	59	0.508169	0.507943	12	+234	-3	120	0.508253	0.508253	0.508253	980.013		
	3	B4	D	Jan. 21	304.67	314.85	4.7	1.8	9.72	65	0.508219	0.507953	9	+221	-3	120	0.508253	0.508253	0.508253	980.013		
	4	B5	D	Jan. 21	349.51	352.54	4.5	1.5	10.60	56	0.507163	0.506905	10	+184	+2	139	0.507209	0.507209	0.507209	980.017		
	5	B5	D	Jan. 21-22	347.35	351.22	5.0	1.7	11.32	63	0.507208	0.506984	9	+154	+2	139	0.507221	0.507221	0.507221	980.017		
	6	B5	D	Jan. 22	345.43	359.49	5.0	2.0	11.88	63	0.507247	0.506984	9	+131	-1	139	0.507221	0.507221	0.507221	980.017		
	7	B6	D	Jan. 24	353.56	368.30	6.1	1.7	13.10	54	0.507081	0.506807	9	+80	+8	140	0.507013	0.507013	0.507013	980.013		
	8	B6	D	Jan. 24-25	353.34	368.11	4.9	1.8	13.05	58	0.507085	0.506807	9	+82	+5	140	0.507016	0.507016	0.507016	980.016		
	9	B6	D	Jan. 25	353.30	368.06	5.2	1.9	12.98	62	0.507086	0.506802	11	+85	+1	140	0.507014	0.507014	0.507014	980.014		
Washington, D. C., Coast and Geodetic Survey Office, C. L. Garner.	1	A4	D	July 8-9	1838	303.64	307.84	4.7	1.8	21.95	59	0.508247	0.508008	9	-291	+5	470	0.508375	0.508375	0.508375	980.004	
	2	A4	D	July 9	304.22	298.25	5.4	2.1	22.00	59	0.508231	0.508006	12	-293	+5	470	0.508375	0.508375	0.508375	980.004		
	3	A4	D	July 9-10	390.85	378.36	5.4	2.0	22.37	56	0.506444	0.506416	11	-309	+8	523	0.506608	0.506608	0.506608	980.017		
	4	A5	D	July 10	388.44	378.56	5.2	2.1	22.40	56	0.506444	0.506416	11	-310	+8	523	0.506608	0.506608	0.506608	980.017		
	5	A5	D	July 10	389.62	378.64	5.3	1.7	22.40	56	0.506444	0.506416	11	-310	+8	523	0.506608	0.506608	0.506608	980.017		
	6	A5	D	July 10-11	413.12	378.64	5.3	1.7	22.40	56	0.506444	0.506416	11	-310	+8	523	0.506608	0.506608	0.506608	980.017		
	7	A6	D	July 11	413.12	378.64	5.0	2.1	22.97	53	0.506059	0.506059	9	-324	+9	567	0.506283	0.506283	0.506283	980.021		
	8	A6	D	July 11	413.12	378.64	5.1	2.1	22.70	55	0.506059	0.506059	9	-324	+9	567	0.506283	0.506283	0.506283	980.021		
	9	A6	D	July 11	413.33	378.64	5.1	1.7	22.70	55	0.506056	0.506056	9	-323	+9	567	0.506280	0.506280	0.506280	980.020		

Washington, D. C., Coast and Geodetic Survey Office, C. L. Garnier.			N. 125. Atlantic C. y, N. J., C. L. Garnier.			N. 126. Bridgehampton, N. Y., C. L. Garnier.			N. 127. Chatham, Mass., C. L. Garnier.			N. 128. Rockland, Me., C. L. Garnier.			N. 129. Lancaster, N. H., C. L. Garnier.		
1	A4	D	July 21.....	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	
2	A4	D	July 22.....	287.27	302.52	300.88	300.98	300.88	300.98	300.88	300.98	300.88	300.98	300.88	300.98	300.88	
3	A4	D	July 23.....	288.56	301.89	301.28	301.38	301.28	301.38	301.28	301.38	301.28	301.38	301.28	301.38	301.28	
4	A4	D	July 24.....	289.22	302.84	310.75	310.85	310.75	310.85	310.75	310.85	310.75	310.85	310.75	310.85	310.75	
5	A5	D	July 25.....	331.92	352.84	331.92	331.92	331.92	331.92	331.92	331.92	331.92	331.92	331.92	331.92	331.92	
6	A5	D	July 26.....	336.86	354.04	336.86	336.86	336.86	336.86	336.86	336.86	336.86	336.86	336.86	336.86	336.86	
7	A6	D	July 27.....	337.32	355.02	337.32	337.32	337.32	337.32	337.32	337.32	337.32	337.32	337.32	337.32	337.32	
8	A6	D	July 28.....	376.83	401.30	376.83	376.83	376.83	376.83	376.83	376.83	376.83	376.83	376.83	376.83	376.83	
9	A6	D	July 29.....	376.74	402.54	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	
10	A6	D	July 30.....	376.74	401.85	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	376.74	
11	A4	D	Sept. 5.....	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	
12	A4	D	Sept. 6.....	300.88	300.98	300.88	300.88	300.88	300.88	300.88	300.88	300.88	300.88	300.88	300.88	300.88	
13	A4	D	Sept. 7.....	310.75	310.85	310.75	310.75	310.75	310.75	310.75	310.75	310.75	310.75	310.75	310.75	310.75	
14	A5	D	Sept. 8.....	422.51	401.30	422.51	422.51	422.51	422.51	422.51	422.51	422.51	422.51	422.51	422.51	422.51	
15	A5	D	Sept. 9.....	425.32	410.08	425.32	425.32	425.32	425.32	425.32	425.32	425.32	425.32	425.32	425.32	425.32	
16	A6	D	Sept. 10.....	425.02	411.84	425.02	425.02	425.02	425.02	425.02	425.02	425.02	425.02	425.02	425.02	425.02	
17	A6	D	Sept. 11.....	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	1838	
18	A6	D	Sept. 12.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
19	A6	D	Sept. 13.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
20	A6	D	Sept. 14.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
21	A6	D	Sept. 15.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
22	A6	D	Sept. 16.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
23	A6	D	Sept. 17.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
24	A6	D	Sept. 18.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
25	A6	D	Sept. 19.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
26	A6	D	Sept. 20.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
27	A6	D	Sept. 21.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
28	A6	D	Sept. 22.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
29	A6	D	Sept. 23.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
30	A6	D	Sept. 24.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
31	A6	D	Sept. 25.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
32	A6	D	Sept. 26.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
33	A6	D	Sept. 27.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
34	A6	D	Sept. 28.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
35	A6	D	Sept. 29.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
36	A6	D	Sept. 30.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
37	A6	D	Sept. 31.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
38	A6	D	Sept. 32.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
39	A6	D	Sept. 33.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
40	A6	D	Sept. 34.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
41	A6	D	Sept. 35.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
42	A6	D	Sept. 36.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
43	A6	D	Sept. 37.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
44	A6	D	Sept. 38.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
45	A6	D	Sept. 39.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
46	A6	D	Sept. 40.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
47	A6	D	Sept. 41.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
48	A6	D	Sept. 42.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
49	A6	D	Sept. 43.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
50	A6	D	Sept. 44.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
51	A6	D	Sept. 45.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
52	A6	D	Sept. 46.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
53	A6	D	Sept. 47.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
54	A6	D	Sept. 48.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
55	A6	D	Sept. 49.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
56	A6	D	Sept. 50.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
57	A6	D	Sept. 51.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
58	A6	D	Sept. 52.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
59	A6	D	Sept. 53.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
60	A6	D	Sept. 54.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
61	A6	D	Sept. 55.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
62	A6	D	Sept. 56.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
63	A6	D	Sept. 57.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
64	A6	D	Sept. 58.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
65	A6	D	Sept. 59.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
66	A6	D	Sept. 60.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
67	A6	D	Sept. 61.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
68	A6	D	Sept. 62.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
69	A6	D	Sept. 63.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	
70	A6	D	Sept. 64.....	305.72	328.14	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72	305.72			

^a Rate correction determined from observations on stars for time.

Chromometer 3477 failed to break for the last day's observations.

Rate correction determined from comparisons with Western Union time signals.

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pendulum	Date	Coincidence Interval	Total arc		Period uncorrected				Corrections (seventh decimal place)				Period corrected		θ	Mean g		
					Chronometer No. 1828	Chronometer No. 1838	Temperature	Pressure	Chronometer No. 1828	Chronometer No. 1838	Arc	Temperature	Pressure	Chronometer No. 1828	Chronometer No. 1838	Mean				
																			Rate	Flexure
																			Dynes	
No. 130. Whitehall, N. Y., C. L. Garner.	1	A4	Oct. 15, 1914.	321.14	337.67	5.1	1.8	17.91	58	0.5007725	0.5007415	-9	-122	+4	5	-18	+295	0.5007570	880.428	
	2	A4	Oct. 15-16	325.20	338.25	5.4	1.9	17.34	61	0.5007699	0.5007692	-11	-106	+4	3	-18	+286	0.5007591	880.431	
	3	A4	Oct. 16	325.35	338.61	5.2	1.9	17.34	61	0.5007696	0.5007694	-10	-98	+3	0	-18	+286	0.5007596	880.430	
	4	A5	Oct. 16	410.94	411.80	5.3	1.7	17.71	58	0.5007691	0.5007691	-10	-111	+4	4	-26	+286	0.5007583	880.425	
	5	A5	Oct. 16-17	420.22	423.45	5.1	1.9	17.34	60	0.5007697	0.5007694	-10	-106	+4	4	-26	+286	0.5007583	880.428	
	6	A5	Oct. 17	420.60	423.02	5.4	2.0	17.48	60	0.5007691	0.5007690	-11	-101	+4	4	-26	+286	0.5007580	880.428	
	7	A6	Oct. 17	433.81	438.21	5.2	1.9	18.14	61	0.5007698	0.5007696	-11	-132	+3	1	-21	+289	0.5007587	880.420	
	8	A6	Oct. 17-18	443.58	449.16	5.5	1.8	18.26	63	0.5007642	0.5007630	-11	-135	+1	0	-21	+289	0.5007565	880.431	
	9	A6	Oct. 18	441.21	471.66	5.3	1.8	17.98	64	0.5007634	0.5007630	-10	-125	+0	0	-21	+289	0.5007562	880.432	
No. 131. Little Falls, N. Y., C. L. Garner.	1	A4	Nov. 5	325.36	339.38	5.4	1.9	14.33	58	0.5007696	0.5007377	-11	-28	+5	7	+23	+233	0.5007717	880.378	
	2	A4	Nov. 5-6	326.42	337.58	5.4	1.9	14.00	60	0.5007671	0.5007416	-11	-42	+3	7	+23	+233	0.5007704	880.370	
	3	A4	Nov. 6	326.90	338.30	5.4	2.0	13.67	61	0.5007659	0.5007416	-11	-56	+2	5	+31	+201	0.5007735	880.370	
	4	A5	Nov. 6	426.66	433.46	5.5	1.9	13.40	58	0.5007648	0.5007644	-11	-67	+3	3	+31	+201	0.5007658	880.379	
	5	A5	Nov. 6-7	426.37	442.86	5.2	1.9	13.33	60	0.5007670	0.5007652	-10	-70	+3	3	+31	+201	0.5007666	880.376	
	6	A5	Nov. 7	426.06	444.51	5.2	1.7	13.25	62	0.5007654	0.5007631	-10	-74	+3	3	+31	+201	0.5007649	880.378	
	7	A6	Nov. 7	462.08	470.99	5.2	1.9	13.25	57	0.5007637	0.5007613	-10	-74	+3	3	+31	+201	0.5007611	880.377	
	8	A6	Nov. 7-8	462.08	467.75	5.0	1.9	13.23	59	0.5007636	0.5007630	-10	-74	+3	3	+31	+201	0.5007635	880.368	
	9	A6	Nov. 8	451.88	468.40	5.1	1.8	13.10	59	0.5007639	0.5007633	-9	-80	+3	0	+24	+235	0.5007629	880.366	
No. 132. Watertown, N. Y., C. L. Garner.	1	A4	Nov. 11	326.83	338.22	5.2	1.7	13.70	63	0.5007433	0.5007402	-10	-54	+3	2	+22	+72	0.5007509	880.455	
	2	A4	Nov. 11-12	327.61	339.46	5.4	2.0	13.70	60	0.5007437	0.5007376	-10	-54	+3	2	+22	+72	0.5007480	880.460	
	3	A4	Nov. 12	327.94	340.86	5.2	1.9	13.45	58	0.5007409	0.5007343	-11	-63	+3	2	+22	+72	0.5007481	880.468	
	4	A5	Nov. 12	440.02	444.99	5.5	1.9	13.97	53	0.5007465	0.5007423	-12	-69	+3	1	+36	+104	0.5007477	880.469	
	5	A5	Nov. 12-13	442.83	448.33	5.1	2.0	13.35	59	0.5007465	0.5007452	-10	-69	+3	1	+36	+104	0.5007475	880.462	
	6	A5	Nov. 13	445.98	451.64	5.2	1.9	12.75	58	0.5007462	0.5007441	-10	-84	+3	4	+36	+104	0.5007472	880.468	
	7	A6	Nov. 13	470.16	473.90	5.2	1.9	13.33	60	0.5007434	0.5007431	-11	-70	+3	4	+36	+104	0.5007430	880.468	
	8	A6	Nov. 13-14	473.07	481.42	5.1	1.9	12.13	57	0.5007424	0.5007400	-10	-126	+3	4	+36	+104	0.5007430	880.463	
	9	A6	Nov. 14	452.23	484.99	5.2	1.9	11.30	59	0.5007460	0.5007460	-11	-155	+3	4	+36	+104	0.5007375	880.465	
No. 133. Southport, N. Y., C. L. Garner.	1	A4	Nov. 22	328.88	338.35	5.1	1.8	2.91	55	0.5007388	0.5007400	-9	-506	+6	112	+139	-12	0.5008021	880.250	
	2	A4	Nov. 22-23	327.30	337.74	5.1	1.8	2.16	60	0.5007432	0.5007413	-9	-496	+4	112	+139	-12	0.5008031	880.248	
	3	A4	Nov. 23	328.97	338.72	5.0	1.6	2.94	65	0.5007437	0.5007432	-9	-506	+4	112	+139	-12	0.5008010	880.255	
	4	A5	Nov. 23	446.85	448.48	5.3	1.9	2.91	53	0.5007401	0.5007418	-10	-506	+5	181	+142	-12	0.5008012	880.254	
	5	A5	Nov. 23-24	446.18	448.12	4.9	1.9	2.71	63	0.5007401	0.5007402	-9	-514	+2	181	+145	-12	0.5008026	880.250	
	6	A5	Nov. 24	450.10	448.28	5.6	1.9	2.16	59	0.5007401	0.5007402	-11	-537	+0	181	+165	-12	0.5008056	880.250	
	7	A6	Nov. 24	470.04	476.75	5.8	1.7	2.46	56	0.5007325	0.5007350	-9	-575	+5	171	+153	-12	0.5008045	880.257	
	8	A6	Nov. 24-25	474.03	472.56	5.2	1.1	2.86	62	0.5007390	0.5007390	-7	-508	+7	171	+153	-12	0.5008049	880.245	
	9	A6	Nov. 25	470.70	470.41	4.9	2.0	3.24	68	0.5007317	0.5007320	-12	-492	+1	171	+153	-12	0.5008044	880.244	
No. 134. Erie Pa., C. L. Garner.	1	A4	Nov. 28	319.70	322.72	5.2	1.9	12.52	59	0.5007892	0.5007759	-11	-104	+3	17	+103	-6	0.5007899	880.281	
	2	A4	Nov. 28-29	319.31	322.48	5.2	1.8	12.36	62	0.5007842	0.5007764	-10	-111	+1	17	+103	-6	0.5007854	880.277	
	3	A4	Nov. 29	319.12	323.03	5.0	1.7	12.29	64	0.5007846	0.5007731	-9	-114	+0	17	+103	-6	0.5007852	880.277	
	4	A5	Nov. 29	410.97	416.51	5.4	1.9	12.42	56	0.5008089	0.5008090	-11	-108	+6	17	+103	-6	0.5008080	880.280	
	5	A5	Nov. 29-30	410.98	416.55	5.0	1.8	12.52	57	0.5008080	0.5008090	-9	-104	+3	17	+103	-6	0.5008080	880.281	
	6	A5	Nov. 30	409.84	416.89	5.0	1.8	12.56	58	0.5008107	0.5008107	-9	-102	+3	17	+103	-6	0.5008107	880.280	
	7	A6	Nov. 30	433.90	441.54	5.4	1.9	12.76	58	0.5007858	0.5007858	-11	-94	+4	4	+108	-6	0.5007858	880.278	
	8	A6	Nov. 30	432.65	440.72	5.3	1.8	12.84	59	0.5007855	0.5007855	-10	-91	+4	4	+108	-6	0.5007855	880.274	
	9	A6	Dec. 1	432.49	440.64	5.1	1.7	12.96	60	0.5007857	0.5007850	-9	-85	+3	4	+108	-6	0.5007861	880.275	

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Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pen- dulum	Posi- tion	Date	Coincidence In- terval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected		Corrections (seventh decimal place)					Period corrected		θ	Mean θ	
					Chro- no- meter No. 1828	Chro- no- meter No. 1838	Ini- tial	Final			Chro- no- meter No. 1828	Chro- no- meter No. 1838	Arc	Tem- pera- ture	Pres- sure	Rate		Chro- no- meter No. 1828	Flex- ure No.			
																Chro- no- meter No. 1828	Flex- ure No.					
No. 163, Albany, Ga., C. L. Garner.	1	A4	D	1915 Mar. 26	248.04	255.38	5.4	5.4	13.74	58	0.5010090	0.5009809	-11	+53	5	-54	+241	-11	0.5010084	Dynes	979.449 ± 0.001	
	2	A4	D	Mar. 26-27	247.58	255.07	5.4	5.4	2.0	14.03	58	0.5010118	0.5009829	-11	+41	3	-54	+241	-11	0.5010084		979.443
	3	A4	D	Mar. 27	247.36	254.93	5.4	5.4	2.0	14.18	61	0.5010128	0.5009836	-11	+34	2	-54	+241	-11	0.5010084		979.443
	4	A5	D	Mar. 27	249.60	259.10	5.3	5.3	2.0	14.48	57	0.5008358	0.5008019	-11	+22	6	-53	+235	-11	0.5008300		979.458
	5	A5	D	Mar. 27-28	249.25	258.75	5.2	5.2	1.7	14.58	58	0.5008368	0.5008027	-10	+18	5	-53	+235	-11	0.5008316		979.452
	6	A5	D	Mar. 28	248.94	258.44	5.2	5.2	2.4	14.54	60	0.5008377	0.5008036	-13	+19	3	-53	+235	-11	0.5008338		979.444
	7	A6	D	Mar. 28	312.60	323.02	5.3	5.3	2.7	14.54	65	0.5008410	0.5007752	-14	+19	2	-46	+215	-11	0.5007956		979.450
	8	A6	D	Mar. 28-29	312.08	322.40	5.2	5.2	1.6	14.58	63	0.5008424	0.5007766	-9	+23	0	-46	+215	-11	0.5007978		979.448
	9	A6	D	Mar. 29	312.05	322.84	5.2	5.2	1.7	14.46	65	0.5008424	0.5007756	-10	+23	2	-46	+215	-11	0.5007978		979.450
No. 162, Macon, Ga., C. L. Garner.	1	A4	D	Apr. 1	248.37	255.84	5.6	5.6	2.0	19.65	56	0.5010086	0.5009730	-12	-195	8	-73	+218	-8	0.5008804	979.553	
	2	A4	D	Apr. 1-2	248.48	255.60	5.3	5.3	1.9	19.57	58	0.5010082	0.5009736	-11	-191	8	-73	+218	-8	0.5008804	979.551	
	3	A4	D	Apr. 2	248.62	256.02	5.4	5.4	2.2	19.30	59	0.5010078	0.5009734	-12	-180	5	-73	+218	-8	0.5008804	979.551	
	4	A5	D	Apr. 2-3	300.34	310.01	5.3	5.3	1.8	19.40	60	0.5008338	0.5008078	-10	-184	4	-79	+186	-8	0.5008804	979.550	
	5	A5	D	Apr. 3	300.46	310.37	5.1	5.1	1.8	19.37	63	0.5008344	0.5008088	-9	-183	1	-79	+186	-8	0.5008804	979.553	
	6	A5	D	Apr. 3	300.66	310.78	5.4	5.4	2.1	19.20	64	0.5008350	0.5008097	-11	-176	0	-79	+186	-8	0.5008804	979.555	
	7	A6	D	Apr. 3	313.08	322.95	5.3	5.3	1.7	19.33	62	0.5007998	0.5007733	-12	-181	4	-80	+177	-8	0.5007711	979.546	
	8	A6	D	Apr. 3-4	313.12	323.38	5.3	5.3	2.2	19.35	62	0.5007997	0.5007719	-12	-182	2	-80	+177	-8	0.5007711	979.555	
	9	A6	D	Apr. 4	313.70	324.55	5.2	5.2	1.4	19.20	64	0.5007992	0.5007715	-9	-176	0	-80	+177	-8	0.5007703	979.556	
No. 165, Opelika, Ala., C. L. Garner.	1	A4	D	Apr. 8	247.23	251.99	5.3	5.3	1.7	15.16	59	0.5010133	0.5009940	-10	-7	4	-51	+110	-13	0.5010056	979.460	
	2	A4	D	Apr. 8-9	246.58	250.38	5.3	5.3	1.8	15.34	62	0.5010147	0.5009955	-10	-14	1	-51	+110	-13	0.5010060	979.449	
	3	A4	D	Apr. 9	246.75	250.17	5.1	5.1	1.9	15.36	63	0.5010152	0.5009963	-10	-15	0	-51	+110	-13	0.5010079	979.447	
	4	A5	D	Apr. 9	298.08	306.30	5.3	5.3	1.8	15.58	58	0.5008401	0.5008175	-9	-33	5	-63	+139	-13	0.5008286	979.465	
	5	A5	D	Apr. 9-10	297.66	304.73	5.1	5.1	1.7	15.78	60	0.5008413	0.5008217	-9	-33	3	-63	+139	-13	0.5008294	979.465	
	6	A5	D	Apr. 10	297.28	304.36	5.2	5.2	2.0	15.88	61	0.5008424	0.5008227	-11	-37	2	-63	+139	-13	0.5008301	979.458	
	7	A6	D	Apr. 10	309.52	317.06	5.2	5.2	1.6	16.11	64	0.5008490	0.5007897	-9	-47	2	-72	+113	-13	0.5008304	979.457	
	8	A6	D	Apr. 10-11	308.60	315.50	5.0	5.0	1.7	16.31	64	0.5008484	0.5007896	-9	-57	2	-72	+113	-13	0.5007951	979.460	
	9	A6	D	Apr. 11	308.36	315.64	5.0	5.0	1.8	16.36	65	0.5008481	0.5007893	-9	-57	2	-72	+113	-13	0.5007965	979.452	
No. 174, Birmingham, Ala., C. L. Garner.	1	A4	D	Apr. 15	245.60	252.30	5.2	5.2	1.9	20.96	58	0.5010290	0.5009928	-11	-250	3	-86	+201	-12	0.5009847	979.533	
	2	A4	D	Apr. 15-16	246.00	253.20	5.2	5.2	1.8	20.53	61	0.5010183	0.5009833	-10	-242	2	-86	+201	-12	0.5009846	979.537	
	3	A4	D	Apr. 16	246.18	253.68	5.1	5.1	2.1	20.27	62	0.5010176	0.5009825	-10	-221	2	-86	+201	-12	0.5009846	979.538	
	4	A5	D	Apr. 16	297.71	306.02	5.3	5.3	1.8	20.20	57	0.5008412	0.5008183	-9	-218	1	-80	+186	-12	0.5008409	979.538	
	5	A5	D	Apr. 16-17	297.77	306.00	5.1	5.1	1.8	20.15	59	0.5008410	0.5008187	-9	-216	5	-80	+186	-12	0.5008409	979.539	
	6	A5	D	Apr. 17	297.20	306.64	5.2	5.2	2.0	20.27	60	0.5008426	0.5008195	-11	-221	4	-80	+186	-12	0.5008404	979.537	
	7	A6	D	Apr. 17	309.52	317.68	5.1	5.1	1.8	20.47	61	0.5008490	0.5007892	-9	-229	3	-84	+186	-12	0.5008409	979.537	
	8	A6	D	Apr. 17-18	309.34	318.13	5.1	5.1	1.7	20.75	63	0.5008465	0.5007871	-9	-211	1	-84	+186	-12	0.5007759	979.531	
	9	A6	D	Apr. 18	309.22	318.19	5.2	5.2	1.8	20.70	65	0.5008468	0.5007869	-10	-219	1	-84	+186	-12	0.5007752	979.538	
No. 166, Huntsville, Ala., C. L. Garner.	1	A4	D	Apr. 21	251.13	254.20	5.6	5.6	2.0	21.25	58	0.5009975	0.5009534	-12	-262	6	-87	+229	-13	0.5009607	979.631	
	2	A4	D	Apr. 21-22	251.23	254.31	5.4	5.4	1.9	21.23	58	0.5009971	0.5009530	-11	-261	6	-87	+229	-13	0.5009607	979.627	
	3	A4	D	Apr. 22	251.22	253.93	5.3	5.3	2.2	21.07	60	0.5009971	0.5009535	-12	-254	4	-87	+229	-13	0.5009610	979.635	
	4	A5	D	Apr. 22	305.30	310.97	5.2	5.2	1.9	20.95	56	0.5008402	0.5008183	-9	-249	8	-86	+53	-13	0.5007841	979.630	
	5	A5	D	Apr. 22-23	305.58	310.10	5.1	5.1	1.8	20.80	57	0.5008405	0.5008187	-9	-249	7	-86	+53	-13	0.5007841	979.632	
	6	A5	D	Apr. 23	305.40	310.80	5.3	5.3	2.1	20.70	57	0.5008409	0.5008191	-11	-239	4	-86	+53	-13	0.5007851	979.633	
	7	A6	D	Apr. 23	318.60	325.94	5.2	5.2	1.8	20.77	58	0.5007899	0.5007682	-10	-242	6	-109	+96	-13	0.5007519	979.633	
	8	A6	D	Apr. 23-24	318.40	327.58	5.2	5.2	1.8	20.80	60	0.5007894	0.5007643	-10	-243	4	-109	+96	-13	0.5007491	979.641	
	9	A6	D	Apr. 24	318.48	327.62	5.1	5.1	2.0	20.07	62	0.5007892	0.5007645	-10	-238	2	-109	+96	-13	0.5007487	979.640	

No. 173. Greenville, Ala., C. L. Garner.	1	A4	D	Apr. 28	285.50	245.46	5.3	1.9	22.13	57	5010394	5010205	11	-269	+4	-102	+202	-10	5010104	5010099	5010092	979.437 ±0.000
	2	A4	D	Apr. 28-29	284.06	245.31	5.3	1.8	22.20	61	5010323	5010212	10	-265	+4	-102	+202	-10	5010108	5010107	5010107	979.437
	3	A4	D	Apr. 29	284.06	245.31	5.1	1.8	22.03	62	5010323	5010217	10	-265	+4	-102	+202	-10	5010113	5010118	5010117	979.434
	4	A5	D	Apr. 29	283.72	246.40	5.3	1.7	22.05	62	5010765	5010765	10	-268	+7	-109	+212	-10	5010113	5010118	5010117	979.434
	5	A5	D	Apr. 30	283.58	246.34	5.1	1.9	22.10	57	5010770	5010770	10	-268	+7	-109	+212	-10	5010113	5010118	5010117	979.438
	6	A5	D	Apr. 30	283.58	246.34	5.3	2.4	21.33	57	5010770	5010770	13	-265	+7	-109	+212	-10	5010113	5010118	5010117	979.438
	7	A5	D	Apr. 30	283.84	246.30	5.4	1.9	22.03	60	5010772	5010772	11	-265	+4	-109	+212	-10	5010113	5010118	5010117	979.438
	8	A5	D	Apr. 30	283.52	246.20	5.2	1.7	22.17	64	5010771	5010771	10	-300	+1	-109	+212	-10	5010113	5010118	5010117	979.441
	9	A5	D	May 1	285.28	246.49	5.1	2.1	22.17	62	5010779	5010779	10	-300	+3	-109	+212	-10	5010113	5010118	5010117	979.440
	10	A5	D	May 1	287.38	246.82	5.1	1.7	22.36	62	5010779	5010779	9	-300	+3	-109	+212	-10	5010113	5010118	5010117	979.443
	11	A6	D	May 1-2	286.43	246.43	5.3	1.3	22.12	64	5010779	5010779	10	-311	+2	-109	+212	-10	5010113	5010118	5010117	979.437
	12	A6	D	May 2	286.43	246.43	5.3	1.3	22.12	64	5010779	5010779	10	-311	+2	-109	+212	-10	5010113	5010118	5010117	979.436
No. 164. Pensacola, Fla., C. L. Garner.	1	A4	D	May 5	232.89	241.84	5.4	2.0	23.64	59	5010758	5010758	11	-370	+7	-117	+317	-8	5010297	5010292	5010294	979.361
	2	A4	D	May 5-6	232.68	241.78	5.1	2.2	23.79	62	5010758	5010758	8	-378	+7	-117	+317	-8	5010305	5010302	5010304	979.357
	3	A4	D	May 6	232.68	241.78	5.2	2.2	23.72	61	5010758	5010758	12	-378	+7	-117	+317	-8	5010305	5010302	5010304	979.356
	4	A5	D	May 6-7	278.36	240.77	5.1	1.7	23.62	57	5010767	5010767	9	-374	+7	-117	+317	-8	5010305	5010302	5010304	979.356
	5	A5	D	May 7	278.36	240.77	5.2	1.8	23.82	57	5010767	5010767	10	-378	+7	-117	+317	-8	5010305	5010302	5010304	979.359
	6	A6	D	May 7	278.36	240.77	5.2	1.8	23.82	57	5010767	5010767	10	-378	+7	-117	+317	-8	5010305	5010302	5010304	979.358
	7	A6	D	May 7	280.42	240.74	4.9	1.8	24.09	56	5010767	5010767	14	-378	+7	-117	+317	-8	5010305	5010302	5010304	979.358
	8	A6	D	May 7-8	280.42	240.74	5.2	1.9	24.09	56	5010767	5010767	11	-384	+2	-117	+317	-8	5010305	5010302	5010304	979.358
	9	A6	D	May 8	281.82	240.74	5.3	2.2	24.16	53	5010767	5010767	12	-384	+2	-117	+317	-8	5010305	5010302	5010304	979.353
No. 167. Arkansas City Ark., C. L. Garner.	1	A4	D	May 21	248.44	255.11	5.4	2.2	25.38	56	5010165	5010019	12	-435	+7	-143	+311	-14	5010663	5010678	5010670	979.605
	2	A4	D	May 21-22	248.56	255.18	5.3	2.1	25.30	56	5010165	5010019	12	-435	+7	-143	+311	-14	5010663	5010678	5010670	979.604
	3	A4	D	May 22	248.56	255.18	5.2	2.1	25.09	60	5010167	5010019	11	-408	+5	-143	+311	-14	5010663	5010678	5010670	979.596
	4	A5	D	May 22	248.56	255.18	5.2	2.1	25.09	60	5010167	5010019	11	-408	+5	-143	+311	-14	5010663	5010678	5010670	979.596
	5	A5	D	May 22-23	295.32	312.44	5.2	2.0	24.75	62	5010336	5010167	11	-407	+5	-143	+311	-14	5010663	5010678	5010670	979.594
	6	A5	D	May 23	295.32	312.44	5.3	2.0	24.66	56	5010336	5010167	11	-399	+5	-143	+311	-14	5010663	5010678	5010670	979.592
No. 168. Memphis, Tenn., C. L. Garner.	1	A4	D	May 27	256.88	260.16	5.4	1.8	23.52	65	5009751	5009306	10	-357	+0	-59	+365	-9	5009316	5009316	5009316	979.744
	2	A4	D	May 27-28	256.88	260.16	5.4	2.0	23.52	65	5009751	5009306	11	-357	+7	-59	+365	-9	5009316	5009316	5009316	979.741
	3	A4	D	May 28	257.50	270.24	5.4	2.0	23.72	59	5009728	5009283	12	-337	+6	-59	+365	-9	5009316	5009316	5009316	979.738
	4	A5	D	May 28	257.50	270.24	5.4	2.0	23.72	59	5009728	5009283	12	-337	+6	-59	+365	-9	5009316	5009316	5009316	979.738
	5	A5	D	May 28-29	314.78	330.78	5.2	2.0	22.54	61	5007037	5007170	11	-318	+4	-46	+356	-9	5007534	5007534	5007534	979.739
	6	A5	D	May 29	314.78	330.78	5.2	2.0	22.54	61	5007037	5007170	11	-318	+4	-46	+356	-9	5007534	5007534	5007534	979.745
	7	A6	D	May 29	314.83	332.80	5.3	2.3	22.30	64	5007033	5007523	12	-302	+11	-49	+351	-9	5007534	5007534	5007534	979.744
	8	A6	D	May 29	330.26	330.08	5.2	2.1	22.30	63	5007581	5007131	10	-302	+11	-49	+351	-9	5007534	5007534	5007534	979.736
	9	A6	D	May 30	329.60	340.20	5.1	2.1	21.57	57	5007587	5007160	10	-268	+7	-49	+381	-9	5007244	5007244	5007244	979.736
No. 169. Mammoth Spring, Ark., C. L. Garner.	1	A4	D	June 2	299.28	279.76	5.4	2.0	17.94	55	5009032	5009032	11	-123	+8	-74	+262	-13	5009032	5009032	5009032	979.835
	2	A4	D	June 3	298.81	279.27	5.2	2.0	17.87	58	5009318	5009088	10	-130	+6	-74	+262	-13	5009032	5009032	5009032	979.835
	3	A4	D	June 3	298.81	279.27	5.0	2.0	17.87	58	5009318	5009088	10	-130	+6	-74	+262	-13	5009032	5009032	5009032	979.835
	4	A5	D	June 3-4	331.18	344.62	5.4	1.9	17.99	56	5007360	5007269	11	-127	+5	-77	+227	-13	5007345	5007345	5007345	979.830
	5	A5	D	June 3-4	331.18	344.62	5.2	2.0	18.03	59	5007375	5007269	11	-127	+5	-77	+227	-13	5007345	5007345	5007345	979.830
	6	A5	D	June 4	330.04	344.32	5.2	2.0	18.35	55	5007586	5007272	11	-130	+8	-77	+227	-13	5007345	5007345	5007345	979.829
	7	A6	D	June 4	347.02	363.78	5.1	1.9	18.35	55	5007215	5009081	10	-140	+8	-58	+274	-13	5007000	5007000	5007000	979.830
	8	A6	D	June 4-5	345.34	361.32	5.3	1.9	18.40	59	5007229	5009089	11	-145	+3	-58	+274	-13	5007000	5007000	5007000	979.832
	9	A6	D	June 5	345.60	364.00	5.1	1.9	18.40	61	5007244	5009089	11	-145	+3	-58	+274	-13	5007000	5007000	5007000	979.832
No. 170. Hopkinsville, Ky., C. L. Garner.	1	A4	D	June 8	299.28	279.76	5.4	2.0	17.94	55	5009032	5009032	11	-123	+8	-74	+262	-13	5009032	5009032	5009032	979.835
	2	A4	D	June 8-9	298.81	279.27	5.2	2.0	17.87	58	5009318	5009088	10	-130	+6	-74	+262	-13	5009032	5009032	5009032	979.835
	3	A4	D	June 9	298.81	279.27	5.0	2.0	17.87	58	5009318	5009088	10	-130	+6	-74	+262	-13	5009032	5009032	5009032	979.835
	4	A5	D	June 9	331.18	344.62	5.4	1.9	17.99	56	5007360	5007269	11	-127	+5	-77	+227	-13	5007345	5007345	5007345	979.830
	5	A5	D	June 9-10	329.28	347.49	5.3	2.0	21.52	61	5007034	5007269	11	-127	+5	-77	+227	-13	5007345	5007345	5007345	979.830
	6	A5	D	June 10	329.28	347.49	5.3	2.0	21.52	61	5007034	5007269	11	-127	+5	-77	+227	-13	5007345	5007345	5007345	979.830
	7	A6	D	June 10	343.92	363.81	5.1	1.9	21.40	62	5007033	5007269	12	-268	+4	-61	+370	-10	5007244	5007244	5007244	979.834
	8	A6	D	June 10-11	343.92	363.81	5.1	1.9	21.40	62	5007033	5007269	12	-268	+4	-61	+370	-10	5007244	5007244	5007244	979.834
	9	A6	D	June 11	343.12	364.73	5.1	1.8	21.32	61	5007246	5009089	9	-265	+3	-61	+370	-10	5009032	5009032	5009032	979.833
No. 171. Danville, Ky., C. L. Garner.	1	A4	D	June 15	265.46	261.46	5.3	2.0	22.01	57	5009436	5009095	11	-264	+7	-101	+436	-13	5009032	5009032	5009032	979.838
	2	A4	D	June 15-16	265.53	261.53	5.2	2.0	21.75	59	5009433	5009095	11	-263	+5	-101	+436	-13	5009032	5009032	5009032	979.835
	3	A4	D	June 16	265.48	261.50	5.4	2.2	21.50	60	5009435	5009095	12	-272	+4	-101	+436	-13	5009032	5009032	5009032	979.831
	4	A5	D	June 16-17	325.50	351.59	5.5	1.8	21.33	62	5007092	5007128	11	-263	+2	-128	+438	-13	5007277	5007277	5007277	979.837
	5	A5	D	June 17	325.25	351.58	5.2	2.0	21.27	57	5007091	5007128	11	-263	+2	-128	+438	-13	5007277	5007277	5007277	979.837
	6	A6	D	June 17	325.25	351.58	5.1	1.7	21.13	61	5007091	5007128	11	-263	+2	-128	+438	-13	5007277	5007277	5007277	979.837
	7	A6	D	June 17-18	342.80	369.32	5.1	2.0	21.13	61	5007091	5007128	11	-263	+2	-128	+438	-13	500			

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pendulum	Date	Coincidence interval		Total arc		Temperature ° C.	Pressure mm.	Period uncorrected				Corrections (seventh decimal place)				Period corrected		Mean g
				Chronometer No. 1825	Chronometer No. 1838	Initial	Final			Chronometer No. 1825	Chronometer No. 1838	Arc	Temperature	Pressure	Rate	Chronometer No. 1825	Chronometer No. 1838	Mean		
No. 176, Prestonsburg, Ky., C. L. Garner.	1	A4	1915 June 21	265.52	265.33	5.4	2.1	23.15	60	0.500433	0.500877	11	-312	5	-115	0.500859	0.500862	979.881 ±0.001		
	2	A4	June 21-22	265.36	265.16	5.4	1.9	23.09	61	0.500439	0.500882	11	-339	1	-115	0.500861	0.500867			
	3	A4	June 22	265.17	265.00	5.4	2.0	22.96	63	0.500436	0.500879	11	-334	0	-115	0.500893	0.500886			
	4	A5	June 22-23	326.00	325.82	5.3	1.9	22.95	60	0.5007180	0.5007189	10	-333	5	-122	0.5007208	0.5007209			
	5	A5	June 23	325.64	325.66	5.2	1.8	22.86	64	0.5007180	0.5007189	10	-329	3	-122	0.5007218	0.5007216			
	6	A5	June 23	325.70	325.74	5.4	2.0	22.74	62	0.5007185	0.5007187	11	-334	9	-126	0.5007223	0.5007220			
	7	A6	June 23-24	341.78	341.66	5.4	2.0	22.60	55	0.5007325	0.5007325	11	-318	5	-126	0.5008575	0.500872			
	8	A6	June 24	341.44	341.64	5.2	2.0	22.52	59	0.5007333	0.5007332	11	-315	5	-126	0.500874	0.500880			
No. 172, Clifton Forge, Va., C. L. Garner.	1	A4	June 27	266.30	266.30	5.4	1.9	20.33	54	0.500406	0.500903	11	-223	9	-112	0.5009036	0.5009035	979.844 ±0.001		
	2	A4	June 27-28	266.71	266.59	5.2	1.2	20.00	61	0.5008992	0.5008991	18	-269	5	-112	0.5009055	0.5009056			
	3	A4	June 28	266.18	266.18	5.2	3.3	19.90	61	0.5009040	0.5009041	16	-265	3	-112	0.5009067	0.5009068			
	4	A5	June 28	328.26	328.18	5.2	1.9	19.87	52	0.5007328	0.5007327	11	-208	11	-103	0.5007391	0.5007391			
	5	A5	June 28-29	327.96	328.94	5.2	1.9	19.85	58	0.5007335	0.5007335	11	-207	3	-103	0.5007381	0.5007386			
	6	A5	June 29	327.54	328.61	5.2	2.1	19.85	62	0.5007344	0.5007342	11	-214	2	-103	0.5007312	0.5007308			
	7	A6	June 29	342.76	342.76	5.2	2.0	20.10	55	0.5007345	0.5007345	11	-207	9	-106	0.500870	0.500876			
	8	A6	June 29-30	342.40	342.34	5.3	1.8	20.13	60	0.5007312	0.5007312	10	-215	7	-106	0.500878	0.500876			
No. 175, Lexington, Va., C. L. Garner.	1	A4	July 2	265.86	265.86	5.1	1.9	20.03	57	0.5007313	0.500848	11	-212	4	-106	0.5008578	0.5008698	979.861 ±0.001		
	2	A4	July 2-3	265.83	265.83	5.1	2.1	21.51	53	0.500431	0.500853	10	-273	11	-129	0.500908	0.5009023			
	3	A4	July 3	265.83	265.83	5.1	2.1	21.15	57	0.500432	0.500851	11	-258	4	-120	0.500910	0.500919			
	4	A5	July 3	327.21	327.21	5.2	2.0	20.87	60	0.5007325	0.5007325	11	-240	4	-120	0.500911	0.500919			
	5	A5	July 3-4	327.42	327.42	5.1	1.8	20.80	59	0.5007331	0.5007331	10	-239	2	-120	0.500913	0.500921			
	6	A5	July 4	326.46	326.46	5.0	1.8	20.63	62	0.5007345	0.5007345	10	-239	2	-120	0.500913	0.500921			
	7	A6	July 4-5	342.22	342.22	5.1	1.8	20.57	62	0.5007318	0.5007318	10	-239	2	-120	0.500913	0.500921			
	8	A6	July 5	342.12	342.12	5.0	1.8	20.57	62	0.5007318	0.5007318	10	-239	2	-120	0.500913	0.500921			
Washington, D. C., Coast and Geodetic Survey Office, C. L. Garner.	1	A4	July 5-6	342.89	342.89	5.1	1.8	20.47	62	0.5007303	0.5007303	10	-239	2	-120	0.500917	0.500922	979.859 ±0.001		
	2	A4	July 6	343.14	343.14	5.1	1.9	20.43	59	0.5007290	0.5007290	10	-238	5	-120	0.500921	0.500931			
	3	A4	July 6	343.14	343.14	5.1	1.8	20.37	59	0.5007296	0.5007296	9	-225	5	-120	0.500929	0.500930			
	4	A4	July 12	263.08	263.08	5.3	2.0	22.40	62	0.5008847	0.5008847	11	-352	6	-100	0.500879	0.500889			
	5	A4	July 12-13	263.18	263.18	5.2	1.8	22.36	62	0.5008847	0.5008847	11	-350	3	-100	0.500879	0.500889			
	6	A4	July 13	263.04	263.04	5.4	2.2	22.12	64	0.5008818	0.5008818	12	-340	3	-100	0.500888	0.500888			
	7	A5	July 13-14	324.91	324.91	5.2	1.9	22.12	64	0.5007351	0.5007351	11	-340	5	-100	0.500926	0.500926			
	8	A5	July 14	324.54	324.54	5.2	1.9	22.12	64	0.5007351	0.5007351	11	-340	5	-100	0.500926	0.500926			
No. 186, Aberdeen, S., Dak., C. L. Garner.	1	A4	Aug. 5	334.82	334.82	5.3	1.8	17.31	56	0.5007178	0.500900	10	-97	7	-121	0.5007248	0.5007262	980.550 ±0.001		
	2	A4	Aug. 5-6	333.90	332.50	5.2	1.8	17.28	61	0.5007303	0.500846	10	-96	3	-121	0.5007272	0.5007265			
	3	A4	Aug. 6	333.20	332.34	5.0	1.9	17.35	65	0.5007314	0.500846	10	-98	1	-121	0.5007265	0.5007262			
	4	A5	Aug. 6-7	432.32	432.32	5.2	2.0	17.68	57	0.5007590	0.5005102	11	-112	3	-128	0.5005119	0.5005117			
	5	A5	Aug. 7	432.61	432.61	5.2	1.9	17.87	61	0.5007590	0.5005105	11	-120	3	-128	0.5005127	0.5005126			
	6	A5	Aug. 7	431.44	431.72	5.4	2.1	18.00	64	0.5007591	0.5005105	11	-126	3	-128	0.5005127	0.5005127			
	7	A6	Aug. 7	458.48	458.48	5.2	1.9	18.17	59	0.5005458	0.5005458	11	-133	9	-124	0.5005189	0.5005188			
	8	A6	Aug. 7-8	458.16	458.16	5.3	1.9	18.20	59	0.5005462	0.5005462	11	-134	5	-124	0.5005190	0.5005189			

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Per- du- lum	Date	Coincidence interval		Total arc		Tem- pera- ture ° C.	Pres- sure mm.	Period uncorrected		Corrections (seventh decimal place)					Period corrected		Mean θ	Dynes
				Chro- no- meter No. 1828	Chro- no- meter No. 1838	Initial	Final			Arc	Tem- pera- ture	Rate		Chro- no- meter No. 1828	Flex- ure No. 1838	Chro- no- meter No. 1828	Mean			
												Chro- no- meter No. 1828	Chro- no- meter No. 1838							
No. 194, Huntley, Mont., C. L. Garner.	1	A4	Sept. 22, 1915	328.38	331.15	5.4	2.2	14.31	53	0.5007625	0.5007561	-12	+28	+10	8	+62	0.5007631	0.5007537	980.409	
	2	A4	Sept. 22, 1915	327.78	330.62	5.1	1.8	14.31	64	0.5007339	0.5007373	-11	+21	+1	8	+62	0.5007640	0.5007546	980.410	
	3	A4	Sept. 23, 1915	327.48	330.92	5.3	2.1	14.31	61	0.5007316	0.5007350	-11	+16	+5	8	+62	0.5007633	0.5007539	980.410	
	4	A5	Sept. 23, 1915	425.68	431.65	5.3	2.1	14.36	56	0.5005800	0.5005834	-11	+23	+7	23	+79	0.5005802	0.5005708	980.412	
	5	A5	Sept. 23, 1915	423.84	431.30	5.2	2.0	14.56	58	0.5005906	0.5005940	-11	+18	+5	23	+79	0.5005895	0.5005831	980.408	
	6	A5	Sept. 24, 1915	422.62	431.30	5.3	2.0	14.76	58	0.5005923	0.5005957	-11	+10	+5	23	+79	0.5005902	0.5005838	980.408	
	7	A6	Sept. 24, 1915	447.67	457.52	4.9	1.8	15.05	59	0.5005931	0.5005965	-9	+2	+4	38	+85	0.5005902	0.5005838	980.412	
	8	A6	Sept. 24, 1915	447.64	457.86	5.0	1.9	15.06	58	0.5005931	0.5005965	-10	+3	+4	38	+85	0.5005934	0.5005870	980.413	
	9	A6	Sept. 25, 1915	447.45	457.74	5.3	2.0	14.91	59	0.5005934	0.5005968	-11	+4	+5	38	+85	0.5005941	0.5005877	980.410	
No. 195, Lander, Wyo., C. L. Garner.	1	A4	Sept. 29, 1915	274.40	282.60	5.2	1.8	17.05	55	0.5009127	0.5009062	-10	86	+8	134	+126	0.5009095	0.5009030	979.916	
	2	A4	Sept. 29, 1915	274.96	282.48	5.4	2.1	16.96	54	0.5009109	0.5009044	-11	82	+9	134	+126	0.5009081	0.5009016	979.917	
	3	A4	Sept. 30, 1915	274.06	282.33	5.4	1.9	16.78	62	0.5009139	0.5009074	-11	75	+12	135	+126	0.5009111	0.5009046	979.910	
	4	A5	Sept. 30, 1915	340.10	352.74	5.4	2.0	16.78	51	0.5007962	0.5007897	-11	75	+12	135	+126	0.5007934	0.5007869	979.916	
	5	A5	Sept. 30, 1915	339.88	352.30	5.3	1.9	16.66	58	0.5007966	0.5007901	-11	70	+5	135	+126	0.5007938	0.5007873	979.913	
	6	A6	Oct. 1, 1915	340.42	352.80	5.2	1.9	16.56	58	0.5007955	0.5007890	-11	65	+5	135	+126	0.5007927	0.5007862	979.916	
	7	A6	Oct. 1, 1915	356.43	369.30	5.2	1.9	16.83	52	0.5007023	0.5006958	-11	77	+11	126	+123	0.5007000	0.5006935	979.913	
	8	A6	Oct. 1, 1915	356.36	369.38	5.3	1.8	16.78	62	0.5007025	0.5006960	-10	75	+12	126	+123	0.5007002	0.5006937	979.914	
	9	A6	Oct. 2, 1915	357.03	369.90	5.3	1.9	16.48	58	0.5007012	0.5006947	-11	62	+5	126	+123	0.5006984	0.5006919	979.912	
No. 198, Edgemont, S. Dak., C. L. Gar- ner.	1	A4	Oct. 5, 1915	300.88	307.58	5.5	2.4	15.24	54	0.5008323	0.5008258	-14	10	+3	101	+126	0.5008295	0.5008230	980.181	
	2	A4	Oct. 5, 1915	297.22	305.07	5.3	1.9	17.16	61	0.5008425	0.5008360	-11	90	+6	101	+126	0.5008397	0.5008332	980.180	
	3	A4	Oct. 6, 1915	285.26	303.38	5.2	2.1	18.35	57	0.5008481	0.5008416	-11	140	+6	101	+126	0.5008453	0.5008388	980.178	
	4	A4	Oct. 6, 1915	283.50	302.13	5.3	2.1	19.58	58	0.5008532	0.5008467	-11	192	+6	101	+126	0.5008504	0.5008439	980.183	
	5	A4	Oct. 6, 1915	292.46	301.30	5.3	2.0	20.40	57	0.5008583	0.5008518	-11	226	+2	101	+126	0.5008555	0.5008490	980.185	
	6	A4	Oct. 7, 1915	292.10	300.68	5.3	2.0	20.55	62	0.5008573	0.5008508	-11	233	+2	101	+126	0.5008545	0.5008480	980.184	
	7	A5	Oct. 7, 1915	307.00	301.50	5.5	2.0	20.90	55	0.5008621	0.5008556	-12	247	+3	106	+154	0.5008593	0.5008528	980.186	
	8	A5	Oct. 7, 1915	305.54	300.40	5.3	1.9	21.27	61	0.5008617	0.5008552	-11	263	+3	106	+154	0.5008589	0.5008524	980.185	
	9	A5	Oct. 8, 1915	307.27	301.74	5.2	2.1	20.70	60	0.5008617	0.5008552	-11	239	+4	106	+154	0.5008589	0.5008524	980.185	
No. 202, Moorcroft, Wyo., C. L. Garner.	1	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	2	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	3	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	4	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	5	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	6	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	7	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	8	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	
	9	A6	Oct. 8, 1915	307.58	303.32	5.3	2.0	20.20	57	0.5008458	0.5008393	-11	218	+7	117	+136	0.5008430	0.5008365	980.188	

No. 201. Wasta, S. Dak., C. L. Garner.										980.339 ±0.001										
1	A4	D	Oct. 20	322.30	320.89	5.3	1.9	12.17	02	3007789	5007367	11	+119	+1	58	+144	10	5007510	5007510	980.340
2	A4	D	Oct. 20-21	321.52	329.96	5.3	2.1	12.57	58	5007788	5007368	11	+102	+4	38	+144	10	5007510	5007510	980.336
3	A4	D	Oct. 21	321.87	329.66	5.4	1.9	12.75	58	5007784	5007365	11	+91	+4	38	+144	10	5007510	5007510	980.336
4	A5	D	Oct. 21	414.60	428.31	5.4	1.6	12.01	57	5006937	5005813	9	+88	+5	67	+130	10	5006937	5006937	980.344
5	A5	D	Oct. 21-22	412.87	426.82	5.5	1.9	13.17	57	5006933	5005814	12	+77	+7	66	+130	10	5006933	5006933	980.340
6	A5	D	Oct. 22	412.28	426.54	5.3	1.9	13.22	58	5006971	5005888	11	+75	+5	67	+130	10	5006971	5006971	980.339
7	A6	D	Oct. 22	435.74	451.31	5.5	2.0	13.38	57	5006754	5005315	12	+68	+6	69	+120	10	5006754	5006754	980.339
8	A6	D	Oct. 22-23	435.83	450.20	5.3	1.8	13.55	58	5005712	5005340	11	+60	+7	69	+120	10	5005712	5005712	980.339
9	A6	D	Oct. 23	435.79	450.37	5.1	1.8	13.57	59	5005713	5005358	11	+60	+7	69	+120	10	5005713	5005713	980.339
No. 206. Valentine, Nebr., C. L. Garner.										980.211 ±0.000										
1	A4	D	Oct. 26	294.96	306.22	5.4	2.2	20.49	57	5008180	5008177	12	+280	+7	107	+195	9	5008180	5008180	980.213
2	A4	D	Oct. 26-27	295.70	305.76	5.2	2.0	19.45	58	5008189	5008190	11	+228	+6	107	+195	9	5008189	5008189	980.210
3	A4	D	Oct. 27	295.75	306.27	5.2	2.0	19.95	58	5008188	5008190	11	+228	+6	107	+195	9	5008188	5008188	980.210
4	A5	D	Oct. 27	371.94	390.03	5.2	2.1	20.33	58	5008176	5008176	11	+223	+6	109	+189	9	5008176	5008176	980.211
5	A5	D	Oct. 27-28	370.74	388.00	5.2	2.0	20.69	58	5008172	5008172	11	+218	+6	109	+189	9	5008172	5008172	980.210
6	A5	D	Oct. 28	371.92	388.16	5.4	1.9	20.30	58	5008176	5008176	11	+218	+6	109	+189	9	5008176	5008176	980.210
7	A6	D	Oct. 28	371.92	388.16	5.4	1.9	20.30	58	5008176	5008176	11	+218	+6	109	+189	9	5008176	5008176	980.210
8	A6	D	Oct. 28-29	391.54	410.20	5.1	1.9	20.35	55	5008393	5008102	10	+224	+2	110	+174	9	5008393	5008393	980.212
9	A6	D	Oct. 29	392.28	410.15	5.1	1.7	20.07	65	5008381	5008103	9	+289	+1	110	+174	9	5008381	5008381	980.219
No. 205. Randolph, Nebr., C. L. Garner.										980.236 ±0.000										
1	A4	D	Nov. 2	302.48	310.14	5.5	2.2	17.42	56	5008270	5008074	13	+101	+7	85	+123	12	5008075	5008075	980.236
2	A4	D	Nov. 2-3	301.92	309.75	5.2	2.1	17.80	67	5008294	5008074	8	+122	+6	85	+123	12	5008071	5008069	980.235
3	A4	D	Nov. 3	301.01	308.00	5.1	2.8	18.00	67	5008316	5008106	13	+126	+3	85	+123	12	5008081	5008075	980.235
4	A5	D	Nov. 3	390.91	394.41	5.3	2.0	18.07	63	5006572	5006316	11	+139	+1	94	+136	12	5006317	5006321	980.237
5	A5	D	Nov. 3-4	390.08	393.82	5.3	2.0	18.37	58	5006586	5006336	11	+134	+5	94	+136	12	5006320	5006320	980.237
6	A5	D	Nov. 4	378.02	392.96	5.3	2.0	18.37	58	5006586	5006336	11	+134	+5	94	+136	12	5006320	5006320	980.237
7	A6	D	Nov. 4	402.95	416.30	5.3	1.9	18.37	56	5006227	5006012	11	+150	+1	82	+134	12	5006329	5006326	980.235
8	A6	D	Nov. 4-5	401.77	415.98	5.3	1.9	18.37	56	5006227	5006012	11	+150	+1	82	+134	12	5006329	5006329	980.237
9	A6	D	Nov. 5	402.36	417.02	5.1	1.6	18.30	58	5006221	5006032	11	+131	+1	82	+134	12	5006360	5006358	980.234
No. 208. Leon, Iowa, C. L. Garner.										980.133 ±0.001										
1	A4	D	Nov. 10	284.84	294.75	5.4	2.2	23.35	53	5008586	5008196	12	+350	+11	189	+296	11	5008335	5008310	980.133
2	A4	D	Nov. 10-11	290.49	293.96	5.2	2.0	24.15	61	5008580	5008196	11	+351	+4	189	+296	11	5008340	5008338	980.136
3	A4	D	Nov. 11	290.91	293.77	5.2	2.0	23.74	63	5008316	5008319	11	+306	+2	189	+296	11	5008315	5008313	980.131
4	A5	D	Nov. 11	331.44	373.14	5.3	2.1	23.06	59	5007124	5007090	11	+319	+6	195	+296	11	5006755	5006768	980.140
5	A5	D	Nov. 11-12	331.44	373.14	5.3	2.1	22.62	59	5007115	5007110	11	+319	+6	195	+296	11	5006755	5006758	980.134
6	A5	D	Nov. 12	331.39	373.04	5.2	1.9	21.37	58	5007064	5006758	11	+275	+4	195	+296	11	5006756	5006761	980.134
7	A6	D	Nov. 12	371.51	393.72	5.2	2.1	21.92	56	5006738	5006758	11	+240	+8	171	+186	11	5006232	5006240	980.131
8	A6	D	Nov. 12-13	372.46	393.34	5.2	2.0	21.96	59	5006721	5006755	11	+251	+5	171	+186	11	5006236	5006246	980.129
9	A6	D	Nov. 13	374.51	394.14	5.2	1.9	21.00	60	5006834	5006831	11	+251	+4	171	+186	11	5006244	5006256	980.129
No. 209. Laurel, Md., C. L. Garner.										980.119 ±0.001										
1	A4	D	Nov. 18	280.32	299.14	5.5	2.3	18.30	65	5008576	5008371	13	+135	+1	127	+178	13	5008384	5008381	980.119
2	A4	D	Nov. 18-19	287.38	297.03	5.1	1.8	18.57	62	5008718	5008403	9	+101	+1	2	+178	13	5008777	5008770	980.119
3	A5	D	Nov. 19	285.54	296.58	5.1	2.2	20.76	61	5008771	5008414	12	+211	+3	127	+178	13	5008777	5008770	980.121
4	A5	D	Nov. 19	332.86	369.45	5.3	2.0	22.61	65	5006765	5006775	11	+320	+9	130	+200	13	5006760	5006763	980.114
5	A5	D	Nov. 19-20	332.64	369.45	5.4	2.0	22.62	62	5006769	5006783	11	+319	+5	130	+200	13	5006761	5006765	980.112
6	A5	D	Nov. 20	333.00	370.69	5.3	2.1	22.38	62	5006762	5006764	11	+319	+5	130	+200	13	5006761	5006765	980.115
7	A6	D	Nov. 20	370.13	390.00	5.2	2.0	23.16	57	5006763	5006765	11	+319	+5	130	+200	13	5006761	5006765	980.123
8	A6	D	Nov. 20-21	369.36	388.38	5.2	1.9	23.49	59	5006778	5006765	11	+312	+6	130	+200	13	5006779	5006780	980.125
9	A6	D	Nov. 21	368.92	388.00	5.1	1.9	23.38	61	5006780	5006765	10	+351	+4	130	+200	13	5006782	5006780	980.128
10	A6	D	Nov. 21	368.90	388.22	5.1	1.8	23.64	64	5006787	5006765	10	+351	+4	130	+200	13	5006782	5006780	980.128
11	A6	D	Nov. 21-22	367.46	397.60	5.1	1.9	23.69	63	5006813	5006772	9	+362	+6	135	+205	13	5006784	5006780	980.113
12	A6	D	Nov. 22	368.66	397.90	5.2	1.8	23.69	63	5006791	5006768	11	+339	+2	135	+205	13	5006795	5006802	980.113
No. 212. Rockville, Md., C. L. Garner.										980.111 ±0.001										
1	A4	D	Nov. 27	280.04	298.75	5.4	2.2	17.80	59	5008335	5008392	12	+117	+7	88	+148	12	5008394	5008402	980.108
2	A4	D	Nov. 27-28	290.38	298.30	5.2	1.9	17.90	60	5008325	5008392	11	+122	+4	88	+148	12	5008396	5008396	980.110
3	A4	D	Nov. 28	291.56	299.16	5.4	2.2	17.41	60	5008380	5008392	12	+101	+4	88	+148	12	5008398	5008398	980.111
4	A5	D	Nov. 28	396.78	379.39	5.3	2.1	16.80	65	5006925	5006920	11	+79	+1	97	+136	12	5006925	5006929	980.115
5	A5	D	Nov. 28-29	396.80	379.38	5.3	2.0	16.91	60	5006925	5006928	11	+80	+1	97	+136	12	5006925	5006929	980.115
6	A5	D	Nov. 29	395.14	378.87	5.1	2.1	17.15	59	5006936	5006928	10	+90	+4	97	+136	12	5006932	5006934	980.111
7	A6	D	Nov. 29	381.06	397.34	5.1	2.1	17.74	60	5006938	5006928	10	+115	+4	97	+136	12	5006939	5006939	980.108
8	A6	D	Nov. 29-30	381.87	398.11	4.9	1.7	17.51	62	5006953	5006940	10	+106	+2	127	+142	12	5006953	5006954	980.111
9	A6	D	Nov. 30	383.08	399.64	5.1	1.6	16.98	63	5006954	5006940	10	+106	+2	127	+142	12	5006953	5006954	980.111
No. 214. Fairfax, Va., C. L. Garner.										980.079 ±0.001										
1	A4	D	Dec. 3	311.78	318.22	5.5	2.0	4.16	61	5009331	5007889	12	+454	0	16	+185	9	5008180	5008187	980.076
2	A4	D	Dec. 3-4	310.61	317.28	5.3	1.8	4.74	63	5009332	5007892	10	+430	-2	16	+185	9	5008187	5008186	980.077
3	A4	D	Dec. 4	317.38	317.58	5.5	2.4	4.79	52	5009331	5007881	14	+128	+3	16	+185	9	5008180	5008187	980.077
4	A5	D	Dec. 4	400.00	410.79	5.3	1.3	4.39	61	5009258	5008993	8	+415	+1	26	+193	9	5008769	5008771	980.081
5	A5	D	Dec. 4-5	399.46	410.33	5.3	1.0	4.44	60	5009258	5008993	8	+415	+1	26	+193	9	5008769	5008771	980.081
6	A5	D	Dec. 5	399.89	411.36	5.9	1.5	4.26	60	5009259	5008995	11	+450	+4	38	+197	9	5008770	5008772	980.079
7	A6	D	Dec. 5	421.71	436.26	5.1														

Pendulum observations and reductions—Continued.

Station and observer	Swing No.	Pen- du- lum	Post- tion	Date	Coincidence In- terval		Total arc		Tem- pera- ture	Pres- sure	Period uncorrected		Corrections (seventh decimal place)					Period corrected		θ	Mean θ	
					Chro- no- meter No. 1828	Chro- no- meter No. 1838	Initial	Final			Chromom- eter No. 1828	Chromom- eter No. 1838	Arc	Tem- pera- ture	Pres- sure	Rate		Chronom- eter No. 1828	Chronom- eter No. 1838			
																Chro- no- meter No. 1828	Flex- ure No. 1838		Chronom- eter No. 1828			Mean
No. 213, Upper Marl- boro, Md., C. L. Gar- ner.	1	A4	D	1915 Dec. 11-12	319.25	321.44	mm.	mm.	3.14	64	0.5007846	0.5007701	-11	+497	-	+131	+197	0.5008142	0.5008145	Dynes	980.090	
	2	A4	D	Dec. 12-13	320.09	322.78	5.2	2.3	2.87	58	0.5007822	0.5007757	-6	+508	-	+131	+197	0.5008111	0.5008110	980.093		
	3	A4	D	Dec. 12-13	320.09	322.78	5.2	0.7	2.87	58	0.5007822	0.5007757	-6	+508	-	+131	+197	0.5008111	0.5008110	980.089		
	4	A5	D	Dec. 12-13	408.46	415.98	5.6	2.1	2.74	63	0.5007138	0.5007017	-12	+511	-	+3	+188	0.5007703	0.5007703	980.084		
	5	A5	D	Dec. 12-13	408.46	415.98	5.6	2.1	3.07	65	0.5007138	0.5007017	-12	+511	-	+3	+188	0.5007703	0.5007703	980.082		
	6	A5	D	Dec. 12-13	408.46	415.98	5.6	2.2	3.31	61	0.5007138	0.5007017	-12	+511	-	+3	+188	0.5007703	0.5007703	980.079		
	7	A6	D	Dec. 13-14	426.24	438.23	5.2	1.8	3.27	59	0.5005872	0.5005711	-10	+469	-	+2	+59	0.5006372	0.5006372	980.083		
	8	A6	D	Dec. 13-14	426.24	438.23	5.2	1.9	3.41	59	0.5005872	0.5005711	-10	+469	-	+2	+59	0.5006372	0.5006372	980.081		
	9	A6	D	Dec. 13-14	426.22	439.07	5.1	2.0	3.64	62	0.5005873	0.5005700	-10	+470	-	+6	+59	0.5006372	0.5006372	980.083		
No. 219, Hagerstown, Md., C. L. Garner.	1	A4	D	1916 Jan. 8-9	280.91	291.58	5.7	2.5	20.36	49	0.5008016	0.5007859	-14	-225	14	-111	+194	0.5008371	0.5008371	Dynes	980.046	
	2	A4	D	Jan. 8-9	282.36	291.85	5.3	1.9	19.97	55	0.5008070	0.5007906	-11	-208	9	-111	+194	0.5008310	0.5008310	980.051		
	3	A4	D	Jan. 9-10	282.73	292.36	5.2	2.1	19.65	50	0.5008058	0.5007906	-11	-195	8	-111	+196	0.5008310	0.5008310	980.032		
	4	A5	D	Jan. 9-10	351.14	365.02	5.4	2.0	19.03	56	0.5007131	0.5006977	-9	-207	8	-96	+196	0.5008094	0.5008094	980.043		
	5	A5	D	Jan. 9-10	351.08	366.16	5.2	1.4	20.33	58	0.5007131	0.5006977	-9	-223	6	-96	+196	0.5008094	0.5008094	980.049		
	6	A5	D	Jan. 10-11	319.82	365.44	5.2	2.8	20.57	59	0.5007157	0.5006994	-14	-233	5	-96	+196	0.5008100	0.5008100	980.048		
	7	A6	D	Jan. 10-11	363.76	383.11	5.1	1.9	20.85	54	0.5008455	0.5008334	-10	-245	10	-121	+207	0.5008170	0.5008170	980.012		
	8	A6	D	Jan. 10-11	364.06	383.70	5.0	1.8	21.27	56	0.5008460	0.5008321	-9	-263	8	-121	+207	0.5008166	0.5008166	980.019		
	9	A6	D	Jan. 11-12	364.06	382.96	5.2	2.0	21.53	57	0.5008476	0.5008337	-11	-274	7	-121	+207	0.5008468	0.5008468	980.019		
Washington, D. C., Coast and Geodetic Survey Office, C. L. Garner.	1	A4	D	1919 Jan. 19-20	301.79	310.51	5.3	2.1	9.59	62	0.5008297	0.5008064	-11	+227	0	-114	+131	0.5008389	0.5008389	Dynes	980.035	
	2	A4	D	Jan. 19-20	301.77	310.51	5.0	1.8	9.83	48	0.5008268	0.5008030	-9	+217	14	-114	+131	0.5008366	0.5008366	980.034		
	3	A4	D	Jan. 20-21	301.22	310.58	5.4	1.3	10.01	57	0.5008313	0.5008073	-11	+209	14	-114	+131	0.5008383	0.5008383	980.034		
	4	A5	D	Jan. 20-21	381.10	395.68	5.0	1.0	10.40	66	0.5008569	0.5008323	-9	+197	5	-120	+133	0.5008632	0.5008632	980.036		
	5	A5	D	Jan. 20-21	379.72	395.64	4.5	1.3	10.60	71	0.5008503	0.5008367	-8	+184	4	-120	+133	0.5008610	0.5008610	980.036		
	6	A5	D	Jan. 21-22	378.72	394.64	4.5	1.3	10.60	71	0.5008503	0.5008367	-8	+184	4	-120	+133	0.5008610	0.5008610	980.036		
	7	A6	D	Jan. 21-22	307.63	414.46	5.1	1.5	11.34	63	0.5008265	0.5008039	-8	+153	1	-139	+131	0.5008260	0.5008260	980.027		
	8	A6	D	Jan. 21-22	305.11	413.20	5.1	1.5	12.00	60	0.5008385	0.5008101	-10	+126	2	-139	+131	0.5008305	0.5008305	980.030		
	9	A6	D	Jan. 22-23	302.02	410.28	5.2	2.2	12.65	73	0.5008320	0.5008085	-12	+98	10	-139	+131	0.5008312	0.5008312	980.034		
	1	A6	D	Feb. 4-5	305.76	411.37	5.2	1.9	12.46	53	0.5008325	0.5008092	-9	+106	7	-116	+138	0.5008304	0.5008304	980.028		
	2	A6	D	Feb. 4-5	305.76	411.37	5.1	1.8	12.56	55	0.5008325	0.5008092	-9	+106	7	-116	+138	0.5008304	0.5008304	980.028		
	3	A6	D	Feb. 5-6	306.00	413.13	5.0	1.8	12.33	58	0.5008321	0.5008089	-9	+112	4	-116	+138	0.5008302	0.5008302	980.028		

Chapter II.—DESCRIPTIONS OF STATIONS.

There are given below the descriptions of the 219 stations in the United States with the years in which they were established. The description is designed to enable one to recover the place where the pendulums were swung. The numbering of the stations is the same as that used in other parts of this volume.

No. 1, *Key West, Fla.* (1896).—Post office, southeast basement room. The case was mounted on the concrete floor.

No. 2, *West Palm Beach, Fla.* (1909).—Zapf's Opera House, room in basement under north part of building. The case was mounted on a concrete pier against a stone wall.

No. 3, *Punta Gorda, Fla.* (1909).—Punta Gorda Hotel, in the space partly walled in under the main entrance. The case was mounted on a low pier of concrete and brick against a buttress of the wall.

No. 4, *Apalachicola, Fla.* (1909).—Observatory pendulum room on Weather Bureau signal grounds near the center of the Florida Promenade Park between Fifth and Sixth Avenues and First and Second Streets, extended. The case was mounted on a low brick pier.

No. 5, *New Orleans, La.* (1895).—City Hall, hallway in basement of building. The case was mounted on the slate floor.

No. 6, *Rayville, La.* (1909).—Dr. J. H. Wilkins's office, medicine room in southeast corner of small one-story brick building south of the Vicksburg, Shreveport & Pacific Railway tracks and three and one-half telegraph poles west of the crossing of the Vicksburg, Shreveport & Pacific and the St. Louis, Iron Mountain & Southern Railways. The case was mounted on bricks cemented together and to the concrete floor.

No. 7, *Galveston, Tex.* (1895).—Ball High School, storeroom on the ground floor. The case was mounted on the concrete floor.

No. 8, *Point Isabel, Tex.* (1909).—Constructed pendulum room 2.65 meters north and 0.67 meter west of the longitude pier used by Assistant Smith in 1906 and about 110 meters north of the lighthouse. The case was mounted on a low concrete pier.

No. 9, *Laredo, Tex.* (1895).—Commissary of Fort McIntosh, room in the basement. The case was mounted on a low brick pier build against the foundation wall.

No. 10, *Austin, Tex. (capitol)* (1895).—Capitol Building, basement room southeast of the rotunda. The case was mounted on the concrete floor.

No. 11, *Austin, Tex. (university)* (1895).—University of Texas, main building, Aquarium room in basement. The case was mounted on the corner of a concrete wall.

No. 12, *McAlester, Okla.* (1909).—High school just east of the Masonic Temple, northeast corner of the shower-bath room on the ground floor. The case was mounted on three 6-inch cube stone blocks, each cemented to the concrete floor.

No. 13, *Little Rock, Ark.* (1896 and 1914).—Post office, north center basement room. The case was mounted on the concrete floor.

No. 14, *Columbia, Tenn.* (1909).—Old dormitory of the high and public school, in southeast corner of basement near bathing tank. The case was mounted on three 6-inch concrete blocks, each cemented to the concrete floor.

No. 15, *Atlanta, Ga.* (1896).—State Capitol, northwest basement room of the Washington Street wing. The case was mounted on the asphaltum floor.

No. 16, *McCormick, S. C.* (1909).—McCormick oil mill of the Anderson Phosphate Co., four and one-half telegraph poles west of the Charleston & Western Carolina Railway depot, in the southeast corner of the furnace room at the south end of the building. The case was mounted on a low brick pier.

No. 17, *Charleston, S. C.* (1896).—South Carolina Military Academy (citadel), storeroom in the southwest corner of the ground floor. The case was mounted on the brick floor.

No. 18, *Beaufort, N. C.* (1909).—Masonic Hall on Turner Street, one block south of the courthouse; small room near the center of the north side of the basement. The case was mounted on a low concrete pier.

No. 19, *Charlottesville, Va.* (1894).—University of Virginia, basement of biological laboratory. The case was mounted on a low brick pier.

No. 20, *Deer Park, Md.* (1894).—East corner of swimming-pool building west of the Deer Park Hotel. The case was mounted on a low stone pier.

No. 21, *Washington, D. C.* (1900).—Office of the United States Coast and Geodetic Survey, New Jersey Avenue and B Street SE., pendulum room in southwest corner of basement. The case was mounted on a massive brick pier.

No. 22, *Washington, D. C. (Smithsonian Institution)* (1891).—Northeast basement of the Smithsonian Institution. The case was mounted on a brick pier.

No. 23, *Baltimore, Md.* (1893).—Johns Hopkins University, basement of the physical laboratory. The case was probably mounted on a brick or masonry pier.

No. 24, *Philadelphia, Pa.* (1894).—University of Pennsylvania, small room in northwest corner of basement of College Hall. The case was mounted on the concrete floor.

No. 25, *Princeton, N. J.* (1894).—College of New Jersey, basement of magnetic observatory or electrical building. The case was mounted on a tall brick pier.

No. 26, *Hoboken, N. J.* (1891).—Basement of the Stevens Institute of Technology. The case was probably mounted on a brick or masonry pier.

No. 27, *New York, N. Y.* (1899).—Columbia University, in a small room in the sub-basement near the center of the front of the Physics Building. The case was mounted on a brick pier.

No. 28, *Worcester, Mass.* (1899).—Worcester Polytechnic Institute, in the southwest corner of the constant temperature room of the physical laboratory which is near the middle of the north side of the basement. The case was mounted on a stone pier.

No. 29, *Boston, Mass.* (1894).—New addition to State house, vault in northeast part of basement. The case was mounted on the concrete floor.

No. 30, *Cambridge, Mass.* (1894).—Harvard College Observatory, basement room north of equatorial foundation. The case was mounted on the heavy stone doorsill.

No. 31, *Calais, Me.* (1895).—Basement of high-school building. The case was mounted on the concrete floor.

No. 32, *Ithaca, N. Y.* (1894).—Cornell University, in the metric room in the northeast part of the basement of Lincoln Hall. The case was mounted on a tall brick pier.

No. 33, *Cleveland, Ohio* (1894).—Adelbert College, in balance room in the west corner of the basement. The case was mounted on a large brick pier with capstone.

No. 34, *Cincinnati, Ohio* (1894).—Cincinnati Observatory on Mount Lookout, in the basement north of the foundation of the meridian circle. The case was mounted on a low brick pier built on the brick floor.

No. 35, *Terre Haute, Ind.* (1894).—Rose Polytechnic Institute, in the west room of the basement of the main building. The case was mounted on a large brick pier with slate top.

No. 36, *Chicago, Ill.* (1894).—University of Chicago, constant temperature room in the northeast part of the main floor of the Ryerson Physical Laboratory. The case was mounted on a massive brick pier with capstone.

No. 37, *Madison, Wis.* (1906).—University of Wisconsin, in the basement of Science Hall. The case was mounted on a brick pier.

No. 38, *St. Louis, Mo.* (1894).—Washington University, in the south basement room of the chemical laboratory, which is near the northwest corner of St. Charles and Seventeenth Streets. The case was mounted on a low pier built on the brick floor.

No. 39, *Kansas City, Mo.* (1894).—Franklin School at the northeast corner of Washington Avenue and Fourteenth Street, in a small storeroom in the south part of the basement. The case was mounted on bricks cemented to the concrete floor.

No. 40, *Ellsworth, Kans.* (1894).—Ellsworth County courthouse, near the center of the basement. The case was mounted on a large stone doorsill.

No. 41, *Wallace, Kans.* (1894).—Stone residence northwest of station belonging to the Union Pacific Railway, in the basement. The case was mounted on a stone doorsill.

No. 42, *Colorado Springs, Colo.* (1894).—Colorado College, small room near northeast corner of basement of Hagerman Hall. The case was mounted on a low pier built on the concrete floor.

No. 43, *Pikes Peak, Colo.* (1894).—Small storeroom at south end of stone building on the east side of the summit. The case was mounted on large stones cemented to the concrete floor.

No. 44, *Denver, Colo.* (1894).—University of Denver, in the basement of Chamberlin Observatory south of the equatorial foundation. The case was mounted on large stones cemented to the concrete floor.

No. 45, *Gunnison, Colo.* (1894).—La Veta Hotel, small room beneath the sidewalk at the northeast corner. The case was mounted on a heavy stone doorsill.

No. 46, *Grand Junction, Colo.* (1894).—Brunswick Hotel, on Main Street west of Fourth Street, in the cellar under the northeast corner. The case was mounted on a low brick pier.

No. 47, *Green River, Utah* (1894).—Palmer House, in the east corner of the cellar under the south part of the building. The case was mounted on a low brick pier built on the concrete floor.

No. 48, *Pleasant Valley Junction, Utah* (1894).—Residence of T. Arrowsmith, about 65 meters north of the Rio Grande Western Railway station, in the west corner of the cellar. The case was mounted on a low brick pier.

No. 49, *Salt Lake City, Utah* (1894).—Small astronomical observatory in the southeast corner of Temple Block. The case was mounted on a stone pier 1 meter high.

No. 50, *Grand Canyon, Wyo.* (1894).—Canyon Hotel, in Yellowstone Park, in the unfinished basement at the west end of the main building. The case was mounted on a low brick pier.

No. 51, *Norris Geyser Basin, Wyo.* (1894).—In Yellowstone Park, in a small room at the entrance to the storehouse west of the lunch station at Norris Geyser Basin. The case was mounted on three wooden posts driven into the ground and braced.

No. 52, *Lower Geyser Basin, Wyo.* (1894).—Fountain Hotel, in Yellowstone Park, in an unfinished room in the basement at the north end of the central wing. The case was mounted on a low brick pier.

No. 53, *Seattle, Wash. (university)* (1899).—Washington State University, just northeast of Lake Union, in the physical laboratory which is near the east end of the basement of the main building. The case was mounted on a masonry pier with marble top.

No. 54, *San Francisco, Cal.* (1891).—This station is probably located in the Davidson Observatory in Lafayette Park. The case was mounted on a brick pier.

No. 55, *Mount Hamilton, Cal.* (1891).—Lick Observatory, on Mount Hamilton. The case was mounted on a brick pier.

No. 56, *Seattle Wash. (high school)* (1891 and 1899).—High-school building, in a small room used for storing arms partitioned off from the northwest room of the basement. The case was mounted on the concrete floor.

No. 57, *Iron River, Mich.* (1909 and 1910).—High school, just north of the center of town and two blocks west of the railway depot, in a small room in the basement, which is near the foot of the stairway leading from the western one of the main entrances to the basement floor. The case was mounted on three bricks cemented to the concrete floor, one brick under each footplate.

No. 58, *Ely, Minn.* (1909).—High school, 1905, small storage room under stair landing in west end of basement. The case was mounted on the concrete floor.

No. 59, *Pembina, N. Dak.* (1909).—Public school, also used as high school, temporary room constructed in west corner of the basement. The case was mounted on low concrete pier.

No. 60, *Mitchell, S. Dak.* (1909).—Dakota Wesleyan University, College Hall 1889, chemical storeroom in the south side of the basement about 30 feet from the southwest corner of the building. The case was mounted on the concrete floor.

No. 61, *Sweetwater, Tex.* (1910).—Cyclone cellar of Russell Rhoades just to the rear of his dwelling, which is the second house on the east side of the street leading south from the Texas & Pacific Railway tracks to the Sweetwater Mineral Springs Park. The case was mounted on the concrete floor.

No. 62, *Kerrville, Tex.* (1910).—Lowry Block, a little south of the courthouse grounds, in the basement. The case was mounted on the concrete floor.

No. 63, *El Paso, Tex.* (1910).—El Paso High School, North Kansas and Arizona Streets, small room under stairway in the southwest side of the basement and near the outside basement door. The case was mounted on the concrete floor.

No. 64, *Nogales, Ariz.* (1910).—Public-school building, small room used as library and storeroom in the south side of the basement. The case was mounted on a concrete pier.

No. 65, *Yuma, Ariz.* (1910).—Public-school building, corner of Second Avenue and Third Street, a temporary room constructed in the southeast corner of the basement room which is to be used for manual training. The case was mounted on the concrete floor.

No. 66, *Compton, Cal.* (1910).—High school, in the northeast corner of the southwest corner room of the basement. The case was mounted on the concrete floor.

No. 67, *Goldfield, Nev.* (1910).—High school, corner of Ramsey and Euclid Streets, in small oil room on the boys' side of the basement near the northwest side of the building. The case was mounted on the concrete floor.

No. 68, *Yavapai, Ariz.* (1910).—Yavapai Point, in small tunnel on the rim of the Grand Canyon, 1.2 miles east of El Tovar Hotel. The case was mounted on three stones cemented to the rocky floor of the tunnel.

No. 69, *Grand Canyon, Ariz.* (1910).—Bright Angel trail, in a tunnel on the mining claim of Mr. Cameron near the bottom of the Grand Canyon, 55 paces west from the steep part of the trail known as the "corkscrew" and 12 feet above the bed of a creek. The case was mounted on three stones embedded in a 4-inch layer of concrete on the rocky floor of the tunnel.

No. 70, *Gallup, N. Mex.* (1910).—Public-school building, temporary room constructed in the northeast corner of the basement. The case was mounted on a low concrete pier.

No. 71, *Las Vegas, N. Mex.* (1910).—Normal school on Main Street between Eighth and Ninth Streets, East Las Vegas, girls' dormitory, a temporary room constructed in the southeast corner of the west room of the basement. The case was mounted on the concrete floor.

No. 72, *Shamrock, Tex.* (1910).—Cyclone cellar near the northwest corner of the residence of E. H. Small, about one-half mile southwest of the main part of Shamrock. The case was mounted on the concrete floor.

No. 73, *Denison, Tex.* (1910).—High school, northwest corner of Main Street and Barrell Avenue, in basement storeroom between the physical and chemical laboratories. The case was mounted on three concrete blocks, each cemented to the concrete floor.

No. 74, *Minneapolis, Minn.* (1910).—University of Minnesota, constant temperature room, near the center of the basement of the physical laboratory. The case was mounted on a stone plinth 4 inches thick cemented to the tile floor.

No. 75, *Lead, S. Dak.* (1910).—High-school building, vault near the middle of the east side of the basement. The case was mounted on three concrete blocks molded in place on the concrete floor.

No. 76, *Bismarck, N. Dak.* (1910).—Will School building, superheating room, center of basement. The case was mounted on a low concrete pier.

No. 77, *Hinsdale, Mont.* (1910).—Public school, middle of the north side of the basement. The case was mounted on a low concrete pier.

No. 78, *Sandpoint, Idaho* (1910).—Farmington Central School, alcove under the stairs of the main entrance in the middle of the north side of the basement. The case was mounted on three bricks, each cemented to the concrete floor.

No. 79, *Boise, Idaho* (1910).—High-school building, new (1908) east wing of boys' dressing room in south part of basement directly under the Tenth Street entrance. The case was mounted on three bricks, each cemented to the concrete floor.

No. 80, *Astoria, Oreg.* (1910).—Federal Building (customhouse and post office), temporary room constructed in the west part of the basement. The case was mounted on three bricks, each cemented to the concrete floor.

No. 81, *Sisson, Cal.* (1910).—Sisson Tavern at Berryvale, about 1 mile west and $\frac{1}{4}$ mile south of the Sisson railroad station, a temporary room constructed in the basement under the southwest corner of the main part of the building. The case was mounted on a concrete pier.

No. 82, *Rock Springs, Wyo.* (1910).—City Hall, room near the middle of the southeast side of the basement and just east of the boiler room. The case was mounted on a low concrete pier.

No. 83, *Paxton, Nebr.* (1910).—Globe Hotel, cellar under the storehouse at the rear of the hotel. The case was mounted on three bricks, each cemented to the concrete floor.

No. 84, *Washington, D. C. (Bureau of Standards)*, (1910).—Room No. 16, near the center of the basement of the physical laboratory or main building. The case was mounted with one brick under each footplate cemented to the concrete floor.

No. 85, *North Hero, Vt.* (1909 and 1910).—Irving House, middle of east side of the east room of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 86, *Lake Placid, N. Y.* (1909).—Lake Placid Inn, storeroom in the east corner of the basement directly below the hotel dining room. The case was mounted on a low concrete pier.

No. 87, *Potsdam, N. Y.* (1909).—Clarkson School of Technology, photometric room, on the ground floor, directly north of north entrance to the furnace room. The case was mounted on a stone pier composed of two large stone blocks resting on the concrete floor.

No. 88, *Wilson, N. Y.* (1909).—Wilson High School, middle furnace room in the center of the basement. The case was mounted on a low concrete pier.

No. 89, *Alpena, Mich.* (1909).—City hall, alcove under steps at the northwest end of the basement hall and just to the left of the entrance to the office of chief of police. The case was mounted on the concrete floor.

No. 90, *Virginia Beach, Va.* (1911).—Arlington Hotel, temporary room constructed in the northeast corner of the basement of the north wing. The case was mounted on low concrete pier which in turn rested on the brick floor.

No. 91, *Durham, N. C.* (1911).—Trinity College, Academic Building, small room in middle of east end of basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 92, *Fernandina, Fla.* (1911).—Federal Building, northeast corner of Center and Fourth Streets, coal room in the southeast corner of the basement. The case was mounted on three bricks each cemented to the concrete floor.

No. 93, *Wilmer, Ala.* (1911 and 1915).—Abandoned ice house at the east end of the post office, which is located at the point where the main road from the railway station turns to the westward. The case was mounted on a brick pier.

No. 94, *Aliceville, Ala.* (1911).—Constructed pendulum room located on a public highway or West First Street, 47.5 feet north of the building line on the north side of Third Avenue and 23 feet west of the building line on the east side of West First Street. The case was mounted on a concrete pier.

No. 95, *New Madrid, Mo.* (1911).—High-school building, furnace room in the basement at the west end of the west wing. The case was mounted on three bricks each cemented to the concrete floor.

No. 96, *Mena, Ark.* (1911).—High-school building, southwest corner of Eleventh Street and Magnolia Avenue, furnace room in the basement under the east end of the building. The case was mounted on three bricks each cemented to the concrete floor.

No. 97, *Nacogdoches, Tex.* (1911).—M. E. Church on Hospital and Pecan Streets, small room off the west end of the vestry in the north end of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 98, *Alpine, Tex.* (1911).—High-school building at the foot of Sixth Street, small basement room in the middle of the west side of the building directly under the west entryway. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 99, *Farwell, Tex.* (1911).—Farwell Hotel at the southwest corner of the public square, basement room in southwest corner of the building, which is unoccupied. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 100, *Guymon, Okla.* (1911).—Summers Building, small inside room off the northeast corner of the barber shop. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 101, *Helenwood, Tenn.* (1911).—Observatory pendulum room on the premises of Mr. Duncan, directly opposite the railroad station at Helenwood, 40 feet south of Mr. Duncan's north fence line and 16 feet west of his east fence line and about 400 feet east of the railroad station. The case was mounted on a pier of concrete building blocks.

No. 102, *Cloudland, Tenn.* (1909).—Summit of Roan Mountain, Old Cloudland Hotel, northwest corner of the southeast room on the ground floor. The case was mounted on a concrete pier.

No. 103, *Hughes, Tenn.* (1909 and 1911).—Observatory pendulum room on Lewis Hughes's farm, in the corner of his pasture lot, and about 75 feet due east of the north end of his house, which is the first house on the east side of Cove Creek just south of its junction with Doe River, $1\frac{1}{4}$ miles east of Hughes Gap and $1\frac{3}{4}$ miles west by south from Burbank. The case was mounted on a concrete pier.

No. 104, *Charleston, W. Va.* (1911).—High-school building on Quarrier Street near Broad Street, boys' coat room in the basement under the boys' entrance on the northwest side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 105, *State College, Pa.* (1911).—Chemistry-Physics Building of Pennsylvania State College, photometer room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 106, *Fort Kent, Me.* (1909).—Dickey Hotel, in the north corner of the basement directly under the hotel office. The case was mounted on a low concrete pier.

No. 107, *Prentice, Wis.* (1911).—Public-school building, room in the basement under the east entrance to the building. The case was mounted on a concrete pier.

No. 108, *Fergus Falls, Minn.* (1911).—High-school building on Cavour Street between Court and Union Streets, girls' entrance to the basement from the north side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 109, *Sheridan, Wyo.* (1911).—County courthouse, southwest corner of South Main and West Burkill Streets, room in the northwest corner of the basement known as storage vault No. 2. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 110, *Boulder, Mont.* (1911).—Public school south of the courthouse, boys' toilet in the southeast corner of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 111, *Skykomish, Wash.* (1911).—Public-school building, boiler room. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 112, *Olympia, Wash.* (1911).—Washington School building on West Fifth and Quince Streets, boys' toilet in the basement east of the main entrance on the north side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 113, *Heppner, Oreg.* (1911).—Morrow County courthouse, storage room in the middle of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 114, *Truckee, Cal.* (1911).—High-school building, temporary room constructed in the northeast corner of the southern half of the basement. The case was mounted on a concrete pier.

No. 115, *Winnemucca, Nev.* (1911).—Store owned by H. Warren, on Bridge Street, next to the fire station, furnace room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 116, *Ely, Nev.* (1911).—Graded-school building, storage room in the northeast corner of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 117, *Guernsey, Wyo.* (1911).—Guernsey Hotel, basement room about the middle of the south side. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 118, *Pierre, S. Dak.* (1911).—High-school building opposite the Capitol, storage room in basement between the toilet and the gymnasium. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 119, *Fort Dodge, Iowa* (1911).—High-school building, storage room about the center of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 120, *Keithsburg, Ill.* (1911).—Public-school building, temporary room constructed in the basement under the west part of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 121, *Grand Rapids, Mich.* (1911).—Smaller building on the northwest corner of the new high-school grounds, at Fountain and North Prospect Streets, boiler room in the northwest corner of the basement. The case was mounted on the concrete floor.

No. 122, *Angola, Ind.* (1911).—Public-school building on East Water Street between South Wayne and South Martha Streets, storage room in the southeast corner of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 123, *Albany, N. Y.* (1911 and 1914).—Public School No. 24, at Delaware and Dana Avenues, janitor's storeroom in the basement, under the boys' entrance on the east side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 124, *Port Jervis, N. Y.* (1911).—Church Street School building, basement room about the middle of the southeast side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 125, *Atlantic City, N. J.* (1914).—New high school, corner of Atlantic and Massachusetts Avenues, northwest corner of the dark storeroom in the basement, directly under the steps at the Atlantic Avenue entrance. The case was mounted on a slate slab 3 inches thick cemented to the floor.

No. 126, *Bridgehampton, N. Y.* (1914).—High-school building, near the north side of the laboratory room in the basement. The case was mounted on the concrete floor.

No. 127, *Chatham, Mass.* (1914).—In northwest corner of the small concrete fish house belonging to A. E. Thatcher on the north side of the mill pond. The case was mounted on the concrete floor.

No. 128, *Rockland, Me.* (1914).—Home of Fred Burpee, at 104 Limerock Street, in the northwest corner of the south extension of the basement or cellar. The case was mounted on the concrete floor.

No. 129, *Lancaster, N. H.* (1914).—High school, near the intersection of Main and School Streets, in the basement near the northwest corner of the southwesterly room used as a bath and dressing room for the gymnasium. The case was mounted on the concrete floor.

No. 130, *Whitehall, N. Y.* (1914).—Armory at the corner of Willian and Daultney Streets, near the northwest corner of the dark room in the basement. The case was mounted with one brick under each footplate cemented to the concrete floor.

No. 131, *Little Falls, N. Y.* (1914).—Benton Hall School, on the east side of the park, at the corner of Alexander and Waith Streets, in a temporary room constructed in the most northwesterly room of the basement. The case was mounted on the concrete floor.

No. 132, *Watertown, N. Y.* (1914).—High school, on Sterling Street between Washington and Jay Streets, in the carpenter shop in the basement. The case was mounted on the concrete floor.

No. 133, *Southport, N. Y.* (1914).—In the basement of a small store on Pennsylvania Avenue used as a storeroom by Sargent & Sage, whose grocery store is the next building east at the corner of Pennsylvania and Caton Avenues. The case was mounted on a pier built of brick, stone, and plaster of Paris.

No. 134, *Erie, Pa.* (1914).—Public School No. 2, at the corner of Seventh and Holland Streets, in the basement storeroom under the steps at the south entrance. The case was mounted on the concrete floor.

No. 135, *Parkersburg, W. Va.* (1914).—Post office, in the southeast corner of the small room in the northeast corner of the basement. The case was mounted with one brick under each footplate cemented to the concrete floor.

No. 136, *Columbus, Ohio* (1914).—Franklin County Memorial Hall, on East Broad Street, in the northeast corner of a triangular-shaped room called the kitchen, in the basement back of the stage. The case was mounted with one brick under each footplate cemented to the concrete floor.

No. 137, *Indianapolis, Ind.* (1914).—Post office, in a small triangular-shaped room on the Meridian Street side of the basement used as a storeroom by the engineer of the building and directly across the hall from the west elevator. The case was mounted on the concrete floor.

No. 138, *Springfield, Ill.* (1914).—Edwards Public School, at the corner of Lawrence Avenue West and Edwards Street, in a room near the center of the north front of the basement. The case was mounted on the concrete floor.

No. 139, *Lebanon, Mo.* (1914).—New high school, in the furnace room about 2 feet from the corner of the brick-work supporting the boiler. The case was mounted on the concrete floor.

No. 140, *Joplin, Mo.* (1914).—Post office, a small room with a sloping ceiling under the stairway in the northeast corner of the basement. The case was mounted on the concrete floor.

No. 141, *Fort Smith, Ark.* (1914).—Courthouse, in the northeast corner of the room used as a test room for cement, etc., by the city engineer, in the southeast corner of the basement. The case was mounted on the concrete floor.

No. 142, *Texarkana, Ark.* (1914).—Post office, in the northwest room of the basement of the north wing. The case was mounted on the concrete floor.

No. 143, *Hot Springs, Ark.* (1914).—Garland County courthouse, in the north corner room of the ground floor. The case was mounted on the concrete floor.

No. 144, *Alexandria, La.* (1914).—City hall, in one of the small closets under the steps on the northwest side of the basement and just to the left of the short flight of steps leading to the main hall of the basement. The case was mounted on the concrete floor.

No. 145, *Laurel, Miss.* (1914).—Silas Gardner School, in a room on the north side of the basement, the first room to the left when entering the basement at the east door and just across the hall from the domestic-science kitchen. The case was mounted on the concrete floor.

No. 146, *Richmond, Va.* (1915).—Post office, in a room near the center of the south side of the basement used as a storeroom by the internal-revenue department. The case was mounted with one brick under each footplate cemented to the concrete floor.

No. 147, *Emporia, Va.* (1915).—The station is in the county courthouse. Two sets of observations were made, the first in the office of the commissioner of revenue in the south wing of the courthouse and the second in the southeast corner of the mayor's office, which is the next room. For the first set the case was mounted on the wooden floor and for the second set the case was mounted on the concrete floor.

No. 148, *Greenville, N. C.* (1915).—Proctor Hotel, on the corner of Evans and Third Streets, in room No. 2 of the higher or back level of the basement, the second room from the steps leading from the lower or front part of the basement and on the left side of the hallway. The case was probably mounted on the concrete floor.

No. 149, *Wilmington, N. C.* (1915).—County courthouse at the intersection of Third and Princess Streets, in a room in the basement once used as a storeroom for disinfectants by the city health officer. It is on the side of the basement toward Princess Street and the last room but one on the left side of the corridor at right angles to Third Street. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 150, *Cheraw, S. C.* (1915).—Hotel Covington, in a back room on the first floor, the second room from the northwest end of the building and directly opposite the office of Dr. Purvis. The room is separated from the next one by a partition two-thirds of the way to the ceiling. The case was probably mounted on the concrete floor.

No. 151, *Charlotte, N. C.* (1915).—United States assay office, in a small room in the east corner of the basement. The case was probably mounted on the concrete floor.

No. 152, *Asheville, N. C.* (1915).—Post office, in the northeast corner room of the basement which has two small windows opening on Haywood Street. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 153, *Cleveland, Tenn.* (1915).—Post office, in the southwest corner of the basement, in a room used as a rest room for the rural carriers. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 154, *Winston-Salem, N. C.* (1915).—High school on Cherry Street at the head of Third Street, in the southwest corner of the basement in a room used as a storage room. The case was probably mounted on the concrete floor.

No. 155, *Knorrville, Tenn.* (1915).—Western Union office building, on Gay Street near Vine Street, in the basement in a room used as a storeroom by the linemen and about 10 feet from the foot of the stairs leading down from the main office. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 156, *Bristol, Va.* (1915).—Courthouse and city hall, in a room on the south side of the basement next to the southeast corner room. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 157, *Homestead, Fla.* (1915).—High school, in a temporary room constructed on the north end of the west porch. The case was mounted with two bricks under each footplate cemented together and to the concrete floor of the porch.

No. 158, *Sebring, Fla.* (1915).—Kiln for drying lumber, about 40 meters northeast of the electric-light plant and 100 meters northeast of the Atlantic Coast Line Railway station. The case was mounted on a pier made of concrete blocks cemented together, with two bricks under each footplate cemented together and to the top of the pier.

No. 159, *Titusville, Fla.* (1915).—Small office belonging to J. S. Daniels near the northwest corner of Palm and Julia Streets. The case was mounted on a pier made of concrete blocks cemented together, with two bricks under each footplate cemented together and to the top of the pier.

No. 160, *Leesburg, Fla.* (1915).—George W. Wrenneck Building, at the corner of Main and Seventh Streets, in the southwest corner of the back room. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 161, *Cedar Keys, Fla.* (1915).—House belonging to J. B. Lutterdah, at the northeast corner of Fifth and D Streets, in the northwest corner of the south basement room. The case was mounted on a brick pier with two bricks under each footplate cemented together and to the top of the pier.

No. 162, *Macon, Ga.* (1915).—Post office, near the window of the engineer's room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 163, *Albany, Ga.* (1915).—Grammar school at the corner of Broad and Madison Streets, in the northwest corner of the janitor's storeroom in the basement. The case was mounted with one brick under each footplate cemented to the concrete floor.

No. 164, *Pensacola, Fla.* (1915).—Customhouse and post office, in the northeast corner of the customhouse storeroom in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 165, *Opelika, Ala.* (1915).—New brick store on Avenue A, owned by Mrs. Josephine Denniston and rented by J. Lem Satterwhite, in the southeast end of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 166, *Huntsville, Ala.* (1915).—United States courthouse and post office, in the easternmost room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 167, *Arkansas City, Ark.* (1915).—Courthouse, in the west corner of the grand jury room. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 168, *Memphis, Tenn.* (1915).—Customhouse and post office, in the northeast corner of the northeast room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 169, *Mammoth Spring, Ark.* (1915).—Old Fulton County Bank Building, owned by the Citizens Bank of Mammoth Spring, in a small room used for ice storage in the southwest corner of the north basement room. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 170, *Hopkinsville, Ky.* (1915).—Customhouse and post office, in the southeast corner of the northeast room of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 171, *Danville, Ky.* (1915).—Customhouse and post office, near the center of the north end of the room used as a coal bin in the northeast corner of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 172, *Clifton Forge, Va.* (1915).—Courthouse and post office, in the north end of the storeroom near the center of the west side of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 173, *Greenville, Ala.* (1915).—Courthouse, in the west end of the coal bin in the boiler room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 174, *Birmingham, Ala.* (1915).—United States customhouse and post office at the northeast corner of Second Avenue and Eighteenth Street, in the janitor's office in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 175, *Lexington, Va.* (1915).—Post office at the corner of Lee Avenue and Nelson Street, in the southwest end of the storeroom near the center of the northeast side of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 176, *Prestonsburg, Ky.* (1915).—The Bank Josephine, on Main Street, at the foot of the bridge over the Big Sandy River, in the northwest corner of the southwest room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 177, *Traverse City, Mich.* (1915).—Post office, in storeroom in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 178, *Seney, Mich.* (1915).—Bank of the Boggott, Bacheller & Cool Banking Co., in the vault. The case was mounted on the concrete floor.

No. 179, *Oconto, Wis.* (1915).—High school on School Street, in the mechanical drawing room in the south corner of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 180, *Grand Rapids, Wis.* (1915).—Bandelin Hotel on Grand Avenue, in the basement near the middle of the east side. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 181, *Winona, Minn.* (1915).—Post office, in the northeast corner room of the basement. The case was mounted on the brick floor, with one paving brick under each footplate.

No. 182, *Baldwin, Wis.* (1915).—Town Hall, in the rest room in the basement at the foot of the stairs leading from the main entrance of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 183, *Cumberland, Wis.* (1915).—High-school building, in the boiler room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 184, *Cambridge, Minn.* (1915).—High-school building, in the west part of the boiler room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 185, *Brainerd, Minn.* (1915).—Post office at northwest corner of Maple and Sixth Streets, in a room about midway of the west side of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 186, *Aberdeen, S. Dak.* (1915).—Post office and courthouse, in the north end of the small storeroom at the north end of the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 187, *Faith, S. Dak.* (1915).—W. C. Meyer's residence, about 260 meters west-southwest from the Chicago, Milwaukee & St. Paul Railway Station, in the northwest room of the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 188, *Marmarth, N. Dak.* (1915).—Allison Building, on the corner of Main and First Streets, in the west end of a small storeroom in the basement directly beneath the post office. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 189, *Towner, N. Dak.* (1915).—McHenry County courthouse, in the west end of the vault in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 190, *Crosby, N. Dak.* (1915).—Crosby graded school, in the northwest room in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 191, *Crookston, Minn.* (1915).—Franklin School, in the east part of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 192, *Poplar Mont.* (1915).—Poplar public school in the northeast part of the town, in the east room in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 193, *Miles City, Mont.* (1915).—Lincoln School, on Lake Street, in the south part of the town, in the south end of the west storeroom in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 194, *Huntley, Mont.* (1915).—Huntley Hotel, north-northwest of the railway station, in the southeast corner of the basement room under the south part of the hotel. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 195, *Lander, Wyo.* (1915).—Post office and courthouse, in the south end of the storeroom in the south corner of the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 196, *Faribault, Minn.* (1915).—Central School, in the southeast corner room of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 197, *St. James, Minn.* (1915).—County courthouse, in the basement midway of the north side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 198, *Edgemont, S. Dak.* (1915).—Public-school building, in the southwest corner of the southeast room in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 199, *Dawson, Minn.* (1915).—High-school building, in the dark room in the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 200, *Cokato, Minn.* (1915).—High school, in the basement under the central part of the east side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 201, *Wasta, S. Dak.* (1915).—Residence of James Trask on the east side of the street one block west and two blocks north from the railway station, in the northwest corner of the cellar under the southeast corner of the house. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 202, *Moorecroft, Wyo.* (1915).—Public-school building, on the south side of the east room in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 203, *Duluth, Minn.* (1915).—County courthouse, in a room known as the connecting hall in the basement under the center of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 204, *Osage, Iowa* (1915).—High school, in the basement near the middle of the south side of the building and directly under the galvanized-iron air duct. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 205, *Randolph, Nebr.* (1915).—Public school near the Burlington Railway station, in the southwest corner of a temporary room constructed in the west end of the southernmost ventilating room in the basement under the east side of the building. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 206, *Valentine, Nebr.* (1915).—Public school, in the southeast corner of the southeast room in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 207, *Wheeling, W. Va.* (1915).—German Bank Building, in the basement under the Western Union Telegraph office. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 208, *Leon, Iowa* (1915).—North School, in the south side of the northwest room on the ground floor. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 209, *Laurel, Md.* (1915).—Residence of Col. Frank E. Little on Main Street about 10 minutes walk from the Baltimore & Ohio Railway station, in the east corner of the easternmost room in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 210, *Harrisburg, Pa.* (1915).—Central High School, in the basement near the center of the north side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 211, *Pittsburgh, Pa.* (1915).—Second Ward School on Sherman Avenue just north of North Avenue in the north-side section of Pittsburgh, in the basement under the east front of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 212, *Rockville, Md.* (1915).—High school, in the north end of a small room formerly used as a printing shop in the basement under the north side of the building. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 213, *Upper Marlboro, Md.* (1915).—Masonic Hall on the south side of Main Street about 80 meters west of the courthouse, in the west side of the southeast room in the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 214, *Fairfax, Va.* (1915).—Bungalow belonging to the Rural Homes Development Co. about 300 meters west-northwest from the residence of E. A. Capen, in the southwest corner of the basement. The case was mounted with a small concrete block under each footplate cemented to the concrete floor.

No. 215, *Crisfield, Md.* (1915).—Residence of J. H. Riggin, 101 South Somerset Avenue, in the rear part of the basement. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 216, *Fredericksburg, Va.* (1915).—Post office, storeroom in the basement under the north side of the building. The case was mounted on the concrete floor.

No. 217, *Dover, Del.* (1915).—Wilmington Conference Academy, in the basement under the gymnasium at the middle of the north side of the building. The case was mounted with two bricks under each footplate cemented together and to the concrete floor.

No. 218, *North Tamarack near Calumet, Mich.* (1902).—Observations were made at three different levels at North Tamarack Mine, at the surface of the ground, at a depth of 1200 feet, and at a depth of 4600 feet. The two stations below the ground were occupied by Prof. F. W. McNair, of the Michigan College of Mines. His results are not published here. A temporary pendulum room was probably used for the surface observations. The case was mounted on a masonry pier.

No. 219 *Hagerstown, Md.* (1915).—Post office, in the northeast corner of the boiler room in the northwest corner of the basement. The case was mounted with a small concrete block under each foot plate cemented to the concrete floor.

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